Exhibit A

BEFORE THE ILLINOIS POLLUTION CONTROL BOARD

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IN THE MATTER OF: Petition of Electric Energy, Inc. For a Finding of Inapplicability or, in the Alternative, an Adjusted Standard from 35 Ill. Adm. Code Part 845

AS 2021-005 (Adjusted Standard)

AFFIDAVIT OF LAUREN HUNT MARTIN

I, Lauren Martin, certify under penalty of perjury pursuant to Section 1-109 of the Illinois Code of Civil Procedure, 735 ILCS 5/1-109, that the statements set forth in this affidavit are true and correct, and further state that if called upon to testify in this matter, I would competently testify as follows:

1. I am employed by the Illinois Environmental Protection Agency ("Illinois EPA" or "Agency") as an Environmental Protection Geologist II in the Hydrogeology and Compliance Unit ("HCU") within the Groundwater Section of the Bureau of Water, and I am located in Springfield, Illinois. I have been employed by the Illinois EPA since February of 2020.

2. I have a Bachelor of Science degree in geology from Western Illinois University and a Master of Science in hydrogeology from Illinois State University. My curriculum vitae is attached (Attachment 1) for further detail about my training and experience.

3. As a Geologist in the HCU, my duties include: providing review of hydrogeologic assessments and reports, and providing technical input on the same as well as special projects requiring hydrogeologic and engineering geology expertise; providing construction, engineering geology, and hydrogeologic expertise to Bureau of Water permit programs (industrial, mines and municipal) and Public Water Supply permits; responding to questions from the regulated community, public and other governmental agencies about the provisions of the Illinois Environmental Protection Act ("Act"), Illinois Groundwater Protection Act (ILGPA), and Illinois

Pollution Control Board ("Board") rules adopted thereunder; project management of sites subject to corrective actions under the Act or Board rules; testifying before the Board on proposed rules and in various proceedings; and assisting in the implementation of source water protection programs. As part of these duties, I served as a witness on behalf of the Groundwater Section in support of Illinois EPA's proposed Part 845 throughout the Illinois Pollution Control Board's rulemaking proceedings in R2020-019.

4. I have reviewed the Petition of Electric Energy, Inc. for a Finding of Inapplicability or, in the Alternative, an Adjusted Standard from 35 Ill. Adm. Code Part 845 ("Petition"), along with its supporting documents.

5. I have personal knowledge of the facts set forth in Illinois EPA's Recommendation to the Board as stated below.

6. Figure 2-5 of Petitioner's Exhibit 2 displays drawings illustrating that the Joppa West Ash Pond ("JWAP") was created using embankments in conjunction with a natural topographic depression. Figure 2-3 of Petitioner's Exhibit 2 shows that the design holds CCR and liquids. The embankments have not been removed and the natural topographic depression still exists under the CCR fill.

7. The JWAP (including the settling basin and the larger CCR surface impoundment collectively known as the Joppa West Ash Pond) allows the collection and holding of storm water and CCR material, and the intermingling of storm water and groundwater, within the CCR surface impoundment.

8. Field verification of the compressive strength of materials that are encountered during test pitting and soil sampling assist in the verification of the compaction of the fill materials *in situ* and provide insight on the manner of placement. Materials that are placed by wet sluicing

would not have been compacted as a part of placement. Materials that are dry placed will necessarily compact to some extent due to material handling equipment and may be intentionally compacted to allow for more capacity to store the material and will not be expanded for water saturation.

9. Appendix D of Petitioner's Exhibit 2 contains test pit logs. Test Pit Log 13 documents flowable ash at 2.5 feet. Several other test pit locations were either terminated at 2.5 to 3 feet below ground surface, with "wet" (saturated) conditions or increased moisture conditions encountered. Flowable ash represents saturated, very soft ash (very loose or uncompacted ash) below the water table. Test pit logs did not provide compressive strength field testing results.

10. Attachment 3 of Petitioner's Exhibit 3 contains boring logs, well diagrams, well development, and abandonment forms. Boring logs provide field compressive strength testing for clays and silts. The results of field compressive strength testing of the materials that were tested confirmed the lack of compaction within the JWAP.

11. According to the boring logs from XTPW01 and XSB02, the JWAP contains ash at 0.8 to 35 feet below ground surface ("bgs") and 2.5 to 40 feet bgs, respectively. Groundwater level during drilling was 1.5 feet bgs at XTPW01: moist to wet was logged for XTPW01 at 1.5 to 10 feet bgs, with "wet" being logged after that, signifying that saturated conditions were encountered during drilling. Sonic drilling was performed at the location making notation of other saturation indications not possible. No water level is indicated at XSB02 due to the drilling method (also sonic) and smaller diameter of the drilling rods causing soil samples retrieved to be dried out. XTPW01 was drilled through the middle of the JWAP, XSB02 was drilled on the south side of the JWAP, and no borings were available for review of the material within the settling basin on the

south end of the JWAP. No other borings presented in Petitioner's Exhibit 3 were logged and investigated within the JWAP (including its settling basin).

12. Attached to the Recommendation as Exhibit B ("Rec. Ex. B") is a Phase I Hydrogeological Assessment Report for the Coal Combustion Product Impoundments at the Joppa Generating Station in Joppa, Illinois, dated July 23, 2013 and submitted to Illinois EPA on July 30, 2013. This report is kept by the Illinois EPA in the regular course of business, and it is the regular course of business of the Illinois EPA to transmit the information thereof to be included in this record. The 2013 Hydrogeological Assessment Report, submitted to Illinois EPA on July 30, 2013 and attached to the Recommendation as Exhibit B, is an exact duplicate of the original.

13. My review of the boring logs of the wells surrounding the JWAP confirm that the JWAP is surrounded by clay material. The 2013 Hydrogeologic Assessment Report for the Joppa Station provides site-specific hydraulic conductivity of the clay materials (5.9 x 10⁻⁶ centimeters per second ("cm/s"). *See* Rec. Ex. B at ES-1. Additionally, the blow count values collected during drilling of wells G101, G111, G112B, G112C and G113 reveal that the clay materials encountered at 0 to 50 feet just outside of the JWAP have greater compaction than the materials in the JWAP. *See* Ex. B, App. B The compaction and the hydraulic conductivity indicate that most of the groundwater recharge comes from precipitation and infiltration.

14. Though vegetation exists and has formed an organic layer, it has not prevented erosion of the berms or the surface of the JWAP. CCR material eroded from erosional pathways over uncompacted materials enables the CCR material to travel from the JWAP to Outfall 011 by way of the storm water runoff at the JWAP. Erosion pathways are not always mature enough to be visible from an aerial photograph. Erosional pathways are preferential flow paths for stormwater runoff within the CCR surface impoundment. In many areas, erosional pathways are likely exposed

CCR due to the lack of thickness in the overlying organic sediments that have developed naturally since sluicing of CCR stopped. Though CCR is no longer sluiced to the JWAP, liquids that enter the JWAP flow to low areas, likely carrying eroded CCR material, where they are decanted for discharge. *See* Pet. Ex. 2, Fig. 2-4. Decanting of water from within the impoundment is the same process that was taking place when CCR was being sluiced to the impoundment. Due to the inadequate vegetative cover, transport of CCR necessarily occurs during the erosional processes, likely resulting in its discharge during the decanting process.

15. Table 3.1 of Petitioner's Exhibit 4 identifies monitoring well TPZ117D as the only monitoring well finished in the upper aquifer ("UA"). Figure 3.5 displays TPZ117D as not being directly down gradient of the JWAP, although TPZ117D is nested with TPZ117, TPZ117 is installed in the upper confining unit (UCU) and does have exceedances. Because TPZ117D is not installed in the same hydrogeologic unit as the rest of the monitoring wells at the JWAP, at least an upgradient well, near G-101 and another downgradient well, near G112C, are required for adequate hydrogeologic characterization of the UA.

16. Groundwater flow direction must be based on a minimum of three wells in the same geologic formation. To have a potentially approvable GMZ under Part 620, the owner or operator would have to conduct additional site investigation and assessment of the UA to assure that contaminants from the JWAP are not migrating through the UCU into the UA, in addition to any other required activities.

17. A sufficient soil cover at the JWAP should provide a barrier to groundwater infiltration at the JWAP. The barrier then reduces or eliminates the influx of water with higher amounts or varied amounts of dissolved oxygen. The dissolved oxygen changes the groundwater geochemistry potentially spurring microbial and geochemical processes. The microbial and/or

geochemical processes may enable the potential release of additional metals from the JWAP CCR material to the groundwater downgradient.

18. Topsoil is produced from vegetation, composed of partially decomposed organic materials and thus is not a clay material with a hydraulic conductivity that would prevent infiltration. The JWAP is fully saturated with static groundwater recharged directly through the CCR material in the JWAP, and the JWAP cover is not sufficient to prevent infiltration. However, the mass of heavy metals and other constituents listed in Section 845.600 may have reduced because of mass transport and geochemical processes over the last 45 years. The extent of constituents listed in Section 845.600 remaining above GWPS should be fully investigated. Total metals, as opposed to dissolved metals, in accordance with Section 845.640(i) should be used to compare with Section 845.600 GWPS.

19. Table 3 of Petitioner's Exhibit 3 presents data collected during the 2010 to 2013 Hydrogeologic Assessment and groundwater analytical from samples collected during March 2021. Data from the March 2021 sampling event exhibits what would be GWPS exceedances for pH, arsenic, boron, lithium, molybdenum, and selenium at the source well, XTPW01. What would be exceedances of antimony, arsenic, boron, lead, cobalt, beryllium, and sulfate are present at downgradient wells, TPZ114, G112C, TPZ116, and TPZ117. There are no exceedances in TPZ117D, exhibiting that there is no direct downward vertical hydraulic gradient carrying contamination vertically downward. Alternatively, geochemical reactions and/or microbial processes within the source material and source groundwater may be resulting in the exceedances of several heavy metals in downgradient wells. The reactive transport of metals at the JWAP has not been investigated fully, as the full extent of the total metals has not been characterized.

20. The basic requirements for geochemical monitoring, or groundwater stabilization parameters, have been a part of the Part 620 standards since its inception. The additional field stabilization parameters, dissolved oxygen and oxidation-reduction potential, are required for adequate determination of collection of a representative sample at each individual monitoring well and adequate characterization of geochemical conditions. The additional field stabilization parameters are required for groundwater sampling under Part 257. The necessity for reporting of groundwater stabilization parameters are imperative now that the published materials on geochemistry and metals transport has definitively determined that the existence of reactive transport of metals. I have provided two such published works as Recommendation Exhibits E and F in support of the Agency's Recommendation and the necessity of reporting groundwater stabilization parameters.

21. The Human Health Risk Assessment ("HHRA") presented in Petitioner's Exhibit 4 uses mostly dissolved data collected between 2010 and 2013 and does not accurately present the data collected at the JWAP, omitting G112B and XPTW01 and not addressing what would be exceedances of the GWPS. Table 3.2, which is based on detections and not exceedances of the GWQS or GWPS, summarizes the mostly dissolved metals groundwater data, while omitting the majority of downgradient data from the groundwater results and providing an outsized proportion of cross gradient and upgradient data from outside of the groundwater plume. The arsenic detection limit is above the GWPS and GWQS for the samples collected from 2010 to 2013. G112B was replaced by G112C at the beginning of 2013, skipping one sampling event in the fourth quarter of 2012. The arsenic analytical samples at G112B are above the GWPS and GWQS in six out of nine dissolved samples collected from 2010 to 2012. In the remaining three samples, the laboratory reporting limit exceeded the GWPS, meaning effectively no sample was collected and analyzed

for arsenic during those quarters. The samples collected at TPZ117D should not be compared to other samples, as the samples were collected from a different aquifer. Because the majority of sample analytical data that is used for the evaluation is based on dissolved parameters and not total analytical parameters, the data cannot be used to accurately predict whether precipitation of cobalt is occurring or whether there is a source material that is not adequately characterized at the JWAP, primarily because cobalt is not appearing in dissolved form.

22. The HHRA was based mostly on dissolved metals concentrations and general chemical parameters listed in Section 620.410 and excluded data for monitoring well G112B, which has been abandoned and replaced with well G112C. The abandonment of G112B and installation of G112C was completed with Agency approval for the purpose of the hydrogeologic assessment. G112C still has what would be Section 845.600 GWPS exceedances for cobalt and boron, and also exceeds for boron, cobalt and other parameters monitored under Section 620.420. The use of limited groundwater data, and four quarters of sampling data at G112C compared to twelve quarters of data at upgradient and cross gradient wells (G111, G101, G113), does not accurately weigh the risk associated with the direct downgradient exceedance of multiple GWQS and GWPS.

23. Only one round of sampling for total metals concentrations has been conducted at JWAP. The total metals and general chemical constituents were collected in March 2021. There is an extreme change in pH between the JWAP source well and the downgradient wells indicating a potential for a corrosive environment. The source well is not exceeding all the same constituents as the down gradient wells. Thus, the results of the analyses provided an initial characterization of the potential geochemical complexities that need further investigation.

24. Attached to the Recommendation as Exhibit Y is a draft representation and geospatial configuration I created, utilizing the February 2020 Google Earth image, EEI's March 2021 sampling data and estimated boring locations. Exhibit Y is a fair and accurate depiction of the March 2021 data set and the corresponding sampling locations at the Joppa Station.

25. Exhibit Y is a geospatial configuration of what would be exceedances of Section 845.600 at the JWAP. The pH at the source, XTPW01, was 11.1, whereas the pH at the other wells were 7+-0.3, signifying an acidic groundwater environment that is changing the pH in the source to as low as 6.7 at TPZ117. Exhibit Y also shows that the JWAP groundwater at the source and downgradient is either actively changing due to unknown geochemical parameters and/or the source material has not been adequately characterized. Geochemistry must be understood to eliminate reactive transport of the metals constituents at the West Ash Pond.

26. Attached to the Recommendation as Exhibits N through V are aerial photographs of the Joppa Station from October 1971 through February 2020 that I obtained from Google Earth and Illinois Department of Transportation. I utilized the publicly available resource to create demonstrative exhibits identifying the Joppa West Ash Pond ("JWAP"). Other than the identification markers I added to the images, Recommendation Exhibits N through V provide exact duplicate images of those obtained from Google Earth or Illinois Department of Transportation.

27. Exhibit N shows the Joppa Station in operation in October 1971. The JWAP is evident with wet CCR material being placed through wet placement methods. The plant is operating with emissions flowing out of the stack at the plant. There is a pond to the northeast of the JWAP that is in the same location as the pond associated with the discharge from Outfall 011 that NPDES Permit IL0004171 was modified to include in 1993. The pond functions to collect stormwater runoff from the JWAP and discharges to the Ohio River ("discharge pond").

28. Exhibit O shows the Joppa Station in operation in August 1980. The settling basin on the south side of the JWAP still has water in it. There is erosional surface scarring apparent in the aerial photograph depicting the surface water drainage throughout the JWAP to the low areas. The JWAP is still exposed on the north side with evidence remaining of wet placement of CCR material placement. The northeast pond identified in Exhibit N remains present in the 1980 aerial photo.

29. Exhibit P shows the Joppa Station in operation in March 1993. The settling basin on the south side of the JWAP still has water in it. There is erosional surface scarring apparent in the aerial photograph depicting the surface water drainage throughout the JWAP to the low areas. The JWAP has ponding in several locations but also has vegetation growing on the north and south sides. Just northeast of the JWAP is a discharge pond for draining of the remaining water in the JWAP on the north side. The pond is in relatively the same location as the previously mentioned pond to the northeast of the JWAP but has been modified to encompass a smaller area and a road separates it from the JWAP.

30. Exhibit Q shows the Joppa Station in operation in November 1998. The erosional surface scarring apparent in Exhibit P remains present and leads to low points of ponding at the JWAP. The settling basin on the south side of the JWAP still has water in it. The JWAP has become fully overgrown and has two utility corridor landscaping strips evident crossing it from southeast to northwest. The discharge pond and discharge from the JWAP is still present.

31. Exhibit R shows the Joppa Station in operation in March 2005. The erosional surface scarring apparent in Exhibits P and Q remains present and leads to low points of ponding at the JWAP. The settling basin on the south side of the JWAP still has water in it. The JWAP has become fully overgrown and has two utility corridor landscaping strips evident crossing it from

southeast to northwest and connecting with a third. The discharge pond and discharge from the JWAP is still present.

32. Exhibit S shows the Joppa Station in operation in May 2015. The erosional surface scarring apparent in Exhibits P, Q and R remains present but heavily vegetated and leads to the discharge pond just northeast of the JWAP. The settling basin on the south side of the JWAP is overgrown with vegetation and no water is evident. The JWAP has become fully overgrown and has two utility corridor landscaping strips evident crossing it from southeast to northwest and connecting with a third. The discharge pond and discharge from the JWAP is still present.

33. Exhibit T shows the Joppa Station in operation in March 2017. The erosional surface scarring apparent in the earlier aerial photographs remains present but heavily vegetated and leads to the discharge pond just northeast of the JWAP. The settling basin on the south side of the JWAP is overgrown with vegetation and no water is evident. The JWAP has become fully overgrown and has two utility corridor landscaping strips evident crossing it from southeast to northwest and connecting with a third. There is an exposed spot on the northwest corner. The discharge pond and discharge from the JWAP is still present.

34. Exhibit U shows the Joppa Station in operation in September 2018 and Exhibit V shows the Joppa Station in operation in February 2020. The erosional surface scarring apparent in the earlier aerial photographs remains present but heavily vegetated in both aerials and leads to the discharge pond just northeast of the JWAP. The settling basin on the south side of the JWAP is overgrown with vegetation and no water is evident. The JWAP has become fully overgrown and has two utility corridor landscaping strips evident crossing it from southeast to northwest and connecting with a third. The exposed spot on the northwest corner is covered with low lying vegetation. The discharge pond and discharge from the JWAP is still present.

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35. Petitioner's Exhibit 2, an Expert Engineering Evaluation for Adjusted Standard for Part 845, also performs an aerial photography review of the site. Illinois EPA does not necessarily agree with the aerial findings that the JWAP has not received ash or CCR materials since October 15, 2015. The sediments discussed in Petitioner's Exhibit 2 correlate with the exposed area shown in Exhibit T. See Pet. Ex. 2 at 4. The material was dredged "from the Ohio River near the original discharge structure" and placed within the JWAP. Petitioner's Exhibit 2 does not provide a date for this dredging and placement of material in the JWAP. However, Exhibits S and T indicate that the vegetation was cleared to provide space for the dredged sediments to be placed within the JWAP after October 15 or November 15,2015 and before April 2016 or between October 15/November 15, 2016 and March 2017 due to US Fish and Wildlife Service vegetation clearing guidance for locations where the endangered species use the trees present as habitat. This sediment, which likely contains CCR material, was likely placed after the enactment of Part 257 and has likely been covered with an undetermined amount of fill material as seen in Exhibit T. See Rec. Ex. T, U, and V. Additionally, NPDES Permit No. IL0004171 currently authorizes discharge from the "former ash pond," indicating that the sediments include materials from the former ash pond, JWAP.

36. When the Joppa Station ceased operation of the JWAP in 1973, the whole of the JWAP was not graded; portions were graded leaving low areas with standing water on both ends of the JWAP. While portions of the JWAP were graded for the utility corridor, the ponding of water is still apparent in Exhibits O (1980), P (1993), Q (1998), and R (2005). Upon close inspection, Exhibits O through V show erosional pathways leading to low areas. As the JWAP becomes more vegetated, the erosional surfaces are covered from view by trees, but still have greener and heavier vegetation following the relative same paths easily seen in earlier aerial photographs. Petitioner's Exhibit 2 shows storm water flow paths to the permitted outfall for

stormwater and other water from the JWAP. With the lack of cover and exposed CCR sediments, CCR is likely travelling out of the JWAP and into the outfall or streams leading to the outfall.

37. During the course of the Hydrogeologic Assessment, EEI did not evaluate the JWAP CCR material for leaching, geochemical changes to the groundwater over distance or for exposed sediments.

38. The cost estimate in Petitioner's Exhibit 2 assumes that the infiltration from precipitation through the surface of the CCR surface impoundment is not significant and that the groundwater chemistry is homogeneous and stable, which is contradictory to the data collected in March 2021. The March 2021 data shows an acidic groundwater environment with potential leaching of heavy metals occurring. Cobalt, lead, beryllium, antimony, and sulfate occur downgradient of the source well which may be indicating that leaching of the aforementioned metals and general chemistry parameters is occurring. Those heavy metals and general chemistry parameters occurred downgradient above GWPS. Arsenic is also above GWPS both within the CCR surface impoundment and down gradient of the JWAP. At best, the JWAP CCR surface impoundment has not been fully characterized to understand where the cobalt, lead, beryllium, antimony and sulfate are originating.

39. I reviewed the Source Water Assessment Protection Program ("SWAP") website that identifies surface water intakes and potable wells in the state. Attached to the Recommendation as Exhibit Z is a screenshot of the SWAP website, which is a fair and accurate depiction of the SWAP website and the distance from the Joppa Station to the CWS River Intake Zone 1 Protection Area.

40. According to the SWAP website. The Ohio River at the JWAP flows northwest to the Mississippi River entering a Community Supply Well River Intake Zone 1 Protection Area

within 5 miles of the JWAP. *See* Rec. Ex. Z. The JWAP is discharging to the Ohio River upstream of the protected area. The potential for discharge constituents associated with CCR material from the JWAP to be present in the Ohio River from Outfall 011 is not included in the Conceptual Site Model or Section 3.2 of Petitioner's Exhibit 4. Surface water sampling included mercury only at Outfall 011 and sampling was ceased prior to 2015. Thus, the exposure pathway has not been fully examined.

41. Groundwater has not been fully investigated at this time to substantiate the conclusions of the HHRA or compliance with regulatory limits presented in the Petition. Until March 2021, groundwater samples were filtered, and reported as dissolved, and are not representative of the total metals and general chemistry constituents. Additionally, characterization of the geochemistry of the groundwater has not been completed. Geochemistry must be understood to eliminate reactive transport of the metals constituents at the JWAP.

42. A sufficient evaluation of the organic clay cover and/or remaining heavy metals within the CCR materials of the JWAP and groundwater would require sufficient groundwater results exhibiting the efficacy of the cover or lack of remaining heavy metals for transport in the groundwater. The evaluation should include five years of quarterly analytical data for total metals and general chemical parameters in accordance with Section 845.600. Sufficient data would typically be a minimum of 10 data points for each groundwater season (low season and high season) to properly characterize the effects of precipitation, infiltration, potential flooding, and other potential groundwater recharge impacts at the JWAP.

FURTHER AFFIANT SAYETH NOT

Tata LAUREN HUNT MARTIN

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State of Illinois County of Sangamon

Subscribed and Sworn to before me this 32 day of November 2021.

Notary Public

OFFICIAL SEAL **DAWN A. HOLLIS** NOTARY PUBLIC. STATE OF ILLINOIS MY COMMISSION EXPIRES 03-21-2025

Attachment 1

CURRICULUM VITAE

LAUREN HUNT MARTIN, M.S.

1021 N Grand Avenue East Springfield, Illinois 62704 Illinois Environmental Protection Agency Bureau of Water Division of Public Water Supplies Groundwater Section Springfield, Illinois Environmental Protection Geologist II February 2020 to Present

Ms. Martin has been employed as an engineering geologist in the construction materials testing and geotechnical engineering consulting since 2001 and has been employed as a geologist and hydrogeologist in the environmental consulting industry since 2005. Ms. Martin started at the Illinois EPA in February 2020. During the short time that Ms. Martin has been at the Illinois EPA, Ms. Martin assisted in updates to the Part 845 regulations, implementation of Part 845, implementation of Part 620, and amendments to Part 620. Ms. Martin is involved as project manager for mines, industrial and municipal sites for ongoing support and decision making.

Professional History

Jacobs Engineering (Formerly CH2M) Chicago, Illinois Geologist August 2005 to January 2020

Subject Matter Expert, Bedrock Geology, Confidential Federal Client, Iowa, August 2016 to January 2020. Jacobs Engineering is performing the site investigation for a Remedial Investigation for a large active military installation. Ms. Martin was subject matter expert for the investigation into bedrock. Ms. Martin also assisted in implementation of vegetation clearing, site safety management, site investigation management.

Task Coordinator and Technical Expert, Confidential State Client, Wisconsin, January 2017 to January 2020. Phase I Update for ongoing transportation design project. Ms. Martin wrote and consulted on the proposal and Phase I Update for the client deliverable.

Task Coordinator and Assistant Project Manager, LUST Site, Confidential Federal Client, Illinois, August 2017 to January 2020. Jacobs Engineering is performing the site investigation and corrective action for a LUST site in western Illinois at a former large active military installation. Ms. Martin was the task coordinator and assistant project manager. In a technical role Ms. Martin assisted in providing guidance in closing with monitored natural attenuation coupled with other possible closure alternatives.

Task Coordinator and Project Manager for H&S, Confidential Private Client, Cook and DuPage Counties, Illinois, 2012 to January 2020. Jacobs Engineering is the Design Corridor Manager for a premier transportation project for a confidential private client. Ms. Martin was the Task Coordinator various tasks including serving as the Project Manager for Safety, coordinated the combined geotechnical and environmental field investigation at O'Hare International Airport in 2014 and the follow up environmental field investigation in 2016 including evaluations of soils pursuant to 35 Ill. Admin. Code 1100. Ms. Martin was the task manager for combining the geotechnical and environmental field investigation for the borrow source material along and near the project right of way including identifying design needs and environmental testing needs to comply with 35 Ill. Admin. Code 1100. Coordination consisted of logistics for implementation of field work, work planning, and reporting including coordinating with the client and guiding internal team to ensure design needs were met. Logistics included meeting with Chicago Department of Aviation, FAA, Illinois Tollway, Illinois Department of Transportation, and coordination of access and runway closures for the purpose of field events.

Project Manager and Task Manager, Confidential Private Client, Illinois, February 2008-December 2016. Project site is a liquids terminal near Chicago, Illinois. Site has had many spills of various chemicals over the years around loading racks for railcars and semi-trucks and docks for loading barges. Ms. Martin managed tasks and projects including proposals, emergency environmental compliance response, site remediation, and site characterization. Emergency compliance response included overseeing emergency soil removal actions and subsequent reporting and regulatory agency coordination. Site remediation included emergency spill clean-up, construction of a geomembrane, and mentoring of junior staff on implementing construction plans. Site characterization included installing wells, drilling boreholes, gauging NAPL, and collecting groundwater data requiring mitigation of a multitude of gases, chemicals and subsequent safety hazards associated with chlorinated solvents, petroleum products and proprietary chemicals.

Assistant Project Manager, Site Superintendent, Construction Quality Manager, and Site Safety and Health Officer, Confidential Federal Client, Illinois, September 2014 to September 2016. The Project included the remediation of a railyard within a former military base for coal containing arsenic. Ms. Martin was the assistant project manager during work planning and reporting. During the construction phase, Ms. Martin was the site superintendent, construction quality manager, and site safety and health officer managing all site operations and contractors.

Technical Hydrogeology Lead, Confidential Federal Client, Illinois, August 2010 to July 2014. Project was a former Radar School for the military during WWII. Ms. Martin designed and implemented the technical approach for closure of the site. Ms. Martin wrote and presented environmental data findings and proposed plan to the public in the public meeting. The Site went to a No Further Action Record of Decision in 2013/2014.

Site Characterization Site Manager, Confidential Private Client, Middle East, January to July 2009. The Project involved the design of four new nuclear reactors and surrounding support structures at two proposed sites. Ms. Martin provided oversight and review of project documents for the site characterization during the field investigation and work planning for four new nuclear reactors at two proposed sites. The field investigation included geotechnical, hydrogeologic, geologic, biologic, geophysical and meteorological data collection and analyses.

Geotechnical Field Investigation Lead, Confidential Private Client, Abu Dhabi, UAE, August to November 2008. The Programme was a \$2+ billion Design/Build Tunneling Project for the City of Abu Dhabi in the United Arab Emirates. Ms. Martin led the field investigation including management of contractors from various countries of origin for the first one third section of the 25 mile long tunnel design on behalf of the programme ensuring that the field documentation and laboratory testing was completed as per the tunneling and geotechnical engineer's specifications.

Field Team Member, Field Team Leader, and Task Lead Assistant, Confidential Power Plant, Confidential Location, May-August 2006 and December 2006 to February 2007. The Project involved the design of two new nuclear reactors and surrounding support structures at an existing nuclear power plant. Ms. Martin actively participated in and led various tasks during the Final Safety Analysis Report field work and report construction. Tasks included data collection, data validation, software validation, data analyses and task management.

Various other Geotechnical and Environmental projects. 2005 to 2019. Ms. Martin provided project support, field investigation leadership and implementation to a variety of geotechnical and environmental projects aside from the aforementioned, performing groundwater sampling,

geotechnical field sampling and drilling, well installations, quality control and quality assurance field oversight.

Nicor 2004 Hudson Gas Storage Field, Hudson, Illinois Reservoir Engineering Intern

Ms. Martin worked as a Reservoir Engineering Intern for the Summer of 2004 for Nicor. Ms. Martin's work tasks included supervising the seismic survey crew for her thesis, learning Geographix Software, reducing and analyzing data from the well logs for the various gas storage fields.

Whitney and Associates, Inc. Peoria, Illinois Engineering Geologist and Construction Inspector

Ms. Martin performed various concrete, soils, and asphalt quality assurance and quality control inspections at commercial and federal construction sites. Ms. Martin operated an IDOT and ASTM certified soils and concrete laboratory.

Education

Bachelor of Science, Geology, Western Illinois University

Master of Science, Hydrogeology, Illinois State University

Publications

Peterson, Eric, Lauren I. Martin, and David Malone. Identification of Potential Vertical Gas Migration Pathways Above Gas Storage Reservoirs, World of Engineering, 2015.

Certifications

OSHA 10-hour Construction Safety Awareness, 2005

OSHA 30-hour Construction Safety, 2015

USACE Construction Quality Manager, 2015-2020

WHMIS Certification (safety certification required for environmental site work in Canada),

2010

Additional Training

OSHA HAZWOPER 40-hour Training, 2005; 8-hour Refresher Training, Annually 2006 to

2019

First Aid/CPR Training, Annually or Biannually 2005 to 2019

Munitions Safety Awareness, 2011

Bloodborne Pathogens, 2018

Dangerous Goods Shipping, 2017

Fire Extinguisher Use Training, 2018

Arsenic, 2018

Asbestos, 2005

Behavior Based loss Prevention Systems Training, 2007

Benzene, 2013

Electrical Safety, 2017

Ergonomics Training, 2005

Excavation Safety Training, 2005

Fall Protection Safety Training, 2005

Field Awareness Safety Training, 2005

Global Harmonization Training, 2013

Hand Safety, 2018

Hazard Communication Training, 2005

Ladder Safety, 2005

Lead Safety, 2016

Manual Lifting Safety, 2016

Military Munitions Rule Training, 2018

Noise/Hearing Conservation, 2014

Personal Protective Equipment Training, 2018

Project Manager Health, Safety and Environment Training, 2013

Railroad Contractor Orientation Training, 2010

Railroad Education for Contractors (On-Track), 2010

Railroad Safety Online Training, 2013

Remediation Waste Management Training, 2018

Respirators-Level C, 2018

Various Site Safety Coordinator Trainings in accordance with 29 CFR 1920, every 3 years

2005-2018

Smith System Small Vehicle Backing and Forward Motion Trainings, 2012

Subcontractor Management Training, 2010

Traffic Control Training, 2013

Waste Management Training, 2018

Exhibit B

IEPA - DIVISION OF RECORDS MANAGEMENT RELEASABLE MAY 25 2017 REVIEWER: JMR

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PHASE I HYDROGEOLOGICAL ASSESSMENT REPORT

Coal Combustion Product Impoundments Joppa Generating Station Joppa, Illinois

Project No: 2126

July 23, 2013



JUL 3 0 2013

DIVISION OF FUBLIC WATER SUPPLIES ENVIRONMENTAL PROTECTION AGENCY STATE OF ILLINOIS



ENVIRONMENTAL CONSULTANTS

234 W FLORIDA ST. MILWAUKEE, WI 53204 (P) 414.837.3607 (F) 414.837.3608

PHASE 1 HYDROGEOLOGICAL ASSESSMENT REPORT

COAL COMBUSTION PRODUCT IMPOUNDMENTS JOPPA GENERATING STATION JOPPA, ILLINOIS

Project No. 2126

Prepared For:

ELECTRIC ENERGY INC and AMEREN ENERGY GENERATING COMPANY

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EXECUTIVE SUMMARY

Background and Objectives

Electric Energy Incorporated (EEI) and Ameren Energy Generating Company own and operate the Joppa Generating Station in Joppa, Illinois. The coal-fired power station currently operates one impoundment for coal combustion product (CCP) management purposes, and has another impoundment that is no longer in service. To assess the potential for constituent migration from the impoundments as requested by the Agency in their correspondence dated April 10, 2009 and a follow-up letter on January 25, 2013, EEI commissioned a hydrogeologic study, water well survey, development of a groundwater monitoring plan, and an initial groundwater quality assessment. This report reviews hydrogeologic data pertinent to the site, groundwater quality data, the potential for off-site migration in the event of a release from one of the impoundments, and whether or not there are potential groundwater receptors in the event of a release.

Hydrogeology

Site-specific data were supplemented with geologic data from EEI's nearby landfill facility and published regional data to develop a conceptual model of geology and groundwater flow at the CCP impoundments. Site specific data were collected at seven monitoring wells (G101, G111, G112B, G113, G151, G152, and G153) installed in June 2010. Groundwater samples were collected from these monitoring wells for nine consecutive quarters from August 2010 through August 2012 to establish a statistical baseline for groundwater quality. Monitoring wells G112B and G153 were subsequently determined to be returning groundwater samples that were not representative of the uppermost water bearing formation beneath the CCP impoundments, and were abandoned and replaced with G112C and G152B in January 2013. Two additional quarters of groundwater quality samples were collected from the remaining original and new replacement monitoring wells in March and May 2013.

Three hydrostratigraphic units have been identified in the vicinity of the CCP impoundments:

- The uppermost hydrostratigraphic unit is approximately 50 or more feet thick and is composed of the Equality Formation and the underlying Metropolis Formation. These units consist of predominantly clay and silty clay with some minor intervals of sandy clay. This sufficial groundwater unit extends downward to the McNairy Formation, which was not intercepted by any of the borings advanced around the CCP impoundments. The geometric mean hydraulic conductivity of this hydrostratigraphic unit is 5.9 x 10⁻⁶ cm/s, suggesting that it is a confining unit.
- The McNairy Formation is the lowest unlithified unit identified in the vicinity of the CCP impoundments and rests on top bedrock. Based on regional data, the McNairy Formation is typically more permeable than the overlying Equality and Metropolis Formations owing to the larger amount of sand and gravel in that unit. This hydrostratigraphic unit is approximately 85 feet thick in the vicinity of the CCP impoundments.
- The third hydrostratigraphic unit is defined by the uppermost bedrock unit, the Salem Limestone, which is the uppermost bedrock unit underlying the Station, and has a reported thickness of 200 to 500 feet.

Groundwater occurs within the uppermost hydrostratigraphic unit at depths of 2.6 to 42.7 feet, depending on monitoring well location. Groundwater flow beneath the CCP impoundments is conceptually south toward the Ohio River, a regional groundwater sink. The CCP impoundments, particularly the east



impoundment, are close to the Station property boundary and given expected east-west variations in groundwater flow direction, there may be potential for off-site migration in the event of a release.

Potential for Groundwater Receptors

A search of water well records on file with the Illinois State Geological Survey, Illinois State Water Survey, and Illinois Environmental Protection Agency identified 25 water well records within 2,500 feet of the CCP impoundments. Locations were field verified and no buildings or other evidence of water wells were identified at six of these locations, one location on property recently purchased by EEI where the well will soon be abandoned, and nine wells that are not used for potable water supply, leaving nine wells within the search radius that are may be active and used for potable water supply. In addition, the Ft. Massac and Joppa Water Districts were consulted to verify areas surrounding the impoundments serviced by municipal water; LaFarge Corporation, which owns the water wells west of the impoundments, was consulted to verify the location of potable wells on their property; and Trunkline Gas Pumping Station was consulted to verify the status of wells on their property.

The well search identified no potable water supply wells within 2,500 feet of either CCP impoundment in a position likely to be downgradient. The closest active water supply wells to the CCP impoundments are non-potable, belong to EEI, and are used for plant process water. The closest community water supply well is in the village of Joppa, approximately 3,000 feet to the southeast. Water quality data for this well shows no evidence of impacts from the CCP impoundments.

Groundwater Chemistry

Groundwater monitored in the uppermost hydrostratigraphic unit at the CCP impoundments is classified as Class II because these materials are composed of silt and clay with hydraulic conductivity lower than 1×10^4 cm/s. Excluding the August 2010 sample event, which was bailed and produced anomalous samples that were not representative of groundwater quality as indicated by all subsequent samples, exceedances of Class II groundwater quality standards were identified for two constituents at three monitoring wells:

- pH: G113 (1 of 10 samples) and G151 (8 of 8 samples)
- Boron: G112C (3 of 3 samples)

The only Class II groundwater quality standard exceedance potentially related to the CCP impoundments is boron. Boron had three exceedances at well G112C, which is downgradient of the inactive west impoundment, with concentrations of 3.1 to 3.3 mg/L versus a Class II groundwater quality standard of 2 mg/L. In addition, manganese at G112C was high relative to background, although lower than its Class II groundwater quality standard, and may be associated with coal ash leachate. No other constituent at G112C had a concentration that was high relative to background.

The pH values lower than the 6.5 SU standard are not associated with coal ash leachate, which tends to be alkaline. Additionally, boron concentrations at these monitoring wells were at background concentrations (relative to G101), indicating no correlation between pH and the primary coal ash indicator parameter, boron.

Conclusions

The primary conclusion from voluntary monitoring of groundwater at the Joppa Generating Station CCP impoundments is that past operation of the west ash pond has caused a localized exceedance of Class II groundwater quality standards for boron. The west ash pond is no longer in service. There are no exceedances attributed to the east ash pond, which is currently in service. Exceedances of the Class II

standard for pH were also observed, but those exceedances are not related to CCP impoundment operation. Furthermore:

- The impoundments are underlain by more than 50 feet of clay-rich deposits. These clays restrict migration of leachate from the impoundment to surrounding groundwater.
- Groundwater beneath the impoundments is conceptually interpreted to flow south toward the Ohio River.
- The exceedances attributed to former operation of the west ash pond were only observed in monitoring well G112C, immediately south and downgradient of the impoundment.
- Manganese concentrations in G112C are elevated relative to background, although less than 2 percent of the Class II groundwater quality standard, and while these concentrations may be naturally occurring due to a reduced hydrogeologic environment, the west ash pond cannot be ruled out as a source of this manganese.
- A search of water well records indicates that there are no potential receptors downgradient, and potential receptors are unlikely within 2,500 feet sidegradient of the east impoundment. Drinking water in this area is provided by the Joppa and Ft. Massac Water Districts.
- There are no potential receptors directly downgradient of the west impoundment. There are active potable wells sidegradient, and within 2,500 feet of the west impoundment. These wells are used for sinks and showers, but not drinking water supply. The property owner brings in bottled drinking water.
- The Station's non-potable water supply wells are the closest water wells downgradient of the CCP impoundments. Water quality data for the Station wells and the closest community water supply well (3,000 feet sidegradient of the east impoundment) indicate very low boron and sulfate concentrations, indicating no evidence of impacts from the CCP impoundments after more than 50 years of service.



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1 INTRODUCTION

1.1 Purpose

Electric Energy Incorporated (EEI) and Ameren Energy Generating Company own and operate the Joppa Generating Station in Joppa, Illinois (Figure 1). The coal-fired plant currently operates one impoundment for coal combustion product (CCP) management purposes, and has another impoundment that is no longer in service. To assess the potential for constituent migration from the impoundments as requested by the Agency in their correspondence dated April 10, 2009 and a follow-up letter on January 25, 2013, EEI commissioned a hydrogeologic study, water well survey, development of a groundwater monitoring plan, and an initial groundwater quality assessment.

The objectives of this report are to:

- Summarize hydrogeologic information pertinent to the site.
- Evaluate groundwater quality data to determine whether or not operation of the impoundment has adversely affected groundwater.
- Determine the potential for off-site migration and whether or not there are potential groundwater receptors in the event of a release.



2 SETTING

Portions of the information in this section were previously presented and have been modified from the CCP impoundment hydrogeologic assessment plan (October 2009) and the hydrogeologic report for the Station's CCP landfill (June 2009) prepared by Hanson Professional Services, Inc. (Hanson).

2.1 Power Plant and CCP Impoundments

The Joppa Generating Station (Station) is located west of the Village of Joppa and northeast of the Ohio River in Massac County, Illinois. The Station lies in Section 14, Township 15 North, Range 3 East of the 3rd Principal Meridian. The Station has two CCP impoundments, the West Ash Pond located in the east half of Section 15 and the East Ash Pond located in the west half of Section 14 directly north of the power plant (Figure 2)

During initial operation of the plant, coal ash was impounded within the levees formed by the construction of the Station railroad loop. The East Ash Pond was later constructed inside the railroad loop.

The West Ash Pond (WAP), encompassing approximately 84 acres, was used from the early 1950's until it was removed from service in the 1970's. The base elevation of the WAP is reportedly 320 feet above mean sea level (amsl). The elevation of the top of the CCP within the impoundment ranges from approximately 362 feet amsl towards the south end to 370 feet amsl at the northern tip, although most of the WAP lies at an elevation of 362 feet amsl. The height of the WAP is approximately 22 feet relative to surrounding grade.

The East Ash Pond (EAP), encompassing approximately 103 acres, was built in two stages. The northern portion (Phase I) was placed into service in late 1973. The southern portion (Phase II) was permitted in May 1985 with completion of construction activities in late 1985. The elevation of the top of the CCP within Phase I of the impoundment ranges from approximately 372 to 380 feet amsl, although most of the CCP lies between 372 and 374 feet amsl. The elevation of CCP within Phase II of the impoundment ranges from approximately 372 to 380 feet amsl, although most of the ranges from approximately 351 to 363 feet amsl, with most of the CCP between 352 and 356 feet amsl. The height of the EAP is approximately 55 feet relative to surrounding grade. The EAP is currently operated in accordance with IEPA NPDES Permit No. IL0004171.

2.2 Regional Geology

The Station lies at the southern boundary of the Illinois Basin and the northern edge of the Mississippi Embayment, a relatively low lying area that is part of the Coast Plain Physiographic Province (Figure 3)



(Leighton, 1948). Based on stack-unit maps prepared by the Illinois State Geological Survey (Berg and Kempton, 1987) the vicinity of the Station generally has less than 6 meters (<19.7 feet) of silty and clayey diamictons overlying Cretaceous age sediments, silts, sands, etc. between depths of 6 to 15 meters (19 to 50 feet). However, in some areas along the Ohio River, the predominant unlithified materials are Quaternary age sand and gravel outwash deposits belonging to the Henry Formation. The unlithified materials rest on Mississippian age bedrock.

2.2.1 Unlithified Materials

Regionally, unlithified materials consist of diamictons and lacustrine/alluvial deposits. These deposits may exceed 100 feet in thickness. Several deep boring logs within the property boundary of the Station have thicknesses of unlithified materials ranging from 135 to 142 feet. Four principal unlithified deposits exist in the vicinity of the Station: (1) the Equality Formation; (2) Peoria Silt / Roxana Silt / Loveland Silt; (3) Metropolis Formation; and (4) McNairy Formation (Figure 4).

The Equality Formation is the uppermost material encountered in the vicinity of the Station. The Equality Formation consists of silt, clay, and minor amounts of sand and gravel. The silt and clay are medium to dark gray to brown; less commonly they are greenish to bluish gray. Some reddish to orange-brown layers occur in the upper part of the unit. Consistency varies from stiff to soft, plastic "gumbo." Structure varies from massive to finely laminated or varved. Wood fragments and decomposed vegetation are common. This formation is interpreted as fine-grained fluvial overbank sediments and slack-water lacustrine deposits that accumulated during the Wisconsinan age (Nelson, 2007). Based on seventeen borings advanced as part of a subsurface geologic investigation for the landfill approximately ¼ to 1 mile northwest of the WAP (Hanson, 2009a), the thickness of the Equality Formation ranges from 14 to 32 feet.

Contiguous with the Equality Formation are the Peoria Silt, Roxana Silt, and Loveland Silt (these silts are not shown on regional maps of this area, but have been encountered in soil borings in the vicinity of the Station). The Peoria Silt and Roxana Silt are both wind-blown (eolian) deposits of Wisconsinan age that are difficult to distinguish from one another. Their lower contacts are gradational. The Peoria Silt is a massive, slightly clayey silt with rare fine sand grains. The upper part is generally yellowish brown to dark brown, grading downward to mottled gray and yellowish brown. The Roxana Silt is medium dark brown to reddish brown that typically has uniform color with no mottling and higher clay content than the Peoria Silt. The Loveland Silt is of Illinoian age and is a massive silt, interpreted as an eolian deposit, with high clay content. The Loveland is strongly mottled in yellow, red, and orange and has prominent vertical gray streaks. It is strongly weathered and commonly displays root casts or traces. The Loveland is generally thin and lenticular and its lower contact is gradational to the Metropolis Formation but unconformable to older units.

Underlying the Equality Formation, or at some locations the Loveland Silt, is the Metropolis Formation, which consists of silt, sand, clay, and gravel. The Metropolis is composed of silty sand and sandy silt in a clay matrix and contains scattered pebbles and lenses of gravel. Much of the unit may be classified as diamicton. These sediments are strongly mottled and streaked in shades of gray, yellowish brown, and yellowish orange. The lower part of the formation contains bright red and orange sand. Sediments are poorly sorted to unsorted and massive to weakly stratified. Gravel occurs as common scattered pebbles and as lenses up to 4 feet thick (Nelson, 2007). The Metropolis Formation, originally defined by Nelson et al. (1999a), borders the Ohio River, where it underlies a loess-capped terrace. The Metropolis Formation is interpreted as alluvial sediment deposited in the valley of the ancestral Tennessee River (Nelson et al. 1999a, 1999b). The lower contact is unconformable on the McNairy Formation in most places. Age is Pleistocene, Illinoian, and older. Based on thirteen borings advanced approximately ¼ to 1 mile northwest of the WAP (Hanson, 2009a) the thickness of the Metropolis Formation ranges from 25 to 40 feet. A drillers log for plant well 4, located south of the EAP, indicates fine-grained deposits from the land surface to a depth of 50 feet. These deposits represent the combined thickness of the Equality and Metropolis Formations south of the CCP impoundments.

The lowermost unlithified unit encountered in the vicinity of the Station is the McNairy Formation, which consists of sands, silts, and clays. The McNairy is Upper Cretaceous in age and consists of very fine- to medium-grained sand, mostly highly micaceous, and ranges from white and light-gray to bright orange, red and yellow in color. The silts and clays are light to dark gray and may be mottled in yellow, gray, and magenta. The lower contact is unconformable (Nelson, 2007). Based on a boring advanced to bedrock by Hanson (2009a) approximately 0.7 miles mile northwest of the WAP, the thickness of the McNairy is approximately 76 feet. The drillers log for plant well 4 indicates sand from a depth of 50 to 135 feet, suggesting that the McNairy formation is 85 feet thick south of the CCP impoundments.

Thick outwash deposits of the Wisconsinan aged Henry Formation may be encountered within the Ohio River Valley. These deposits, which are not present beneath the CCP impoundments, consist of sorted and stratified water-laid material that is predominantly sand and gravel.

2.2.2 Bedrock

Bedrock in the region surrounding the Station consists of a sequence of Mississippian System sedimentary rocks hundreds of feet thick and consolidated prior to the Cretaceous Period. The bedrock dips gently northward toward the center of the Illinois Basin. The upper-most bedrock unit near the Station generally consists of limestone. The total thickness of the Mississippian System in southern Illinois is greater than 3,200 ft (Willman et al., 1975).

The uppermost unit encountered in the vicinity of the Station is the Salem Limestone. The Salem Limestone is described as fine-grained, fossiliferous limestone, and is approximately 200 to 500 feet thick

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in the area. The Salem Limestone overlies the Ullin Limestone; the Ullin Limestone is described as a light-colored fine- to coarse-grained limestone. The overall thickness of the Ullin Limestone near the Station is approximately 200 feet. The Fort Payne Formation, which is overlain by the Ullin Limestone, is described as a very fine-grained, siliceous, cherty limestone, and is approximately 200 to 600 feet thick in the study area (Kolata, 2005; Willman et al., 1967; Willman et al., 1975).

2.3 Water Resources

2.3.1 Surface Water

The major surface water body in the vicinity of the Station is the Ohio River, which borders the entire Station property to the south. The southern edges of the WAP and EAP are approximately 1,500 and 2,100 feet from the north bank of the Ohio River, respectively, during normal flow. The primary drainage in the area of the WAP is an intermittent stream that runs parallel to the east side of the impoundment and runs south initially and then south-southwest to the Ohio River. The primary drainage in the vicinity of the EAP is a stream that begins between the east portion of impoundment and the railroad loop and runs approximately 1,000 feet south from a culvert beneath the railroad loop before turning to the south-southwest to the Ohio River. This stream conveys discharge water from the EAP.

2.3.2 Groundwater

No surficial aquifers, i.e., aquifers that are present or exposed at the ground surface, are present in the vicinity of the ash impoundments. Berg, Kempton and Cartwright (1984) classified the area as D2 - uniform, relatively impermeable silty or clayey till at least 20 feet thick with no evidence of interbedded sand and gravel. Aquifers in the area of the Station generally fall into two broad categories: (1) intermittent sand and gravel deposits within the McNairy Formation; and, (2) bedrock consisting of limestone and fractured limestone, which vary widely in transmissivity.

No known wells in the area utilize the deposits of the Equality or Metropolis Formation for groundwater. These formations predominantly consist of silt and clay with isolated lenses of sand and gravel, which do not yield large amounts of water. Most wells in the area obtain groundwater from the McNairy sand and gravels or Mississippian limestone, principally the Salem or Ullin Limestones.

2.3.3 Well Search

Public records were searched to identify water wells located within 2,500 feet of the CCP impoundments. The Station Property is located in Township 15 South, Range 3 East, and the CCP impoundments are located within Sections 14 and 15. The 2,500 foot search radius spans across Sections 10, 11, 14, 15,





22, and 23. All water supply wells within these sections are shown on Figure 5 and tabulated in Appendix A.

The following sources of information were queried to identify water well locations and locations near the Station serviced by public water supplies:

- Illinois State Geological Survey's Illinois Water Well (ILWATER) Internet Map Service
- Illinois State Water Survey Domestic Well Database (ISWS)
- Illinois EPA's web-based Geographic Information System (GIS) files
- Illinois Department of Public Health
- Massac County Health Department
- The Joppa Water District
- The Ft. Massac Water District
- LaFarge Corporation, located immediately west of the Station
- Trunkline Gas Pumping Station, located north of the west ash pond

Records were identified for 68 wells within the six sections surrounding the unlined ash ponds. Twenty of the 68 wells were identified as monitoring wells associated with the Station's landfill. In addition, 9 wells on the LaFarge property west of the power plant were identified as test holes rather than water wells. These 29 wells are not shown on Figure 5 but are listed in Appendix A, Table A-1. The remaining wells are current or former water wells listed for industrial/commercial use or farm/domestic use.

A follow-up field survey was performed to visually verify the locations of water wells within the search radius (Appendix A). During this survey, personnel from the Joppa and Ft. Massac Water Districts were consulted to identify locations served by these districts. This survey identified:

- Eight records with incorrect coordinates. New coordinates were obtained using a hand-held GPS unit, and the locations on Figure 5 reflect the corrected coordinates.
- One well (79) that did not appear in the well records search. This well was added to Table A-1 and Figure 5.
- Six locations where no building and no wells could be located. These locations either represent water well records that have incorrect locations listed in the database or were associated with buildings that were abandoned and torn down. These locations are shown in grey on Figure 5.
- One well on property recently purchased by EEI where the building has been removed and the well will be abandoned. This location is also shown in grey on Figure 5.

In addition, the Station wells (including Midwest Electric Power) and Trunkline Gas Pumping Station wells are shown in grey on Figure 5 because they were verified to be non-potable. The Station wells are used



only for production water, and the Trunkline Gas Pumping Station wells are not active. Both facilities obtain potable water from the Ft. Massac Water District.

Based on information derived from the well search, there are 25 water wells within a 2,500 foot radius of the two CCP impoundments, nine of which may be active and used for potable water (Figure 5). The water wells range from 52 to 451 feet in depth, with an average depth of 189 feet and a median depth of 158 feet. Of the eight water wells within the search radius with sufficient data to indicate the primary water-bearing zone supplying the well, three are in sand and gravel deposits and five are in limestone.

The closest active water supply wells to the EAP are wells 7 and 8, which are Station wells completed at depths of 350 and 403 feet. These wells supply production water, but are not used for potable water supply. The four active Station wells were sampled in February 2013 for analysis of coal ash indicator constituents, boron and sulfate. Boron concentrations in all four wells were <0.10 mg/L and sulfate concentrations were 6 mg/L (Appendix A). These low concentrations demonstrate that groundwater withdrawn from the Station's water wells is not affected by any release from the CCP impoundments.

There are no active potable wells downgradient of the EAP. The only potentially active potable well within 2,500 feet of the EAP that is not upgradient is well 3, which is sidegradient. This well is not considered a potential receptor because it is sidegradient, rather than downgradient of the EAP and is in an area served by the Joppa Water District.

There are no water wells directly downgradient of the WAP. The closest wells to the WAP are wells 49 and 50. These wells are non-potable and supply production water to the combustion gas turbines at the Station. There are two industrial wells (wells 20 and 75) associated with the LaFarge cement plant immediately west of the Station that are sidegradient of the WAP. The cement plant uses bottled drinking water, while well water is used in sinks and shower facilities as well as for production. The closest of these wells is more than 2,400 feet from the WAP.

Based on state records, there is one community water supply (CWS) well in the sections surrounding the CCP impoundments, but outside the 2,500 foot search radius. Well number 51 on Figure 5 and in Appendix A, Table A-1 is located in the village of Joppa in Section 23, 3,000 feet east of the Station property boundary. According to the IEPA database, CWS well 51 has a minimum setback zone of 200 feet, and a Phase I Wellhead Protection Area (WHPA) of 1,000 ft. The western edge of the WHPA falls within the 2,500 foot search radius. On-line water quality data available for this well¹ indicate low boron (<0.010 to 0.044 mg/L) and sulfate (<10 to 25 mg/L) concentrations, demonstrating that groundwater withdrawn by these wells has not been affected by any release from the CCP impoundments.



¹ http://163.191.83.31/dww/JSP/WaterSystemDetail.jsp?tinwsys_is_number=717415&tirwsys_st_code=IL&wsnumber=IL1270100

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3 MONITORING WELL INSTALLATION, DEVELOPMENT, AND SAMPLING

3.1 Monitoring Well Installation and Development

Seven monitoring wells (G101, G111, G112B, G113, G151, G152, and G153) were installed between June 1 and 25, 2010 (Table 1, Figure 1) by Geotechnology, Inc. (Geotechnology, 2010). At each well location, subsurface borings were advanced with a rotary drill rig equipped with hollow-stem augers to facilitate soil classification. Soil was continuously sampled through the center of the hollow stem auger. Monitoring wells, constructed of 2" inside diameter schedule 40 PVC riser and screen, with steel above-ground well covers, were installed at each location to monitor groundwater within the uppermost water-bearing unit adjacent to the impoundments. All of the monitoring wells were screened within one or more of the following unlithified materials: silty clay, silty/sandy clay, clay or silt. The wells were constructed consistent with monitoring well construction standards per 35 IAC 811.318. Drilling and sampling equipment was decontaminated before sampling and between sample locations to prevent cross contamination. The monitoring wells were surveyed by a licensed surveyor.

In a November 7, 2012 meeting between the Illinois Environmental Protection Agency (IEPA) and EEI, it was proposed by EEI that monitoring wells G112B and G152 be relocated because they were installed beneath fill materials that appeared to be impacting analytical results. Subsequent to that meeting and with the IEPA's approval, wells G112B and G152 were replaced by new monitoring wells G112C and G152B in January 2013 by Natural Resource Technology, Inc. (NRT). The original monitoring wells, G112B and G152 were properly sealed and abandoned at that time.

Monitoring well construction, survey data, and screened formation are summarized in Table 1. Boring logs and well diagrams are included in Appendix B. In addition, copies of the monitoring well sealing forms submitted to the Illinois Department of Public Health are also in Appendix B. Boring depths for the original seven monitoring wells and two replacement wells were between 25 and 50 feet bgs. A cross-sectional view of the seven current monitoring wells showing ground surface and well screen elevations is provided in Figure 6.

Following installation, the initial seven monitoring wells were developed in June 2010 by surging and pumping a minimum of five well volumes and until specific conductivity stabilized. The depth to groundwater was measured in each monitoring well using an electronic water level indicator. The two replacement wells (i.e., G112C and G152B) were developed on February 7, 2013. Groundwater levels and elevations at all of the monitoring wells at the EAP and WAP impoundments from August 2010 through May 2013 are provided in Table 2.



MONITORING WELL INSTALLATION, DEVELOPMENT, AND SAMPLING

3.2 Groundwater Sampling and Chemical Analysis

The seven monitoring wells installed in June 2010 were sampled during nine consecutive quarterly monitoring events from August 2010 through August 2012 to establish a statistical baseline for groundwater quality. The monitoring wells were purged and sampled for the first quarterly sampling event on August 17, 2010 using disposable bailers; purging and sampling of wells in subsequent events was through low-flow sampling methods with dedicated bladder pumps. Groundwater levels measured in the seven wells for the first monitoring event ranged from 5.46 to 42.68 feet bgs (Table 2).

During the first monitoring event each well was purged until three well volumes were removed. Water quality parameters including pH, specific conductivity, and temperature were monitored in the field. In subsequent monitoring events, starting with the 4th Quarter event in November 2010, the wells were purged until the field parameters stabilized.

Following the completion of baseline sampling in the 3rd Quarter 2012, evaluation of the initial groundwater quality, and approval of the revised monitoring plan by IEPA, monitoring wells G112B and G152 were abandoned and replaced by wells G112C and G152B. Groundwater sampling of the modified monitoring well network was conducted in the 1st and 2nd Quarters of 2013 for inclusion with this hydrogeologic assessment.

Water samples were field filtered for dissolved constituents, unfiltered for totals, and preserved as required for each constituent. Sample containers were labeled, placed in an ice-filled cooler, and transported using standard chain-of-custody procedures. All groundwater sampling events from August 2010 through May 2013 were conducted by Geotechnology, Inc. and sample analyses conducted by Teklab, Inc., located in Collinsville, Illinois. The initial groundwater sampling information and laboratory analytical reports are provided in the Geotechnology, Inc. monitoring report dated October 19, 2010 (Geotechnology, 2010). The groundwater sampling reports for the 1st and 2nd Quarters of 2013 are found in the groundwater monitoring reports by Geotechnology dated March 25 and May 23, 2013, respectively.

All eleven quarters of groundwater samples were analyzed for the inorganic parameters listed under 35 IAC 620.410 with the exception of radium 226/228.² Table 3 lists the field, general chemistry, and metal parameters monitored along with the analytical methods.



² Perchlorate and vanadium were added to 35 IAC 620.410 on October 5, 2012, after the groundwater monitoring plan for this site was approved, and therefore were not monitored.

4 SITE HYDROGEOLOGY

4.1 Lithology

The information used to describe site hydrogeology is based on the local geology obtained from published sources as presented in Section 2, supplemented with the boring data collected at the seven current monitoring well locations G101, G111, G112C, G113, G151, G152B, and G153. These seven borings ranged from 25 to 50 feet bgs. The upper portion of two other borings (G112B and G152) were determined to be through fill materials that included some coal and an unknown amount of fly ash. The monitoring wells installed within these two borings were abandoned in January 2013 and replaced by nearby wells G112C and G152B, so the lithology data from the earlier well locations is not included in the following discussion.

Other than an 8.5 foot thick silt layer intercepted at boring G152B at a depth of 4 to 12.5 feet bgs, all geologic materials below the top few feet were logged as clay, silty clay, clayey silt, and sandy clay. Out of a total of 296 feet of unlithified materials logged in the seven borings, the following percentages of materials were described:

- 1.0% fill material at the surface, described generically as "Fill" or gravel, and intercepted at well locations G113 and G151
- 3.5% silt or clayey silt, intercepted at depths of 4.5 to 12.5 feet at well G152B and 38 to 40 feet at well G153
- 5.0% sandy clay, intercepted at depths of 32 to 36 feet at well G113, 36 to 42 feet at well G151, and 32 to 38 feet at well G153
- 90.5% clay and silty clay, intercepted through most of the logged depths of all monitoring well locations at both the EAP and WAP

Bedrock was not encountered in the borings for any of the monitoring wells installed around the EAP or WAP, but limestone bedrock was intercepted as part of another study, approximately 3,500 feet northwest of the WAP, at 142 feet bgs (227 feet amsl), and at a depth of 135 feet bgs (~210 feet amsl) at plant well 4, which is 900 feet south of the EAP. The lowest elevation drilled during the hydrogeologic characterization around the two impoundments was at well G112C, which extended to 299 feet amsl.

The uppermost hydrostratigraphic unit encountered by the monitoring wells installed around the two impoundments is composed of the Equality Formation and the underlying Metropolis Formation (Figure 4), which both consist of predominantly clay and silty clay with some minor intervals of sandy clay. This Surficial Groundwater Unit (i.e., Upper Groundwater Unit) extends downward to the McNairy Formation, which was not intercepted by any of the borings advanced around the EAP and WAP.



The McNairy Formation (i.e., Lower Groundwater Unit) is the lowest unlithified unit identified in the vicinity of the Station and rests on top bedrock. Based on regional data, the McNairy Formation is typically more permeable than the overlying Equality and Metropolis Formations owing to the larger amount of sand and gravel in that unit. The McNairy Formation would be considered the second hydrostratigraphic unit at the Station. The third hydrostratigraphic unit is defined by the uppermost bedrock unit, the Salem Limestone, which is the uppermost bedrock unit underlying the Station.

4.2 Groundwater Flow

Groundwater elevation data (potentiometric levels) were collected from the monitoring wells installed within the uppermost water-bearing unit surrounding the CCP impoundments. Groundwater depths and elevations for the eleven quarterly monitoring events are provided on Table 2 and graphically illustrated in time-series plots on Figure 7 (note: only three and two sample events have been recorded for replacement monitoring wells G112C and G152B, respectively). Groundwater levels were the closest to ground surface at the three wells adjacent to the WAP (G111, G112C, and G113), with water levels for the period of August 2010 through May 2013 ranging from 2.64 to 16.65 feet bgs. Groundwater levels were deepest at the three wells adjacent to the EAP (G151, G152B, and G153), with water levels ranging from 17.08 to 42.70 feet bgs.

Groundwater conceptually flows north to south from topographically higher areas at the north end of the site toward the Ohio River which is topographically lower than the rest of the site and a regional discharge point for groundwater. Topographically upgradient from both the EAP and WAP is monitoring well G101, which is conceptually upgradient of the CCP impoundments. However, groundwater elevations in well G101 were lower than all other monitoring wells during two quarters (February 2012 and May 2013) and were the second lowest of all the wells in the remaining nine quarters (Figure 7). Similarly, G151 and G153 have lower groundwater elevations than G152B which is topographically lower than those wells. This appears to be counter-intuitive given that well G152B is further south and conceptually downgradient from the rest of the wells at the EAP. There are no known high capacity wells north of the station that could explain the groundwater elevations observed in G101 (Section 2.3.3).

Based on the lack of correlation between topography and groundwater elevations, and given that the wells are all screened clay that has very low hydraulic conductivity, it is apparent that the measured groundwater elevations are not reflective of groundwater flow patterns in the upper hydrostratigraphic unit in the vicinity of the EAP. Therefore, groundwater elevation measurements from wells G101, G151, and G153 were not included in the development of the potentiometric surface map in the area of the EAP (Figure 8).





Conversely, the three wells adjacent to the WAP (G111, G113, and G112C) appear to have a consistent correlation between topographic and groundwater elevations. Groundwater elevations are highest in the topographically upgradient well G111, which is located west of the central portion of the WAP, and lowest at the topographically downgradient well G112C, located to the south of the impoundment. Therefore, a potentiometric surface map was prepared for the 2nd Quarter 2013 utilizing the three monitoring wells adjacent to the WAP and well G152B south of the EAP (Figure 8) but excluding the non-representative groundwater elevations at background well G101 and the EAP wells G151 and G153. As seen on the map, groundwater flow in the vicinity of the WAP is south-southwest at a gradient of approximately 0.014 ft/ft.

The conceptual model for groundwater flow beneath both impoundments is southwest towards the Ohio River, with baseflow discharge from the unlithified deposits to the river during most of the year, as conceptualized in Figure 9. Given the close proximity of the CCP impoundments, particularly the EAP, to the Station property boundary and expected east-west variations in groundwater flow direction, there may be potential for off-site migration in the event of a release.

4.3 Potential for Groundwater Receptors

A potential groundwater receptor is a potable water supply well located in a position that can be interpreted as downgradient from the CCP impoundment, and screened within a geologic formation that can reasonably be expected to be a groundwater migration pathway in the event of a release.

As described in Section 2.3.3, Figure 5 shows water wells located within the vicinity of the CCP impoundments. The Station and areas within 2,500 feet both east and west of the CCP impoundments obtain drinking water from the Joppa or Ft. Massac Water Districts; although, the LaFarge cement plant to the west reportedly uses well water for sinks and showering, so these wells would be considered potable. The closest cement plant well is slightly less than 2,500 feet west of the WAP. The only downgradient water supply wells are on the Station property; however, these wells are not potable. Water quality data from these wells shows no evidence of impacts from the CCP impoundments. The closest CWS well is in the village of Joppa, approximately 3,000 feet southeast of the EAP. Water quality data for this well shows no evidence of impacts from the CCP impoundment.



5 GROUNDWATER CHEMISTRY

5.1 Overview

The purpose of the sampling and inorganic analysis of groundwater from monitoring wells at the Station was to assess background and downgradient groundwater quality; to evaluate elevated concentrations and those exceeding groundwater standards; and to identify primary factors potentially influencing groundwater quality changes spatially and temporally.

All of the groundwater quality data collected and analyzed for both field and laboratory parameters, including the full list of inorganic constituents listed in 35 IAC 620.410 except for radium 224/226,³ are listed in Appendix C for the 11 quarters of monitoring conducted from August 2010 through May 2013. A statistical summary of all of the water quality data at each active monitoring well, including the mean, median, maximum, minimum, standard deviation, and percent non-detects, is provided in Table 4 for the period of November 2010 through May 2013. The first quarterly monitoring event (conducted in August 2010) is not included in the statistical analysis since the wells were purged and sampled using bailers, as opposed to low-flow sampling methods with dedicated bladder pumps in the subsequent 10 events. In addition, monitoring wells G112B and G152 were not included in the statistical analysis or the discussion that follows because groundwater quality in these monitoring wells was affected by the overlying fill materials, and they were subsequently replaced by G112C and G152B.

5.2 Groundwater Classification

As set forth in 35 IAC 620, any geologic material with a hydraulic conductivity of less than 1×10^{-4} cm/sec, and which does not meet the provisions of Section 620.210 (Class I), Section 620.230 (Class III), or Section 620.240 (Class IV), meets the definition of a Class II – General Resource Groundwater. Based on the hydrogeologic information provided below, groundwater within the shallow (<50 feet bgs) unlithified materials in which the monitoring wells are screened is classified as Class II groundwater and the groundwater quality standards set forth in 35 IAC 620.420 are the applicable groundwater quality standards.

Specifically, groundwater monitored at the CCP impoundments is from the clay, silt, and silty clay of the Equality Formation, Peoria/Roxana/Loveland Silts, or the Metropolis Formation, and does not qualify as Class I groundwater because:



³ Perchlorate and vanadium were added to 35 IAC 620.410 on October 5, 2012, after the groundwater monitoring plan for this site was approved, and therefore were not monitored.

- The CCP impoundments are not within the minimum setback zone of a well which serves as a potable water supply.
- The monitoring wells are screened in clay and silty clay rather than unconsolidated sand, gravel, or sand and gravel which is 5 feet or more in thickness and that contains 12 percent or less of fines.
- The monitoring wells are not screened in a sandstone which is 10 feet or more in thickness, nor are they screened in fractured carbonate which is 15 feet or more in thickness.
- Hydraulic conductivity was tested in 2010 (Geotechnology, 2010), and ranges from 1.1x10⁻⁶ to 7.6x10⁻⁵ cm/s (see table below). The geometric mean hydraulic conductivity for the screened intervals of the monitoring wells is 5.9x10⁻⁶ cm/s.

Monitoring Well	Hydraulic Conductivity (cm/sec)
G101	5.6E-06
G111	1.5E-05
G112B	1.1E-06
G113	6.1E-06
G151	3.1E-06
G152	7.6E-05
G153	1.9E-06
Geometric Mean	5.9E-06

Since shallow groundwater in the uppermost water-bearing unit meets the classification criteria of a Class II (General Resource) groundwater, groundwater quality monitored at the EAP and WAP was compared to the Class II groundwater standards.

5.3 Comparison of Groundwater Quality to Class II Standards

Constituents with exceedances of Class II groundwater quality standards between November 2010 and May 2013 are:

- pH: G113 (1 of 10 samples) and G151 (8 of 8 samples); and
- Boron: G112C (3 of 3 samples).

The only exceedance potentially related to the CCP impoundments is boron. Boron had three exceedances at well G112C during the three monitoring events conducted in the first two quarters of 2013, with concentrations of 3.1 to 3.3 mg/L versus a Class II groundwater quality standard of 2 mg/L.

The pH values lower than the 6.5 SU standard at wells G113 and G151 are not associated with coal ash leachate, which tends to be alkaline. Additionally, the boron concentrations at both these wells were at



background concentrations (relative to G101), indicating no correlation between pH and the primary coal ash indicator parameter, boron.

5.4 Groundwater Quality Analysis

5.4.1 Primary Coal Ash Leachate Indicators

Boron and sulfate are the primary indicator constituents for coal ash leachate. Median boron concentrations in groundwater at the CCP impoundments were mostly lower than the laboratory reporting limit of 0.02 mg/L at all monitoring wells except G112C, located south of the WAP. Only 3 of 46 samples contained boron concentrations above the laboratory reporting limit at the six monitoring wells (other than G112C) collected during ten quarterly monitoring events from November 2010 through May 2013. Those three boron concentrations reported by the laboratory were less than 3 percent of the Class II groundwater quality standard of 2 mg/L.

Median sulfate concentrations were similar to background (as monitored at G101) at G111, G113, and G152B. The highest median sulfate concentrations of 103 and 104 mg/L were observed at wells G151 and G153, respectively, and the highest individual sulfate concentrations (111 mg/L in both instances) were also observed at these wells. All sulfate concentrations observed in groundwater were less than one-third of the Class II groundwater standard.

and the second	Median Co	ncentration
Well No.	Boron mg/L	Sulfate mg/L
G101	<0.02	33
G111	<0.02	24
G112C	3.1	63
G113	<0.02	35
G151	<0.02	103
G152B	<0.02	17
G153	<0.02	104
IL Class II Standard	2.0	400

There is no correlation between boron and sulfate concentrations, suggesting that the sulfate concentrations are not related to the boron concentrations. The CCP impoundments are the only likely source of boron in the area, while sulfate has other potential sources. This lack of correlation suggests that boron is the better indicator constituent for the Station's CCP impoundments than sulfate.



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Boron and sulfate concentrations were stable during the 2½ year monitoring period, with neither parameter increasing or decreasing significantly. Graphs of boron and sulfate trends are shown below. Most boron concentrations were below the detection limit, with the exception of well G112C where the three samples had similar concentration and no discernible increasing or decreasing trend. Sulfate concentration trends were flat for all monitoring wells.



Graph showing boron concentration versus time. Non-detects are plotted as zero values.



Graph showing sulfate concentrations versus time.



5.4.2 Other Constituents Potentially Impacted by Coal Ash Leachate

Median iron and manganese concentrations were higher in samples from monitoring well G112C than in samples from the other monitoring wells at the Station. G112C also had relatively high boron concentrations that suggest potential for a release from the WAP. However, iron and manganese are sensitive to redox conditions, and exhibit a tendency to have relatively high naturally occurring concentration in reduced hydrogeologic environments.

	Median Co	oncentration
Well No.	Iron mg/L	Manganese mg/L
G101	0.020	< 0.005
G111	<0.020	<0.005
G112C	0.039	0.17
G113	<0.020	<0.005
G151	<0.020	0.027
G152B	<0.020	0.010
G153	0.021	< 0.005
IL Class II Standard	5.0	10

Iron concentrations from individual samples in G112C were not high relative to iron concentrations detected in other monitoring wells (see graph below). The median concentration appears relatively high because iron was detected in two of the three samples from G112C, while it was detected in half or fewer of the samples from the other monitoring wells—causing the median value for the other wells to be the reporting limit. The low boron concentrations at the other monitoring wells indicate that iron observed in those wells is not associated with a release from the CCP impoundments, meaning it is likely naturally occurring. Therefore, the iron concentrations at G112C, which are lower than naturally occurring iron concentrations in the other monitoring wells and less than 1 percent of the Class II standard, may also be naturally occurring.



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Graph showing iron concentrations vs time. Non-detects are plotted as zero values.

Manganese concentrations in G112C were higher than in the other wells. Given the close proximity of this monitoring well to the Ohio River, where reducing conditions are expected, it is possible that the manganese is naturally occurring; however, the WAP cannot be ruled out as a potential source for the manganese observed in this monitoring well because the concentrations are higher than observed in any other monitoring well, although less than 2 percent of the Class II groundwater quality standard.







5.4.3 Constituents with Elevated Concentrations Due to Causes Other than Coal Ash Leachate

Barium, chloride, fluoride, and TDS had median concentrations in some downgradient monitoring wells that were higher than the median concentrations in background monitoring well G101. In addition, pH in G151 was low relative to the other monitoring wells. There were no exceedances of Class II groundwater quality standards for barium, chloride, fluoride, and TDS; while pH in G151 (and one sample from G113) was lower than the Class II range. Concentrations in G111, G113, G151, G152B, and G153 are not attributed to coal ash leachate because coal ash indicator concentrations in these monitoring wells are low. The concentrations of barium, chloride, fluoride, TDS, and pH in G112C are not attributed to coal ash leachate because they fall within the range of concentrations observed in the other wells, which are not attributed to a coal ash leachate source.

			Median Con	centration	
Well No.	Barium mg/L	Chloride mg/L	Fluoride mg/L	TDS mg/L	pH SU
G101	0.074	4.5	0.29	245	6.97
G111	0.16	6.0	0.67	363	7.09
G112C	0.062	<5.0	0.80	432	6.79
G113	0.50	29	0.43	590	6.57
G151	0.083	5.0	<0.10	248	6.01
G152B	0.51	49	0.59	483	6.81
G153	0.24	21	0.82	433	6.93
IL Class II Standard	2.0	200	4.0	1,200	6.5/9.0



2.0 Barium 1.5 -G101 Concentration (mg/L) - GI11 - G112C →- G113 G151 ----- G152B -G153 0.5 - - Class II Standard 12 0.0 Nov-10 Feb-11 May-11 Aug-11 Nov-11 Feb-12 Feb-13 May-12 Aug-12 Nov-12 May-13

Graph showing barium concentrations vs time.



Graph showing chloride concentrations vs time. Non-detects are plotted as zero values.



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Graph showing fluoride concentrations vs time. Non-detects are plotted as zero values.



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GROUNDWATER CHEMISTRY

GROUNDWATER CHEMISTRY



Graph showing pH values vs time.

5.4.4 Constituents with Concentrations Near or Below Background

The median nitrate concentration in background monitoring well G101 was higher than the other monitoring wells, indicating that observed nitrate concentrations are due to a source other than the CCP impoundments. The likely nitrate source is agricultural activity immediately north of this monitoring location.

	Median Concentration
Well No.	Nitrate mg/L
G101	1.5
G111	0.12
G112C	<0.05
G113	0.44
G151	1.1
G152B	0.84
G153	0.28
IL Class II Standard	100



Nitrate 100.0 90.0 80.0 - G101 70.0 (mg/L) - G111 60.0 61120 Concentration -G113 50.0 G151 40.0 G152B 30.0 G153 - Class II Standard 20.0 10.0 0.0 -Nov-10 Feb-11 May-11 Aug-11 Nov-11 Feb-12 May-12 Aug-12 Nov-12 Feb-13 May-13

5.4.5 Constituents That Were Infrequently or Not Detected

Antimony, arsenic, beryllium, cadmium, chromium, cobalt, cyanide, lead, mercury, nickel, selenium, silver, and thallium were below their respective reporting limits in all seven monitoring wells during all ten guarterly monitoring events conducted from November 2010 through May 2013.

		Copper mg/L	Zinc mg/L
G101	Max	n/a	n/a
	% BDL	100%	100%
G111	Max	n/a	0.018
	% BDL	100%	80%
G112C	Max	n/a	n/a
	% BDL	100%	100%
G113	Max	n/a	n/a
	% BDL	100%	100%
3151	Max	0.011	0.017
	% BDL	87.5%	62.5
G152B	Max	n/a	n/a
	% BDL	100%	100%
G153	Max	n/a	n/a
	% BDL	100%	100%
Illinois Cla	ass II Standard	0.65	10.



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Graph showing nitrate concentrations. Non-detects are plotted as zero values.

GROUNDWATER CHEMISTRY

Copper and zinc had reportable concentrations in one and five samples, respectively, out of 49 possible samples. However, the maximum concentrations of these constituents was more than an order of magnitude lower than the Class II standard.



6 CONCLUSIONS

6.1 Conclusions

The primary conclusion from voluntary monitoring of groundwater at the Joppa Generating Station CCP impoundments is that past operation of the west ash pond has caused a localized exceedance of Class II groundwater quality standards for boron. The west ash pond is no longer in service. There are no exceedances attributed to the east ash pond, which is currently in service. Exceedances of the Class II standard for pH were also observed, but those exceedances are not related to CCP impoundment operation. Furthermore:

- The impoundments are underlain by more than 50 feet of clay-rich deposits. These clays restrict migration of leachate from the impoundment to surrounding groundwater.
- Groundwater beneath the impoundments is conceptually interpreted to flow south toward the Ohio River.
- The exceedances attributed to former operation of the west ash pond were only observed in monitoring well G112C, immediately south and downgradient of the impoundment.
- Manganese concentrations in G112C are elevated relative to background, although less than 2 percent of the Class II groundwater quality standard, and while these concentrations may be naturally occurring due to a reduced hydrogeologic environment, the west ash pond cannot be ruled out as a source of this manganese.
- A search of water well records indicates that there are no potential receptors downgradient, and potential receptors are unlikely within 2,500 feet sidegradient of the east impoundment. Drinking water in this area is provided by the Joppa and Ft. Massac Water Districts.
- There are no potential receptors directly downgradient of the west impoundment. There are active potable wells sidegradient, and within 2,500 feet of the west impoundment. These wells are used for sinks and showers, but not drinking water supply. The property owner brings in bottled drinking water.
- The Station's non-potable water supply wells are the closest water wells downgradient of the CCP impoundments. Water quality data for the Station wells and the closest community water supply well (3,000 feet sidegradient of the east impoundment) indicate very low boron and sulfate concentrations, indicating no evidence of impacts from the CCP impoundments after more than 50 years of service.



7 REFERENCES

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Table 1. Monitoring Well Construction Details

Phase I Hydrogeologic Assessment Joppa Generating Station Electric Energy Inc. Joppa, IL

		Installation Date	Top of Well Riser Elevation	Ground Elevation	Screen Top Depth (BGS)	Screen Bottom Depth (BGS)	Slotted Screen Length	Screen Top Elevation	Screen Bottom Elevation	Bottom of Boring Elevation	Total Boring Depth	Screened Formation
G101	1	06/01/10	363.69	361.12	36.80	46.80	10.00	324.32	314.32	309.1	52.0	Silty Clay
G111	1	06/24/10	359.17	356,63	32.13	42.13	10.00	324.50	314.50	311.6	45.0	Silty Clay
G112C	2	01/29/13	325.82	323.60	15.00	25.00	10.00	298.30	308.60	298.6	25.0	Silty Clay
G113	1	06/25/10	353.04	350.46	30.69	40.69	10.00	319.77	309.77	306.9	43.6	Silty/Sandy Clay
G151	1	06/19/10	363.60	360.90	31.97	41.97	10.00	328.93	318.93	315.9	45.0	Silty/Sandy Clay
G152B	2	01/30/13	347.48	345.20	34.40	44.40	10.00	300.60	310.80	300.7	44.5	Silty Clay
G153	1	06/18/10	354.65	351.73	30.35	40.35	10.00	321.38	311.38	308.1	43.6	Silty/Sandy Clay & Silt
G112B	I.A.	06/20/10	347.62	345.16	32.41	42.41	10.00	312.75	302.75	300.0	45.2	Silty Clay
G152	1.8	06/21/10	351.18	348.55	13.94	23.94	10.00	334.61	324.61	321.7	26.9	Silty Clay

Monitoring Well Number	Northing ³	Easting ³
G101	202,050.25	831,716.43
G111	200,806.11	829,139.79
G112C	198,552.26	829,088.33
G113	199,599.53	830,364.44
G151	200,437.41	832,154.25
G152B	198,547.23	832,358.44
G153	200,067.47	833,979.90
G112B	198,913.55	828,988.60
G152	198,547.23	832,358.44

Notes:

3

A

B

BGS = below ground surface.

All depths are in feet. All elevation measurements are in feet relative to NAVD 1988.

All wells constructed with 2-inch diameter, 10-slot, Schedule 40 PVC screens.

Drilling and well installation by Geotechnology, Inc.

² Drilling and well installation by Natural Resource Technology, Inc.

Coordinates are referenced to Illinois State Plane Coordinates, East Zone - NAD 1983.

Well sealed and abandoned on 1/28/13.

Well sealed and abandoned on 1/29/13.

Table 3. Field and Laboratory Groundwater Monitoring Parameters

Phase I Hydrogeologic Assessment Joppa Generating Station Electric Energy Inc. Joppa, IL

Field Para	meters		Analysis Method
Groundwater Elevation		in-situ	
pH (field)	1	in-situ	SM 21st ed. 4500-H ⁺
Specific Conductance		in-situ	SM 21st ed. 2520-B
Temperature		in-situ	SM 21st ed. 2550
General Chemist	ry Para	meters	Analysis Method
Chloride	1	dissolved	SW846 9251
Cyanide	1	total	SW846 9012A
Fluoride	1	total	SW846 9214
Nitrogen, Nitrate (as N)	1	dissolved	SM4500-NO3
Sulfate	1	dissolved	ASTM516-90,02
Total Dissolved Solids	1	dissolved	SM21 2540 C
META	LS		Analysis Method
Antimony	1	dissolved	SW846 3005A, 7041 (by GFAA)
Arsenic	1	dissolved	SW846 3005A, 6010B (by ICP)
Barium	1	dissolved	SW846 3005A, 6010B (by ICP)
Beryllium	1	dissolved	SW846 3005A, 6010B (by ICP)
Boron	1	dissolved	SW846 3005A, 6010B (by ICP)
Cadmium	1	dissolved	SW846 3005A, 6010B (by ICP)
Chromium	1	dissolved	SW846 3005A, 6010B (by ICP)
Cobalt	1	dissolved	SW846 3005A, 6010B (by ICP)
Copper	1	dissolved	SW846 3005A, 6010B (by ICP)
Iron	1	dissolved	SW846 3005A, 6010B (by ICP)
Lead	1	dissolved	SW846 3005A, 7421 (by GFAA)
Manganese	1	dissolved	SW846 3005A, 6010B (by ICP)
Mercury	1	dissolved	SW846 7470A
Nickel	1	dissolved	SW846 3005A, 6010B (by ICP)
Selenium	1	dissolved	SW846 3005A, 6010B (by ICP)
Silver	1	dissolved	SW846 3005A, 6010B (by ICP)
Thallium	1	dissolved	SW846 3005A, 7841 (by GFAA)
Zinc	1	dissolved	SW846 3005A, 6010B (by ICP)

Notes:

Groundwater quality parameters for Class I: Potable Resource Groundwater (IAC 35 Part 620 Section 410).

Samples filtered and preserved in field.

Table 4. Statistical Summary of Groundwater Quality Data for Period of November 2010 - May 2013

Phase I Hydrogeologic Assessment Joppa Generating Station Electric Energy Inc. Joppa, IL

			Mo	nitoring We	II G101 (N	= 8)			Mor	nitoring We	II G111 (N	= 10)			Mor	itoring We	II G112C (N	= 3)		Monitoring Well G113 (N = 10)					
Parameter, Unit	Class II GW Standard	Mean	Median	Maximum	Minimum	Std Dev	% of Non- Detects	Mean	Median	Maximum	Minimum	Std Dev	% of Non- Detects	Mean	Median	Maximum	Minimum	Std Dev	% of Non- Detects	Mean	Median	Maximum	Minimum	Std Dev	% of Nor Detects
Field Parameters									1							1									
pH, Std Units	6.5/9.0*	6.99	6.97	7.31	6.63	0.23	N/A	7.08	7.09	7.28	6.70	0.155	N/A	6.81	6.79	6.92	6.73	0.097	N/A	6.60	6.57	6,82	6.44	0.11	N/A
General Chemistry Parameters				1	ARREN AND AND				- CRASSINA PA		Lange and the second	THE REAL PROPERTY IN	1			T				Contractor and		T	1		
Chloride (diss), mg/L	200	4.5	4.5	6.0	3.0	0.93	0	6.3	6.0	7.0	5.0	0.67	0	nc	nc	nc	nc	nc	100	30	29	34	28	1.8	0
Cyanide (total), mg/L	0.6	nc	nc	nc	nc	nc	100	nc	nc	nc	nc	nc	100	nc	nc	nc	nc	nc	100	nc	nc	nc	nc	nc	100
Fluoride (total), mg/L	4.0	0.29	0.29	0.33	0.26	0.025	0	0.66	0.67	0.71	0.62	0.033	0	0.78	0.80	0.81	0.74	0.038	0	0.42	0.43	0.45	0.39	0.023	0
Nitrate (diss), mg/L	100	1.3	1.5	1.7	0.28	0.51	0	0.19	0.12	0.72	<0.050	0.21	10	0.15	0.050	0.34	<0.050	0.17	67	0.43	0.44	0.68	0.14	0.15	0
Sulfate (diss), mg/L	400	32	33	35	22	4.4	0	24	24	30	19	3.8	0	63	63	66	60	3.0	0	35	35	50	30	5.8	0
Total Dissolved Solids, mg/L	1,200	246	245	294	208	34	0	357	363	394	322	28	0	440	432	476	412	33	0	600	590	706	524	57	0
		arrenter to														1									COLUMN TO A D
Metals (dissolved)	0.024						100				10.00		100						100	-					100
	0.02	nc	nc	nc	nc	nc	100	nc	nc	nc	nc	nc	100	nc	nc	nc	nc	nc	100	nc	nc	nc	nc	nc	100
Arsenic, mg/L 0.01		nc	nc	nc	nc	nc	100	nc	nc	nc 0.48	nc	nc	100	nc	nc	nc	INC O OFO	nc	1.4.4	nc	nc 0.50	nc 0.55	nc 0,40	0.046	0
Barium, mg./L	2.0	0.20	0.074	0.64	0.044	0.25	0	0.16	0.16	0.18	0.15	0.011	0	0.061	0.062	0.062	0.059	0.0	0	0.49	0.50	and the second se	and the second second	Constant-	100
Beryllium, mg/L	0.5	nc	nc	nc	nc	nc	100	nc	nc	nc	nc	nc	100	nc	nc	nc	nc 3.1	nc	100	nc	nc	nc	nc	nc	100
Boron, mg/L	2.0	nc	nc	nc	nc	nc	100	nc	nc	nc	nc	nc	100	3.2	3.1	3.3		0.12	100	nc	nc	nc	nc	nc	100
Cadmium, mg/L	0.05	nc	nc	nc	nc	nc	100	nc	nc	nc	nc	nc	100	nc	nc	nc	nc	nc	100	nc	nc	nc	nc	nc	100
Chromium, mg/L	1.0	nc	nc	nc	nc	nc	100	nc	nc	nc	nc	nc	100	nc	nc	nc	nc	nc	100	nc	nc	nc	nc	a second second	100
Cobalt, mg/L	1.0	nc	nc	nc	nc	nc	100	nc	nc	nc	nc	nc	100	nc	nc	nc	nc	nc	100	nc	nc	nc	nc	nc	100
Copper, mg/L	0.65	0.039	nc 0.020	0.17	nc <0.020	nc 0.054	100	nc	nc	nc	nc	nc	100	nc 0.036	nc 0.039	nc 0.048	nc <0.020	nc 0.015	33.3	nc	nc	nc	nc	nc	100
ron, mg/L .ead, mg/L	5.0	0.0039	0.020	<0.0070	<0.020	0.0023	12.5	nc	nc	nc	nc	nc	100		0.039	0.040	NC	nc	100	nc	nc	nc	nc	nc	100
Manganese, mg/L	10	0.0030 nc	nc	The second second	100000000	and the second second second	100	nc	nc	nc	nc	nc	100	nc 0.17	0.17	0.18	0.15	0.013	0	0.0074	0.0050	0.025	<0.0050	0.0063	70
Mercury, mg/L	0.010	nc	nc	nc	nc	nc	100	nc	nc	nc	nc		100			0.10	nc	nc	100	0.0074 nc	D.0000	nc	nc	nc	100
vickel, ma/L	2.0	nc		10.000	nc	nc	100	1022.0	nc	nc	nc	nc	100	nc	nc	nc	nc	nc	100	nc	nc	nc	nc	nc	100
Selenium, mg/L	0.05	nc	nc	nc	nc	nc	100	nc	nc	nc	nc	nc	100	nc	nc	nc	nc	nc	100	nc	nc	nc	nc	nc	100
Silver, mg/L	ns	nc	nc	nc	nc	nc	100	nc	nc	пс	nc	nc	100	nc	nc	nc	nc	nc	100	nc	nc	nc	nc	nc	100
fhallium, mg/L	0.020	nc	1000	10000	122.0	nc	100	nc	nc	nc	nc	nc	100	nc	nc	nc	nc	nc	100	nc	nc	nc	nc	nc	100
Zinc, mg/L	10	nc	nc	nc	nc	nc	100	0.011	0.010	0.018	<0.010	0.0026	80	110	nc	nc	nc	nc	100	nc	nc	nc	nc	nc	100
ano, myre	10	nc	110	no	1 10	nc	100	0.011	0.010	0.010	1 -0.010	0.0020	00	HC	1 116	1 110	110	116	100	nu	110	Inc	110	116	1 100

Notes: N = number of observations (does not include August 2010 sampling event, which was not representative due to balling of monitoring wells; all other events used low-flow sampling methods with dedicated bladder pumps). ns = no Class II Groundwater Quality Standard for Parameter. * Lower and Upper limits for pH is the Class I groundwater quality standard of 6.5 and 9.0 Standard Units. Groundwater quality standards for Class II: Potable Resource Groundwater (IAC 35 Part 620 Section 420).

Statistics calculated with replacement of non-detect concentrations at 1X reported non-detect concentration: nc indicates that statistics were not calculated because all values were below reporting levels. Exceeds Class II Groundwater Quality Standard. Parameter is 100% Non-Detect in all 7 monitoring wells.

Table 4. Statistical Summary of Groundwater Quality Data for Period of November 2010 - May 2013

Phase I Hydrogeologic Assessment Joppa Generating Station Electric Energy Inc. Joppa, IL

	T		Mo	nitoring We	II G151 (N	= 8)			Mor	itoring We	II G152B (N	(= 2)		Monitoring Well G153 (N = 8)						
Parameter, Unit	Class II GW Standard	Mean	Median	Maximum		Std Dev	% of Non- Detects	Mean		Maximum		Std Dev	% of Non- Detects	Mean	Median	Maximum	Minimum	Std Dev	% of Nor Detects	
Field Parameters				1								-								
pH. Std Units	6.5/9.0*	6.03	6.01	6.20	5.89	0.10	N/A	6.81	6.81	6.81	6.81	0.00	N/A	6.91	6.93	6.98	6,70	0.086	N/A	
Control of the second second second second	0.0000000000000000000000000000000000000	and the second second	1.2.3.50500	Policia de Carto			Section 1993	1000000000	0.000000773		exercises.						Same distant			
General Chemistry Parameters			1	T																
Chloride (diss), mg/L	200	5.4	5.0	6.0	5.0	0.52	0	49	49	49	48	0.71	0	21	21	24	20	1.6	0	
Cyanide (total), mg/L	0.6	nc	nc	nc	nc	nc	100	nc	nc	nc	пс	nc	100	nc	nc	nc	nc	nc	100	
Fluoride (total), mg/L	4.0	0.21	0.10	0.95	<0.10	0.30	75	0.59	0.59	0.60	0.58	0.014	0	0.83	0.82	0.94	0.75	0.066	0	
Nitrate (diss), mg/L	100	1.2	1.1	2.0	0.62	0.45	0	0.84	0.84	0.87	0.82	0.032	0	0.31	0.28	0.46	0.21	0.075	0	
Sulfate (diss), mg/L	400	103	103	111	98	4.8	0	17	17	18	16	1.4	0	103	104	111	93	6.8	0	
Total Dissolved Solids, mg/L	1,200	252	248	288	228	23	0	483	483	488	478	7.1	0	431	433	484	392	29	0	
	a antipation and a						00200201000	1000000000	1.0.010.0					(81.5			Stores and an an	SIL STATES		
Metals (dissolved)			1																	
Antimony, mg/L	0.024	nc	nc	nc	nc	nc	100	nc	nc	nc	nc	nc	100	пс	nc	nc	nc	nc	100	
Arsenic, mg/L	0.20	nc	nc	nc	nc	nc	100	nc	nc	nc	nc	nc	100	nc	nc	nc	nc	nc	100	
Barium, mg./L	2.0	0.19	0.083	0.79	0.068	0.25	0	0.51	0.51	0.51	0.51	0.0028	0	0.25	0.24	0.31	0.21	0.032	0	
Beryllium, mg/L	0.5	пс	nc	nc	nc	nc	100	nc	nc	nc	nc	nc	100	nc	nc	nc	nc	nc	100	
Boron, mg/L	2.0	0.024	0.020	0.052	<0.020	0.011	87.5	nc	nc	nc	nc	nc	100	0.028	0.020	<0.020	<0.020	0.014	75	
Cadmium, mg/L	0.05	пс	nc	nc	nc	nc	100	nc	nc	nc	nc	nc	100	nc	nc	nc	nc	nc	100	
Chromium, mg/L	1.0	nc	nc	nc	nc	nc	100	nc	nc	nc	nc	nc	100	nc	nc	nc	nc	nc	100	
Cobalt, mg/L	1.0	nc	nc	nc	nc	nc	100	nc	nc	nc	nc	nc	100	nc	nc	nc	nc	nc	100	
Copper, mg/L	0.65	0.010	0.010	0.011	< 0.010	0	87.5	nc	nc	nc	nc	nc	100	nc	nc	nc	nc	nc	100	
Iron, mg/L	5.0	0.25	0.020	1.8	<0.020	0.62	62.5	nc	nc	nc	nc	nc	100	0.025	0.021	0.040	<0.020	0.0072	50	
Lead, mg/L	0.10	nc	nc	nc	nc	nc	100	пс	пс	nc	nc	nc	100	nc	nc	nc	nc	nc	100	
Manganese, mg/L	10	0.029	0.027	0.062	0.011	0.018	0	0.010	0.010	0.015	<0.0050	0.0072	50	0.011	0.0050	0.056	<0.0050	0.018	87.5	
Mercury, mg/L	0.010	nc	nc	nc	nc	nc	100	nc	nc	nc	nc	nc	100	nc	nc	nc	nc	nc	100	
Nickel, mg/L	2.0	nc	nc	nc	nc	nc	100	пс	nc	nc	nc	nc	100	nc	nc	nc	nc	пс	100	
Selenium, mg/L	0.05	nc	nc	пс	nc	nc	100	nc	nc	nc	nc	nc	100	nc	nc	nc	nc	nc	100	
Silver, mg/L	ns	nc	nc	nc	nc	nc	100	nc	nc	nc	nc	пс	100	nc	nc	nc	nc	nc	100	
Thallium, mg/L	0.020	nc	nc	nc	nc	nc	100	nc	nc	nc	nc	nc	100	nc	nc	nc	nc	nc	100	
Zinc, mg/L	10	0.012	0.010	0.017	<0.010	0.0030	62.5	nc	nc	nc	nc	nc	100	nc	nc	nc	nc	nc	100	

Notes: N = number of observations (does not include August 2010 sampling event, which was not representative due to bailing of monitoring wells; all other events used low-flow sampling methods with dedicated bladder pumps). ns = no Class II Groundwater Quality Standard for Parameter. * Lower and Upper limits for pH is the Class I groundwater quality standard of 6.5 and 9.0 Standard Units.

Groundwater quality standards for Class II: Potable Resource Groundwater (IAC 35 Part 620 Section 420). Statistics calculated with replacement of non-detect concentrations at 1X reported non-detect concentration: nc indicates that statistics were not calculated because all values were below reporting levels. Exceeds Class II Groundwater Quality Standard. Parameter is 100% Non-Detect in all 7 monitoring wells.

APPENDIX A WELL SEARCH

A.1 Well Search Overview

The following sources of information were utilized in order to determine community water source and water well locations:

- Illinois State Geological Survey's Illinois Water Well (ILWATER) Internet Map Service
- Illinois State Water Survey Domestic Well Database
- Illinois EPA web-based Geographic Information System (GIS) files
- Illinois Department of Public Health
- Massac County Health Department

A.2 Illinois State Geological Survey (ISGS)

The ISGS website provided an ArcIMS View Map as well as a database query for water wells. ISGS database information including any boring logs and well construction information is provided in this Appendix.

A.3 Illinois State Water Survey (ISWS)

All of the wells found through the ISWS database, also known as the Domestic Well Database, were previously identified on the ISGS website except for three locations, see Table A-1, (well numbers: 75-77). Records contained within the ISWS database, consisting of public, industrial, and commercial water wells, were not all received as of the date of this report. Since the ISWS database generally contains the same well information as the ISGS and Illinois EPA databases, some ISWS well entries on the Appendix A-1 Table were marked as pending. Should any new information be acquired from the ISWS including additional water wells not previously identified from the other sources of the well information, it will be provided as an addendum to this report.

A.4 Illinois Environmental Protection Agency (IEPA)

The Illinois EPA database website provided ArcIMS Viewer Maps showing information on community, non-community, and public water supply wells as defined on the Illinois EPA website:

 Community Water Supply (CWS): a public water supply that serves or is intended to serve at least 15 service connections used by residents or regularly serves at least 25 residents.


APPENDIX A Well Search

Based on the IEPA maps, there are two CWS wells in the vicinity of the Station. One CWS well is located in Section 24, east of the Station, and east of Joppa. This CWS well is not within the 2500 foot search radius from the impoundments. The second CWS well, listed on Figure 5 as well number 51, is located directly east of the Station, in Section 23 and the village of Joppa. CWS well no. 51 has a Minimum Setback Zone (MSZ) of 200 feet and a Phase I Wellhead protection area (WHPA) of 1000 ft. A MSZ is an area of 200 or 400 radial feet surrounding a water well supplying public water system through which contaminants from a source are theoretically likely to move and reach the well. The Phase I WHPA extends the surface and subsurface area surrounding the water well to 1,000 radial feet. The two CWS wells were not identified on the ISGS website.

Twenty-eight water wells owned by the Station were identified in the IEPA database, located within Sections 10, 14, 15, and 23. The IEPA database noted 20 wells owned by the Station as monitoring wells. These 20 monitoring wells can be seen in Table A-1 and are located on the Station property in Section 10.

A.5 Massac County Health Department

Attempts were made to contact the Massac County Health Department to confirm the CWS well systems located in the area. No personnel from the county health department have responded at the date of this report. Should any new information be acquired from the county health department including additional water well information not previously identified from the other sources, it will be provided as an addendum to this report.

A.6 Field Survey

A field survey was conducted on July 11, 2013 to verify selected well locations listed in the ISGS, ISWS, and IEPA databases and to locate wells not identified within the databases. Eight wells listed within State databases, and originally located based on the original boring and/or well logs, were re-located on the well location map based on the visual survey. In addition, six wells could not be located and there was no evidence of any house or building at those locations; therefore it was assumed that there was no active potable supply or receptor at that location. Finally, one well that was not identified in the state records was located and added to the Figure and Table. Meetings were held with the Joppa and Ft. Massic Water Districts to determine whether buildings with well records were serviced by the water districts.

The LaFarge Corporation and Trunkline Gas Pumping Station were consulted to review well locations on their properties, which are immediately west and north of the WAP, respectively. LaFarge personnel indicated that they had four active wells and two inactive wells, and that the remaining borings were likely "test holes". LaFarge also revised and refined the locations for these wells. Trunkline indicated that their wells are no longer active.

Appendix A WELL SEARCH.DOCX



2

Staff: JMR

37



Bureau ID: Site Name:	170000128298 W1270100004 Dynegy Joppa Plant 2100 Portland Rd	Media File Type: WA	ATER	
Site City:	Јорра	State: IL	Zip: 62953-	
		ord has bee ally or who public dis Exemption	lly exempt closure	
		-		
		Redac	tion	
	·			

Exempt Doc #: 12 Document Date: 7 /30/2013 Document Description: PHASE 1 HYDROGEOLOGICAL ASSESSMENT REPORT - APPENDIX A WELL SURVEY REPORTS

Category ID: 06I Cat	egory Description:	GROUNDWATER HYDROGEOLOGIC RPTS	Exempt Type:	Redaction
Permit ID:			Date of Determination:	5 /25/2017

Table A-1. Well Search Results Phase I Hydrogeologic Assessment

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Joppa Generating Station

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Мар	Source of I	Well Informa	tion	Location Name at time of	Well			. Locat	ion		Year Drilled	Aquifer Type	Formation	Well Use	Corrected L (visual su			coordinates Degrees)	CWS		
Well#	ISGS (API)	ISWS	IEPA	completion	Depth	County	Township	Ĺ	Section	SubSection					Latitude (N)	Longitude (W)	Latitude (N)	Longitude (W)	Metered Location	Verified Water Well	
$-\frac{1}{2}$	121270000100		1	Bechtel Corp	304	Massac	155	3E	14		1955			IC					Yes (FM)	Yes	A (NP)
2	121270002300		23	Missouri Portland Cemt	140	Massac	155	3E	15	NW SW	1961			IC	37443 6731		27 314550	00.044002	N (1)	Ná	<u> </u>
3 4	<u>121270003000</u> 121270003100	366704 366705	30		153	Massac	155	3E	14	SW SW NE	1941	<u>.</u>	<u></u>	FD	37º 12.873'	<u>88° 50.699'</u>	37.214550	-88.844983	Yes (J)	Nó No (NE)	
5	121270003100	300705	31 48	Jappa Comprostor Station #7	156	Massac	155	3E 3E	14		1941			FD	· ·		i		No Voc (EMI)	No (NS)	• NA(NP)
6	121270004800		48	Joppa Compressor Station #7 Joppa Compressor Station #7	150 166	Massac	15S 155	3E 3E	10		1950 1950		~	1C 1C		}i			Yes (FM) Yes (FM)	 	NA(NP)
7	121270004900		49 50	Electric Energy Inc	350	Massac Massac	155	3C 3E	10		1950			<u>п</u>			·		Yes (FM)	Yes	A (NP)
8	121270005100		51	Electric Energy Inc	403	Massac	155	3E 3E	14		1951				37•12.879'		37.214650	-88.856083	Yes (FM)	Yes	A (NP)
	121270005200		52	Joppa Grade School	138	Massac	155	3E	14		1940			FD	57 12.075	00 51.505	57.214050		Yes (J)	No (NS)	NA*
10	121270005300		53	Electric Energy Inc	235	Massac	155	3E	15		1951								Yes (FM)	110 (110/	NA(NP)
11	121270005400		54 ·	Joppa Colored Schl	137	Massac	155	3E 3E	23		1940			FD				<u>├</u>	No	No (NS)	NA
12	121270005500		55		65	Massac	155	36	23		1941			FD		· · · · · ·		i	No	No (NS)	NA
13	121270011100	275092	111		78	Massac	155	3E	11		1969	Unconsolidated	gravel & sand	FD	37° 13.433'	88° 50.956'	37.223883	-88.849267	Yes (FM)	Yes	U
14	121270014600	275090	146		150	Massac	155	3E	11	SE SE SE		Unconsolidated	sand gravel	FD			1		1	1	1
16	121270015800	275097	158		160	Massac	155	3E	14	NW NW NE	1971			FD				<u> </u>	No	No (NS)	U
19	121270019800	275091	198		283	Massac	155	3E	11	NE NE SE	1973	Bedrock	broken lime	FD				h		1	1
20	121272022000	**	20220	Mo Portland Cement	110	Massac	155	3E	15	_	1974			IC						1	1
21	121272025500	275089	20255		52	Massac	155	3E	10	SW SE SW	1976			FD	37•13.305'	88° 52.297'	37.221750	-88.871617	No	Yes	NA (PSA)
23	121272047100	275088	20471		175	Massac	155	_ 3E	10	NE SE NW	1987	Bedrock	chert	FD						1	1
26	121272051900		20519	Missouri Portland Cement Co.	110	Massac	155	3E	15		1985			IC							1
27	121272052000		20520	Missouri Portland Cmt Co.	110	Massac	155	ЗE	15		1985	Unconsolidated	alluvial	IC							
29	121272067500	265617	20675		94	Massac	155	3E	11	NE SE SW	1994	Unconsolidated	gravel	FD	37° 13.359'	88° 50.934'	37.222650	-88.848900	Yes (FM)	Yes	NA
32	121272069900	286483	20699		280	Massac	155	3E	11	NW NE NE	1995	Bedrock	chert	FD							
33	121272085100		23716.08871	Maple Grove School	76	Massac	15S	3E	10		1997			IC							
34	121272085600		24645.42174	Lafarge Corp.	98	Massac	155	3E	15	NE NW SW	1997	Unconsolidated	sand & gravel	. IC							
35	121272091900			Missouri Portland Cement Co	451	Massac	155	3E	15	÷	1961			IC			<u> </u>			.	
36	121272092600			Missouri Portland Cement Co	136	Massac	155	3E	15	NW	1961			1C	•	ļ				1	
37	121272092700		25574.75477	Missouri Portland Cement Co	110	Massac	155	3E	15	NW	1961	-		IC		ļ	 _		1		
38	121272092800		26504.08779	Missouri Portland Cement T.H.	130	Massac	155	3E	15	NW	1962			IC							
39	121272092900		27433.42082	Missouri Portland Cement T.H.	138	Massac	155	3E	15	NW	1962			10	ļ	<u> </u>	<u> </u>		.ļ		
40	121272093000		28362.75385	Missouri Portland Cement T.H.	105	Massac	15S	3E	15	NW	1962	-		10					1	4	
41	121272093300		29292.08688	Missouri Portland Cement T.H.	105	Massac	155	3E	15	NW	1962			IC			┼━───				
42	121272093400		30221.4199	Missouri Portland Cement T.H.	169	Massac	155	3E	15	NW	1962		<u> </u>	IC			<u> </u>			N((1)(C)	
43 44	121272094200		31150.75293	Electrical Energy Corp (Joppa)	90	Massac	155	3E	23		1952			<u>іс</u>					No	No (NS)	NA
44	121272096300		32080.08596	Maple Grove School	362	Massac	155	3E	10		1999				 	<u> </u>	┢────	·			
47	121272100900 121272103000	322429	34868.08504 35797.41807	┼──┓┓┓┛┛┓	202	Massac	155	3E	10		2000	Bedrock	limestone	FD					Yes (FM)	No No	<u> </u>
49	121272103000		36726.7511	Midwort Electric Rower Co	202	Massac	155	3E	10	SE NE SE	2000	Bedrock	limestone	FD	37612.000	000 E1 0001	37 116667	-88.866533	Yes (FM)	Yes	A (NP)
50	121272103900		37656.08413	Midwest Electric Power Co. Midwest Electric Power, Inc	238	Massac Massac	15S 15S	3E 3E	15	SW NW NE	1999	Bedrock Bedrock	limestone limestone	10	37°13.000' 37°13.140'	88° 51.992' 88° 52.010'	37.216667 37.21900000		No	Yes	A (NP)
51	121272104000		70900	widwest Electric Power, Inc.		Massac	155	35	23			Bedrock	limestone	CWS	57-15,140	00. 22.010	1.21300000	-00.00000000000000000000000000000000000		103	
52	121272105700		70901			Massac	155	35	24					CWS		<u>+</u>	<u> </u>	+	-		
53	121272106100	362229	39514.75018		92	Massac	155	3E	14	NW NE NE	2001	Unconsolidated	gravel	FD	37°13.211'	88° 50.508'	37,220183	-88.841800	No	No	Ä
54	121272109500		40444.08321	La Farge Corp.	1472	Massac	155	3E	15					FD	+	1	+	+			
55	121272110900			Electric Energy, Inc.	73	Massac	155	3E	10	NW NW SW	2006	Unconsolidated	sand	MONIT	<u> </u>		1	†	+	1	1
56	121272111000			Electric Energy, Inc.	60	Massac	155	3E	10	NE NW SW	2006	Unconsolidated	sand	MONIT	1	+	-1	<u> </u>	1	+	
57	121272111100		~	Electric Energy, Inc.	66	Massac	155	3E	10	SE NW SW	2006	Unconsolidated	sand	MONIT	1		<u> </u>	-1	-1	-	-
58	121272111200			Electric Energy, Inc.	61	Massac	155	3E	10	SE SW SW	2005	Unconsolidated	sand	MONIT			1		·		1
59	121272111300			Electric Energy, Inc.	73	Massac	155	3E	10	NE SW SW	2006	Unconsolidated	sand	MONIT				1	1		
6 0	121272111400			Electric Energy, Inc.	81	Massac	155	3E	10	SW NW SW	2006	Unconsolidated	sand	MONIT					1		
61	121272111500			Electric Energy, Inc.	68	Massac	155	3E	10	SE SW SW	2006	Unconsolidated	sand	MONIT	1			1	1		
62	121272111600			Electric Energy, Inc.	71	Massac	155	3E	10	NW NW SW	2006	Unconsolidated	sand	MONIT				·			-
63	121272111700			Electric Energy, Inc.	81	Massac	155	3E	10	NE SW SW	2006	Unconsolidated	sand	MONIT	1		T		1		-1
64	121272111800			Electric Energy, Inc.	68	Massac	15S	3E	10	SW SW SW	2006	Unconsolidated	sand	MONIT	1			1			
65	121272111900			Electric Energy, Inc.	29	Massac	155	3E	10	NW NW SW	2006	Unconsolidated		MONIT							1
66	121272112000			Electric Energy, Inc.	. 12	Massac	155	3E	10	NE NW SW	2006	Unconsolidated	silt	MONIT	1		<u> </u>				
67	121272112100	-		Electric Energy, Inc.	20	Massac	155	3E	10	SE NW SW	2006	Unconsolidated	clayey sand	MONIT				1			
	121272112200			Electric Energy, Inc.	13	Massac		3E	10	SE SW SW	2006	Unconsolidated		MONIT	1	- <u> </u>	1			· · · · · · · · · · · · · · · · · · ·	

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Table A-1. Well Search Results Phase I Hydrogeologic Assessment

Joppa Generating Station

Мар	Source of	Well Informa	tion	Location Name at time of	Well			Locat	ion						Corrected I	ocation		coordinates Degrees)			
Well#	ISGS (API)	ISWS	IEPA	completion	Depth	County	Township	Range	Section	SubSection	Year Drilled	Aquifer Type	Formation	Well Use	(visual su Latitude (N)	rrvey) Longitude (W)	Latitude (N)	Longitude (W)	CWS Metered Location	Verified Water Well	Current Well Status
69	121272112300			Electric Energy, Inc.	18	Massac	15\$	3E	10	NE SW SW	2006	Unconsolidated	silt	MONIT							
70	121272112400			Electric Energy, Inc.	27	Massac	155	3E	10	SW NW SW	2006	Unconsolidated	silt	MONIT							
71	121272112500			Electric Energy, Inc.	16	Massac	155	3E	10	SE SW SW	2006	Unconsolidated	silt	MONIT							<u> </u>
72	121272112600			Electric Energy, Inc.	23	Massac	155	3E	10	NW NW SW	2006	Unconsolidated	silt & sand	MONIT				[
. 73	121272112700			Electric Energy, Inc.	24	Massac	155	3E	10	NE SW SW	2006	Unconsolidated	silty sand	MONIT							· · · · · · · · · · · · · · · · · · ·
74	121272112800			Electric Energy, Inc.	20	Massac	155	3E	10	SW SW SW	2006	Unconsolidated	silt	MONIT			•		<u> </u>		
75	121272117200			LaFarge N.A., Midwest River	227	Massac	155	3E	15	NW NE SW	2010	Bedrock	limestone	IC							
76	-	275094			162	Massac	155	3E			1961			FD							
77		366703				Massac	15S	ЗE			1896			FD							
78		366706			65	Massac	155	ЗE			1941			FD						<u> </u>	
79						Massac	15S	3E	11					, FD	37°13.278'	88° 50.938'	37.22130000	-88.84896667	No	Yes	A

Source of Information

IEPA Illinois Environmental Protection Agency

ISGS Illinois State Geological Survey

ISWS Illinois State Water Survey

SWAP IEPA Source Water Assessment

Well Use

CWS Community Water Supply Well

MONIT Joppa Power Station Monitoring Well

FD Farm and/or Domestic Water Well

IC Industrial/Commercial Water Well

<u>Notes</u>

-- Not Applicable or no information available

A Active

NA Not Active

U Unknown

NP Non-potable / industrial use only

J Village of Joppa CWS metered location

FM Fort Massac Water District CWS metered location

NS No structure and/or well at location based on visual survey

Antenan Research

PSA Pending seal and abandonent of well

Reported sealed but no record

LATITUDE 37.216133

COUNTY Massac

42

83

154

158

227 227

15 - 158 - 3E

Water Well for Commercial Operation Bottom Тор clay 0 gravel & sand 42 gray clay 83 broken up limestone 154 gray limestone 158 Total Depth 10" STEEL from -1' to 157' Casing: Water from limestone at 160' to 222'. Static level 56' below casing top which is 3' above GL Pumping level 67' when pumping at 700 gpm for 3 hours Permanent pump installed at 147' on December 22, 2010, with a Remarks: Driller's Estimated Welth Preitdy Roof Sportsport Additional Lot: Subdivision: Joppa Plant location info: Address of well: same as above Location source: Global Positioning System verified Permit #: 127-12-Permit Date: November 9, 2010 COMPANY Beanland, Glen FARM LaFarge N.A., Midwest River DATE DRILLED December 3, 2010 NO. COUNTY NO. 21172 ELEVATION 367GL LOCATION NW NE SW

LONGITUDE -88.873433

API 121272117200

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Electronic Filing: Received, Clerk's Office 11/22/2021 **AS 2021-05** **ILLINOIS STATE GEOLOGICAL SURVEY**

Monitoring				Тор	Bottom
clayey silt				0	19
silty clay				19	20
Total Depth					20
Casing:	2" PVC from -3' 2" PVC SCREEN f 2" PVC from 20'	rom 15' to	20'		
Screen: 5' d	of 2" diameter 1				
Grout: BENT	ONITE from 0 to	13.			
Grout: BENT	ONITE CHIPS from	13 to 14			
Grout: QUAR	TZ SAND from 14	to 20.			
Water from a	silt at 14' to 2	0'.			
Address of a	well: Portland	Rd. & Bac	cus Rd.		
	Joppa, IL	,			
Permit Date	:		Permit #:		
COMPANY	Holcomb Foundat	ion Eng.			
FARM	Electric Energy	, Inc.			
	ED December 1,		NO. MW10S		
ELEVATION	371	COU	NTY NO. 21128		
LOCATION					
LATITUDE		LONGITU	DE -88.874989		

Page 1

Monitoring	Тор	Bottom
clayey silt	0	17
silty sand	17	20
bilty clay	20	24
Total Depth Casing: 2" PVC from -3' to 19' 2" PVC SCREEN from 19' to 23' 2" PVC from 23' to 24' Screen: 4' of 2" diameter 10 slot Scrout: BENTONITE CHIPS from 0 to 16. Grout: QUARTZ SAND from 16 to 24. Nater from silty sand at 17' to 20'. Static level 13' below casing top which is 3' above GL		24
Address of well: Portland Rd. & Baccus Rd. Joppa, IL Location source: Location from the driller		
Permit Date: Permit #:	I	
COMPANY Holcomb Foundation Eng. FARM Electric Energy, Inc.		
DATE DRILLED November 10, 2006 NO. MW09S		
ELEVATION 364 COUNTY NO. 21127		
ELEVATION 364COUNTY NO. 21127LOCATIONNE SW SWLATITUDE37.22415LONGITUDE-88.872644		

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Monitoring	Top	Bottom
clayey silt	0	22
clayey sand	22	23
Total Depth		23
Casing: 2" PVC from -3' to 18' 2" PVC SCREEN from 18' to 23' 2" PVC from 23' to 23'		
Screen: 5' of 2" diameter 10 slot		
Grout: BENTONITE CHIPS from 0 to 17.		
Grout: QUARTZ SAND from 17 to 23.		
Water from silt & sand at 17' to 23'. Static level 22' below casing top which is 3' above GI		
Address of well: Portland Rd. & Baccus Rd. Joppa, IL		
Location source: Location from the driller		
Permit Date: Permit #:		
COMPANY Holcomb Foundation Eng.		
FARM Electric Energy, Inc.		
DATE DRILLED November 17, 2006 NO. MW08S		
ELEVATION 378 COUNTY NO. 21126		
LOCATION NW NW SW		
LATITUDE 37.227853 LONGITUDE -88.874897		

Page 1

Monitoring	s	Top	Bottom
clayey silt	:	0	14
silty clay		14	16
Total Depth	1		16
Casing:	2" PVC from -3' to 10: 2" PVC SCREEN from 10' to 15' 2" PVC from 15' to 16'		
Screen: 5'	of 2" diameter 10 slot		
	CONITE CHIPS from 0 to 9.		
Grout: QUAF	RTZ SAND from 9 to 16.		
Water from	silt at 9' to 14'.		
Static leve	el 16' below casing top which is 3' above GL		
Address of	well: Portland Rd & Baccus Rd. Joppa, IL		
Location ec	burce: Location from the driller		
Permit Date	e: Permit #:		l
COMPANY	Holcomb Foundation Eng.		
FARM	Electric Energy, Inc.		
	LED November 29, 2006 NO. MW07S		
DATE DRIL	360 COUNTY NO. 21125		
ELEVATION	360 COUNTY NO. 21125		
ELEVATION	SE SW SW		

Electronic Filing: Received, Clerk's Office 11/22/2021 **AS 2021-05** ILLINOIS STATE GEOLOGICAL SURVEY

Monitoring	3			Тор	Bottom
clayey silt	z			0	2*
Total Depth	a				27
Casing:	2" PVC from -3	from 21' to 26'			
Screen: 5'	of 2" diameter	10 slot			
Grout: BENT	CONITE CHIPS fro	om 0 to 19.			
Grout: QUAF	RTZ SAND from 1	9 to 27.			
	silt at 19' to ≥l 25' below ca	27'. Sing top which is	3' above GL		
Address of	well: Portland Joppa, 2	l Rd. & Baccus Rd L			
Location so	ource: Location	from the driller			
Permit Date	e:		Permit #:		
COMPANY	Holcomb Founda	tion Eng.			
FARM	Electric Energ	y, Inc.			
DATE DRIL	LED November 14	, 2006 N	O. MW06S		
ELEVATION	373	COUNTY N	0. 21124		
LOCATION	SW NW SW				
LATITUDE		LONGITUDE -8	8.874927		
COUNTY	Massac	API 1212	72112400	10 - 15	S - 3E

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	1	

Page 1

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Page 1

Monitoring		Тор	Bottom
clayey silt		0	16
silty clay		16	18
Total Depth Casing: 2" PVC from -3' t 2" PVC SCREEN fro 2" PVC from 17' t Screen: 5' of 2" diameter 10 Grout: BENTONITE from 0 to 6. Grout: BENTONITE CHIPS from 7 Grout: QUARTZ SAND from 11 to	m 12' to 17' o 18' slot ' to 11.		18
Water from silt at 12' to 16'	· -		
Address of well: Portland Rd Joppa, IL Location source: Location fro			
Permit Date:	Permit	= #:	
COMPANY Holcomb Foundation FARM Electric Energy,	Inc.		
DATE DRILLED December 6, 20			
ELEVATION 364	COUNTY NO. 211	.23	
LOCATION NE SW SW			
LATITUDE 37.22415	LONGITUDE -88.8726	544	

Electronic Filing: Received, Clerk's Office 11/22/2021 **AS 2021-05** ILLINOIS STATE GEOLOGICAL SURVEY

Monitoring	Тор	Bottom
layey silt	0	
layey sand	7	12
ilty clay	12	13
otal Depth asing: 2" PVC from -3' to 7' 2" PVC SCREEN from 7' to 12' 2" PVC from 12' to 13' creen: 5' of 2" diameter 10 slot		13
rout: BENTONITE CHIPS from 0 to 6.		
rout: QUARTZ SAND from 6 to 12.		
ater from clayey sand at 7' to 12'. tatic level 15' below casing top which is 3' above GL		
ddress of well: Portland Rd. & Baccus Rd. Joppa, IL		
ocation source: Location from the driller		
ermit Date.		
ermit Date: Permit #:		<u> </u>
COMPANY Holcomb Foundation Eng.		
ARM Electric Energy, Inc.		
ATE DRILLED December 5, 2006 NO. MW04S		
COUNTY NO. 21122		
COUNTY NO. 21122 COCATION SE SW SW ATITUDE 37.222321 LONGITUDE -88.872675		

Page 1

Monitoring			Top	Bottom
clayey silt			0	16
clayey sand	to 19.5', silty cla	y to 19.7	16	20
Total Depth	2" PVC from -3' to	151		20
	2" PVC SCREEN from 2" PVC from 19' to	15' to 19'		
Screen: 5'	of 2" diameter 10 sl	ot		
Grout: BENT	ONITE from 3 to 12.			
	ONITE CHIPS from 12			
Grout: QUAR	TZ SAND from 13 to 2	.0.		
Water from	clayey sand at 16' t	:o 20'.		
Address of	well: Portland Rd. Joppa, IL	& Baccus Rd.		
Location so	urce: Location from	the driller		
Permit Date	:	Permit #:		
COMPANY	Holcomb Foundation	Eng.		
FARM	Electric Energy, In	c.		
DATE DRIL	ED December 4, 2006	NO. MW03S		
ELEVATION	367	COUNTY NO. 21121		
LOCATION	SE NW SW			
LATITUDE		NGITUDE -88.872612		ليئي النظر
			10 - 15	

Electronic Filing: Received, Clerk's Office 11/22/2021 **AS 2021-05** ILLINOIS STATE GEOLOGICAL SURVEY

Monitoring	Тор	Bottom
clayey silt	0	11
silty clay	11	12
Total Depth Casing: 2" PVC from 12' to 12' 2" PVC from -3' to 7' 2" PVC SCREEN from 7' to 12' Screen: 5' of 2" diameter 10 slot Grout: BENTONITE CHIPS from 0 to 7. Grout: QUARTZ SAND from 7 to 12. Water from silt at 7' to 11'. Static level 9' below casing top which is 3' above GL		12
Address of well: Portland Rd. & Baccus Rd. Joppa, IL		
Permit Date: Permit #:		
COMPANY Holcomb Foundation Eng.		
FARM Electric Energy, Inc. DATE DRILLED November 27, 2006 NO. MW02S ELEVATION 360 COUNTY NO. 21120 LOCATION NE NW SW		
LATITUDE 37.227808 LONGITUDE -88.872581		

Page 1

Page 1

Monitoring	Тор	Bottom
clayey silt	0	24
clay sand	24	28
silty clay	28	29
Total Depth Casing: 2" PVC from -3' to 24' 2" PVC SCREEN from 24' to 28' 2" PVC from 28' to 28'		25
Screen: 4' of 2" diameter 10 slot		
Grout: BENTONITE CHIPS from 0 to 23.		
Grout: QUARTZ SAND from 23 to 29.		
Water from silt at 24' to 28'. Static level 28' below casing top which is 3' above GL		
Address of well: Portland Rd. & Baccus Rd. Joppa, IL		
Location source: Location from the driller		
Permit Date: Permit #:		
Permit Date: Permit #: COMPANY Holcomb Foundation Eng.		
COMPANY Holcomb Foundation Eng.		
COMPANY Holcomb Foundation Eng. FARM Electric Energy, Inc.		
COMPANY Holcomb Foundation Eng. FARM Electric Energy, Inc. DATE DRILLED November 28, 2006 NO. MW01S		
COMPANYHolcomb Foundation Eng.FARMElectric Energy, Inc.DATE DRILLED November 28, 2006NO. MW01SELEVATION 384COUNTY NO. 21119		

Monitoring	Тор	Bottom
clayey silt	0	19
silty clay	19	26
silty sand	26	28
silty clay	28	34
clayey sand	34	51
silty sand	51	63
sand	63	68
Total Depth		68
Casing: 2" PVC from -3' to 63' 2" PVC SCREEN from 63' to 67' 2" PVC from 67' to 68' Screen: 4' of 2" diameter 10 slot Grout: BENTONITE from 0 to 58. Grout: BENTONITE CHIPS from 58 to 61. Water from sand at 63' to 68'. Static level 56' below casing top which is 3' above GL		
Address of well: Portland Rd. & Baccus Rd. Joppa, IL Location source: Location from the driller		
Permit Date: Permit #:		
COMPANY Holcomb Foundation Eng.		
FARM Electric Energy, Inc.		
DATE DRILLED December 1, 2006 NO. MW10D		
ELEVATION 371 COUNTY NO. 21118		
		···÷···]
LOCATION SW SW SW LATITUDE 37.222365 LONGITUDE -88.874989		

Monitoring					Тор	Bottom
clayey silt					0	17
silty sand					17	20
silty clay					20	52
clayey sand					52	61
silty sand					61	71
sand					71	81
Total Depth						81
Casing: 2 2	" PVC from -3 " PVC SCREEN " PVC from 81	from 76' to	· 81'			
	2" diameter					
	ITE from 0 to					
	NITE CHIPS fro					
-	SAND from 73					
	and at 73' to 48' below cas		ich is 3'	above GL		
	ell: Portland Joppa, I	Ľ				
Location sour	rce: Location	from the d	riller			
Permit Date:			Pe	rmit #:		
	lol comb Founda	tion Eng.				
COMPANY H	Orcomb Founda					
	lectric Energ	y, Inc.				
FARM E			NO.	MW09D		
FARM E	lectric Energ D November 10	, 2006	NO. NTY NO.			
FARM E DATE DRILLE ELEVATION 3	lectric Energ D November 10	, 2006				
FARM E DATE DRILLE ELEVATION 3 LOCATION 1	lectric Energ D November 10 64	, 2006 COU		21117		

COUNTY Massac

clayey silt 0 clayey sand 22 silty clay 24 clayey sand 37 silty sand 50 sand 66 Total Depth 66 Casing: 2" PVC from -3' to 66' 2" PVC SCREEN from 66' to 71' 2" PVC from 71' to 71' 2" PVC SCREEN from 66' to 71' 2" PVC from 71' to 71' Screen: 5' of 2" diameter 10 slot Grout: BENTONITE from 0 to 62. Grout: BENTONITE CHIPS from 62 to 64. Grout: QUARTZ SAND from 64 to 71. Water from sand at 66' to 71'. Static level 60' below casing top which is 3' above GL Address of well: Portland Rd. & Baccus Rd. Joppa, IL Location source: Location from the driller Permit Date: Permit #: COMPANY Holcomb Foundation Eng. FARM Electric Energy, Inc. DATE DRILLED November 17, 2006 NO. MWOBD ELEVATION 378 COUNTY NO. 21116 LOCATION NW NW SW	Monitoring			Тор	Bottom
silty clay 24 clayey sand 37 silty sand 50 sand 66 Total Depth 66 Casing: 2" PVC from -3' to 66' 2" PVC SCREEN from 66' to 71' 2" FVC from 71' to 71' Screen: 5' of 2" diameter 10 slot Grout: BENTONITE CHIPS from 62 to 64. Grout: GUARTZ SAND from 64 to 71. Water from sand at 66' to 71'. Static level 60' below casing top which is 3' above GL Address of well: Portland Rd. & Baccus Rd. Joppa, IL Location source: Location from the driller Permit Date: Permit #: COMPANY Holcomb Foundation Eng. FARM Electric Energy, Inc. DATE DRILLED November 17, 2006 NO. MWOBD ELEVATION 378 COUNTY NO. 21116	clayey silt			0	2:
clayey sand 37 silty sand 50 sand 66 Total Depth 66 Casing: 2" PVC from -3' to 66' 2" PVC SCREEN from 66' to 71' 2" PVC from 71' to 71' Screen: 5' of 2" diameter 10 slot Grout: BENTONITE from 0 to 62. Grout: GUARTZ SAND from 64 to 71. Water from sand at 66' to 71'. Static level 60' below casing top which is 3' above GL Address of well: Portland Rd. & Baccus Rd. Joppa, IL Location source: Location from the driller Permit Date: Permit #: COMPANY Holcomb Foundation Eng. FARM Electric Energy, Inc. DATE DRILLED November 17, 2006 NO. MWORD ELEVATION 378 COUNTY NO. 21116	clayey sand			22	24
silty sand 50 sand 50 fotal Depth Casing: 2" PVC from -3' to 66' 2" PVC SCREEN from 66' to 71' 2" PVC from 71' to 71' 2" PVC from 71' to 71' Screen: 5' of 2" diameter 10 slot Grout: BENTONITE from 0 to 62. Grout: BENTONITE CHIPS from 62 to 64. Grout: QUARTZ SAND from 64 to 71. Water from sand at 66' to 71'. Static level 60' below casing top which is 3' above GL Address of well: Portland Rd. & Baccus Rd. Joppa, IL Location source: Location from the driller Permit Date: Permit #: COMPANY Holcomb Foundation Eng. FARM Electric Energy, Inc. DATE DRILLED November 17, 2006 NO. MW08D ELEVATION 378 COUNTY NO. 21116	silty clay			24	3'
sand 66 Total Depth 2" PVC from -3' to 66' Casing: 2" PVC SCREEN from 66' to 71' 2" PVC from 71' to 71' 2" PVC from 71' to 71' Screen: 5' of 2" diameter 10 slot Grout: BENTONITE from 0 to 62. Grout: QUARTZ SAND from 64 to 71. Water from sand at 66' to 71'. Static level 60' below casing top which is 3' above GL Address of well: Portland Rd. & Baccus Rd. Joppa, IL Location source: Location source: Location from the driller Permit Date: Permit #: COMPANY Holcomb Foundation Eng. FARM Electric Energy, Inc. DATE DRILLED November 17, 2006 NO. MW08D ELEVATION 378 COUNTY NO. 21116	clayey sand			37	50
Total Depth Casing: 2" PVC from -3' to 66' 2" PVC SCREEN from 66' to 71' 2" PVC from 71' to 71' Screen: 5' of 2" diameter 10 slot Grout: BENTONITE from 0 to 62. Grout: BENTONITE CHIPS from 62 to 64. Grout: QUARTZ SAND from 64 to 71. Water from sand at 66' to 71'. Static level 60' below casing top which is 3' above GL Address of well: Portland Rd. & Baccus Rd. Joppa, IL Location source: Location from the driller Permit Date: Permit #: COMPANY Holcomb Foundation Eng. FARM Electric Energy, Inc. DATE DRILLED November 17, 2006 NO. MWOBD ELEVATION 378 COUNTY NO. 21116	silty sand			50	60
Casing: 2" PVC from -3' to 66' 2" PVC SCREEN from 66' to 71' 2" PVC from 71' to 71' Screen: 5' of 2" diameter 10 slot Grout: BENTONITE from 0 to 62. Grout: BENTONITE CHIPS from 62 to 64. Grout: QUARTZ SAND from 64 to 71. Water from sand at 66' to 71'. Static level 60' below casing top which is 3' above GL Address of well: Portland Rd. & Baccus Rd. Joppa, IL Location source: Location from the driller Permit Date: Permit #: COMPANY Holcomb Foundation Eng. FARM Electric Energy, Inc. DATE DRILLED November 17, 2006 NO. MW08D ELEVATION 378 COUNTY NO. 21116	sand			66	7:
Joppa, IL Location source: Location from the driller Permit Date: Permit #: COMPANY Holcomb Foundation Eng. FARM Electric Energy, Inc. DATE DRILLED November 17, 2006 NO. MW08D ELEVATION 378 COUNTY NO. 21116	Casing: Screen: 5' Grout: BENT Grout: BENT Grout: QUAR Water from :	2" PVC from - 2" PVC SCREEN 2" PVC from 7 of 2" diamete ONITE from 0 ONITE CHIPS f TZ SAND from sand at 66' to	N from 66' to 71' 71' to 71' r 10 slot to 62. rom 62 to 64. 64 to 71. o 71'.	31	73
Permit Date: Permit #: COMPANY Holcomb Foundation Eng.		Joppa,	IL		
COMPANY Holcomb Foundation Eng. FARM Electric Energy, Inc. DATE DRILLED November 17, 2006 NO. MW08D ELEVATION 378 COUNTY NO. 21116					
FARM Electric Energy, Inc. DATE DRILLED November 17, 2006 NO. MW08D ELEVATION 378 COUNTY NO. 21116	Permit Date	:	Permit #:		
DATE DRILLED November 17, 2006 NO. MW08D ELEVATION 378 COUNTY NO. 21116	COMPANY	Holcomb Found	lation Eng.		
ELEVATION 378 COUNTY NO. 21116	FARM	Electric Ener	rgy, Inc.		
	DATE DRILL	ED November 1	7, 2006 NO. MW08D		
LOCATION NW NW SW	ELEVATION	378	COUNTY NO. 21116		
	LOCATION	NW NW SW			

API 121272111600

10 - 155 - 3E

Page 1

Monitoring	Тор	Bottom
clayey silt	0	14
silty clay	14	33
clayey sand	33	48
silty sand	48	62
Sand	62	68
Fotal Depth		68
Casing: 2" PVC from -3' to 62' 2" PVC SCREEN from 62' to 67' 2" PVC from 67' to 68'		
Screen: 5' of 2" diameter 10 slot		
Grout: BENTONITE from 0 to 57.		
Grout: BENTONITE CHIPS from 57 to 58.		:
Grout: QUARTZ SAND from 58 to 68.		
Mater from sand at 58' to 68'. Static level 43' below casing top which is 3' above GL		
Address of well: Portland Rd. & Baccus Rd. Joppa, IL Location source: Location from the driller		
		:
Permit Date: Permit #:		
COMPANY Holcomb Foundation Eng.		
FARM Electric Energy, Inc.		
DATE DRILLED November 29, 2006 NO. MW07D		
ELEVATION 360 COUNTY NO. 21115		

LATITUDE 37.226024

COUNTY Massac

10 - 155 - 3E

	3	Тор	Bottom
clayey silt	:	0	2
silty clay		28	4
clayey sand	1	40	4
silty sand		48	7
sand		77	6
			8
Grout: BENI	2" PVC from -3' to 76' 2" PVC SCREEN from 76' to 81' 2" PVC from 81' to 81' of 2" diameter 10 slot CONITE from 0 to 69. CONITE CHIPS from 69 to 74.		
	ATION SAND from 74 to 81.		
	sand at 63' to 73'. El 57' below casing top which is 3' above GL		
Address of	well: Portland Rd. & Baccus Rd. Joppa, IL		
Location BC	ource: Location from the driller		
Permit Date	e: Permit #:		
	e: Permit #: Holcomb Foundation Eng.		
COMPANY			
Company Farm	Holcomb Foundation Eng.		
Company Farm	Holcomb Foundation Eng. Electric Energy, Inc. LED November 14, 2006 NO. MW06D		

LONGITUDE -88.874927

API 121272111400

Page 1

		Тор	Bottom
clayey silt		0	1
silty clay		16	2
clayey sand	I	24	3
silty sand		31	5
sand		51	7
Total Depth			7
Casing:	2" PVC from -3' to 68' 2" PVC SCREEN from 68' to 73' 2" PVC from 73' to 73'		
Screen: 5'	of 2" diameter 10 slot		
Grout: BENT	ONITE from 0 to 60.		ļ
Grout: BENT	ONITE CHIPS from 60 to 63.		
Grout: FORM	ATION SAND from 63 to 73.		
	sand at 63' to 73'. El 44' below casing top which is 3' above GL		
	well: Portland Rd. & Baccus Rd. Joppa, IL purce: Location from the driller		
Permit Date	o: Permit #:		
	e: Permit #: Holcomb Foundation Eng.		
COMPANY FARM	Holcomb Foundation Eng.		
COMPANY Farm Date Drili	Holcomb Foundation Eng. Electric Energy, Inc. LED December 6, 2006 NO. MW05D		
COMPANY Farm Date Drili Elevation	Holcomb Foundation Eng. Electric Energy, Inc. LED December 6, 2006 NO. MW05D 364 COUNTY NO. 21113		
COMPANY Farm Date Drili	Holcomb Foundation Eng. Electric Energy, Inc. LED December 6, 2006 NO. MW05D 364 COUNTY NO. 21113 NE SW SW		

COUNTY Massac

	g	Тор	Bottom
clayey sil	t	0	
clayey san	d	7	1:
silty clay		12	2'
clayey san	d	27	4
silty sand		40	54
sand		54	63
Total Dept	Ъ		63
Casing:	2" PVC from -3' to 56' 2" PVC SCREEN from 56' to 60' 2" PVC from 60' to 61'		
	of 2" diameter 10 slot		
	TONITE from 0 to 52.		
	TONITE CHIPS from 52 to 54. RTZ SAND from 54 to 61.		
	sand at 54' to 61'.		
	el 34' below casing top which is 3' above GL		
Address of	well: Portland Rd. & Baccus Rd. Joppa, IL		
Location s	ource: Location from the driller		
LOCATION 5	ource: Location from the driller		
Permit Dat	e: Permit #: Holcomb Foundation Eng.		
Permit Dat COMPANY FARM	e: Permit #: Holcomb Foundation Eng. Electric Energy, Inc.		
Permit Dat COMPANY FARM	e: Permit #: Holcomb Foundation Eng. Electric Energy, Inc. SLED December 5, 2006 NO. MW04D		
Permit Dat COMPANY FARM DATE DRII ELEVATION	e: Permit #: Holcomb Foundation Eng. Electric Energy, Inc. LED December 5, 2006 NO. MW04D		

API 121272111200

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	g	Тор	Bottom
clayey silt	t	0	1
clayey sand	a	16	2
silty clay		20	2
clayey sand	a	25	4
silty sand		44	5
sand		50	6
Total Dept	h		6
Casing:	2" PVC from -3' to 61' 2" PVC SCREEN from 61' to 66' 2" PVC from 66' to 66'		
Screen: 5'	of 2" diameter 10 slot		1
Grout: BEN	TONITE from 6 to 54.		
Grout: BEN	TONITE CHIPS from 54 to 58.		
Grout: QUA	RTZ SAND from 58 to 66.		
	sand at 61' to 66'. el 50' below casing top which is 3' above GL		
Address of	well: Portland Rd. & Baccus Rd. Joppa, IL		
Location se	ource: Location from the driller		
Permit Dat	e: Permit #:		
Permit Dat			
COMPANY FARM	Holcomb Foundation Eng.		
COMPANY FARM	Holcomb Foundation Eng. Electric Energy, Inc. ,LED December 4, 2006 NO. MW03D		
COMPANY FARM DATE DRIL ELEVATION	Holcomb Foundation Eng. Electric Energy, Inc. LED December 4, 2006 NO. MW03D 367 COUNTY NO. 21111		
COMPANY FARM DATE DRIL ELEVATION LOCATION	Holcomb Foundation Eng. Electric Energy, Inc. ,LED December 4, 2006 NO. MW03D		

LOCATION NE NW SW LATITUDE 37.227808

COUNTY Massac

Monitoring	Тор	Bottom
clayey silt	0	1
silty clay	11	1.
clayey sand	14	2
silty clay	26	2
clayey sand	29	4
silty sand	40	5:
sand	52	6
Total Depth Casing: 2" PVC from -3' to 55' 2" PVC SCREEN from 55' to 60' 2" PVC from 60' to 60' Screen: 5' of 2" diameter 10 slot Grout: BENTONITE from 11 to 52. Grout: BENTONITE CHIPS from 52 to 53. Grout: QUARTZ SAND from 58 to 66. Water from sand at 52' to 60'. Static level 36' below casing top which is 3' above	GL	61
Address of well: Portland Rd. & Baccus Rd. Joppa, IL Location source: Location from the driller		
Permit Date: Permit #: COMPANY Holcomb Foundation Eng. FARM Electric Energy, Inc.		
DATE DRILLED November 27, 2006 NO. MW02D		
REFUENCE NO. THEORY NO. 21110		

LONGITUDE -88.872581

API 121272111000

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Monitoring Bottom Тор clayey silt 0 24 clayey sand 24 28 silty clay 28 41 clayey sand 41 49 silty sand 49 64 sand 64 73 Total Depth 73 2" PVC SCREEN from 67' to 72' Casing: 2" PVC from -3' to 67' 2" PVC from 72' to 73' Screen: 5' of 2" diameter 10 slot Grout: BENTONITE from 12 to 63. Grout: BENTONITE CHIPS from 63 to 65. Grout: QUARTZ SAND from 65 to 72. Water from sand at 67' to 73'. Static level 62' below casing top which is 3' above GL Address of well: Portland Rd. & Baccus Rd. Joppa, IL Location source: Location from the driller Permit #: Permit Date: COMPANY Holcomb Foundation Eng. Electric Energy, Inc. FARM DATE DRILLED November 28, 2006 NO. MW01D COUNTY NO. 21109 **ELEVATION 384** NW NW SW LOCATION LONGITUDE -88.874897 LATITUDE 37.227853 10 - 15S - 3E COUNTY Massac API 121272110900

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Test Hole				Тор	Bottom
Total Depth					1472
Gamma Ray L	og filed				
Location so	urce: Field veri	fied			
					Î
					ļ
Permit Date	:		Permit #:		
COMPANY	IL State Geolog	ical Survey			
FARM	La Farge Corp.				
DATE DRILI	LED		NO. J2-04		
ELEVATION			Y NO. 21095		
	1098'N line, 12 37.218362		section -88.872106		
COUNTY	Massac	API 1	21272109500	15 - 15	55 - 3E

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Private Water Well	Тор	Bottom
dirt & clay	o	42
sandy clay	42	50
gravel & clay	50	62
sand & clay	62	87
gravel	87	92
Total Depth Casing: 6.25" PVC from 1' to 89' 6.25" PVC SCREEN from 89' to 92' Screen: 3' of 6.25" diameter .03 slot		92
Grout: CLAY from 0 to 3.		
Frout: ENVIROPLUG from 3 to 85. Grout: WASHED PEA GVL from 85 to 92.		
Static level 60' below casing top which is 1' above GL Pumping level 70' when pumping at 10 gpm for 24 hours Permanent pump installed at 83'.on , with a capacity of Remarks: driller's est. well yield 30 gpm Address of well: same as above Location source: Location from permit	10 gpm	
Permit Date: September 17, 2001 Permit #:		
COMPANY Beanland, Leonard Ralph		
FARM		
FARM CONTRACTOR NO.		

COUNTY Massac

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	ater Supply				Тор	Bottom
no record					0	448
Total Depth						448
Casing:	10" OUTER CASING 1 6" CASING from 0') '			
Static level	32' below casing	top which	is O' abo	ve GL		
	l 175' when pumpi					
-						
						.
						-
Permit Date:	<u>، </u>		Permit	#:		
COMPANY						
FARM	Joppa, Village					
DATE DRILL	ED January 1, 1953		NO. 1			
ELEVATION	0	COUNTY	NO. 2105	57		
LOCATION	500'S 500'E NW/c					

API 121272105700

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opsoil clay & gray silty sand and w/trace of gravel imestone shelf followed by f sy clay andy & silty clay/weather limestone	0 28	2
imestone shelf followed by f sy clay	28	
		16
andy & silty clay/weather limestone	160	26
	263	27
ractured limestone	273	27
Cotal Depth Casing: 12" STAINLESS 49.56FT from -2' to 160' 10" STAINLESS 40.48FT from -2' to 273' Frout: CEMENT from 0 to 273.		27
ize hole below casing: 10"		
Nater from limestone at 273' to 277'. Static level 45' below casing top which is 2' above GL Pumping level 50' when pumping at 600 gpm for 12 hours Permanent pump installed at 150' on , with a capacity c address of well: 2100 Portland Rd. Joppa IL	o£ 600 gpm	
ocation source: Location from permit		
Permit Date: November 18, 1999 Permit #:		
COMPANYStollhans, JeffFARMMidwest Electric Power, IncDATE DRILLED January 19, 2000NO. 5ELEVATION 0COUNTY NO. 21040LOCATIONNW NW NE		
LATITUDE 37.220361 LONGITUDE -88.865779 COUNTY Massac API 121272104000	15 - 15	

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Non Potable Water Well	Тор	Bottom
topsoil & clay w/silty sand	0	22
clay w/fine to medium sand	22	136
fine to medium sand w/clay seams	136	220
weathered limestone	220	225
fractured limestone	225	238
Total Depth Casing: 12" STAINLESS #49.56/FT from -2' to 228' Grout: CEMENT from 1 to 228.		238
Size hole below casing: 12"		
<pre>Water from limestone at 228' to 238'. Static level 40' below casing top which is 2' above GL Pumping level 44' when pumping at 603 gpm for 12 hours Permanent pump installed at 150' on , with a capacity of Address of well: 2100 Portland Rd Joppa IL Location source: Location from permit Location source: Location from permit Permit Date: November 18, 1999 Permit #:</pre>	£ 600 gpm	
COMPANY Stollhans, Jeff		
FARM Midwest Electric Power Co.		
DATE DRILLED February 29, 2000 NO. 6		
ELEVATION 380 COUNTY NO. 21039		
LOCATION SW NW NE		
LATITUDE 37.218537 LONGITUDE -88.86584	15 75	
COUNTY Massac API 121272103900	15 - 15	a - 36

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Irrigation Well	Тор	Bottom
yellow clay	0	27
gravel	27	21
white clay	28	36
yellow sandy clay/gravel	36	58
yellow sandy clay/coarse ylw sand	58	6
yellow sandy clay/white streaks	65	10
fine yellow sand & clay streaks	105	11
chert .	118	14:
chert w/yellow/white clay streaks	142	16
chert w/gravel clay streaks	160	17
weathered limestone	178	18
chert w/gray clay	180	19
fractured gray limestone	191	20
Total Depth Casing: 6.12" PVC from -1' to 140' 4" PVC from 135' to 195' Grout: BENTONITE from 0 to 139.		20:
Water from limestone at 175' to 200'. Static level 41' below casing top which is 1' above GL Pumping level 100' when pumping at 15 gpm for 72 hours		
Remarks: driller's est. well yield 30 gpm		
Address of well: same as above		
Location source: Location from permit		
Permit Date: February 8, 2000 Permit #:		
COMPANY Beanland, Ronald D. FARM DATE DRILLED March 30, 2000 NO.		
ELEVATION 0 COUNTY NO. 21030		
LOCATION SE NE SE LATITUDE 37.225712 LONGITUDE -68.858722		

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ILLINOIS STATE GEOLOGICAL SURVEY

Irrigation Well	Тор	Bottom
yellow clay	0	27
gravel	27	28
white clay	28	36
yellow sandy clay with gravel	36	58
yellow sandy clay with coarse yl sand	58	65
yellow sandy clay with white streaks	65	105
fine yellow sand with clay streaks	105	118
chert	118	142
chert with yellow to white clay streaks	142	160
chert with gray clay streaks	160	178
weathered limestone	178	180
chert with gray clay	180	191
fractured gray limestone	191	202
Interpretation by: John Nelson on 07-APR-00 samples are wet and disaggregated		
Loess: silt, medium yellowish brown; less than 1% sand grains.	0	10
Loess: sandy silt, medium yellowish-brown, 5% to 10% fine to medium sand.	10	25
Metropolis Formation: sandy silt, light gray to yellowish-gray, 10 to 20% very fine to fine sand. note on bag says "little gravel at 27 ft."	25	30
Metropolis Formation: sand, light brownish gray, very fine grained (to coarse silt), fluid.	30	35
Metropolis Formation: sandy silt, yellowish-orange to yellowish-brown, a little gray (mottled?), sand fraction very fine to fine, sand increasing downward.	35	45
Permit Date: Permit #:		

API 121272100900

COMPANY Beanland, John R. FARM DATE DRILLED March 28, 2000 NO. 1 ELEVATION 0 COUNTY NO. 21009 LOCATION 1900'S line, 700'E line of section LATITUDE 37.226406 LONGITUDE -88.859969

COUNTY Massac

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ILLINOIS STATE GEOLOGICAL SURVEY

Metropolis Formation: silty sand, dark yellowish brown, some lighter yellow mottling, very fine to fine, clay present.	45	60	
Metropolis Formation: silty sand, mottled light gray, yellowish gray, yellowish orange; otherwise similar to above. mica appears at 75 feet.	60	80	
McNairy Formation: sand, light yellowish to brownish gray, vey fine grained, clean, dominantly quart2 with a little mica.	80	105	
McNairy Formation: sand, medium yellowish brown, very fine to fine-grained, otherwise as above. scattered coarse sand to small granules, mostly dark brown chert (?) appear at 115 feet. clay present at 120-125 feet.		125	
McNairy Formation: sand, brownish gray, poorly sorted, fine to very coarse, composed fo quartz and dull, opaque gray to brown chert. some clay present.	125	130	
Post Creek Formation: sand and fine gravel, a washed sample consists of fine to medium quartz sand and angular fragments of dull, opaque, light to medium gray and brownish-gray chert. matrix is yellowish- brown silt.	130	135	
Post Creek Formation: gravel, composed of broken chert pebbles, fragments of rounded pebbles common. mostly dull, opaque gray to brown chert as above, some light gray and tripolitic, some sand matrix partially cemented with gravel.	135	140	
otal Depth		202	
ample set # 68834 (0' - 140') Received: April 4, 2000 ocation source: Field verified Verified by: WJN on Ap			
			_
eanland, John R.			

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COUNTY Massac

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Stratigraphic Test	Тор	Bottom
Loess	0	10
Metropolis formation	10	59
Unidentified	59	127
McNairy formation	127	328
Post Creek formation	328	359
Salem limestone	359	362
Interpretation by: W. John Nelson on 27-JUL-99 Drilled with USGS Mobile B-61 with Driller: Gene Cobbs.	eline cori	ng rig.
Silt, yellowish brown with orange and gray mottling, massive, slightly clayey, roots at top, scattered organic matter throughout.	.5	5
Silt, similar to above. Only 1' recovered for 5' run.	5	10
Gap (recovered about 6' for the run from 10' to 20').	10	20
Silt and sand, yellowish orange and light to medium gray, strongly mottled, contains scattered chert granules. This silty sand to sandy silt with a clay matrix. Sand consists of fine to very coarse quartz, common red grains, and brown chert granules with Mounds patina. Massive to laminated, laminated, laminations dip 10 to 30 degrees. Gradational contact:	20	26.7
Sandy silt, light gray and yellowish orange, strongly streaked and mottled. Clay-rich, granules rare. No layering, appears brecciated. Irregular contact:	26.7	33.8
Silty sand, gray, brown, and yellowish-orange mottled, much coarse sand to small grainules in a silty clay matrix, granules are largerly well-rounded	33.8	48.2
Permit Date: Permit #:		
COMPANY IL State Geological Survey FARM Maple Grove School DATE DRILLED NO. 2 ELEVATION OGL COUNTY NO. 20963 LOCATION 2575'S line, 600'E line of section LATITUDE 37.228262 LONGITUDE -88.85959		

API 121272096300

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brown chert, reworked Mounds Gravel. Massive to weakly laminated, laminae gently inclined. Sharp contact:		
Gravel, reworked Mounds-type chert pebbles to 1" across supported in matrix of silty sand, as above. Sharp contact:	48.2	48.5
Sand, reddish orange with a little gray mottling, dominantly fine to medium grained but contains scattered coarse sand grains and small brown chert pebbles. No layering. Barely coherent, a little silt and clay matrix. Black laminae in lower part are probably iron/manganese oxides. Grades to:	48.5	50.8
Sand, colors vary, mostly yellowish gray, some layers light gray and reddish gray. Fine grained, well sorted, subrounded to rounded quarts sand, barely coherent, has irregular nearly horizontal silty lamination. Black layers (common at 54' - 55') proably iron/manganese oxide. Thin gravelly layer at 59', rounded quarts granules and small pebbles, also brown chert pebbles that appear to be reworked Mounds. Grades to:	50.8	60
Sand, light gray with small yellowish-orange and black patches, mainly in upper part of unit. Very fine to fine grained, slightly silty, nearly all quartz with a trace of heavy minerals. Slightly coherent, no lamination noted in upper 10'. Below 70' sand has faint planar laminations that dip about 30 degrees. Quartz grains largely rounded to well- rounded. Grades to:	60	79
Sand, light grayish orange, fine grained, otherwise as above. Sharp contact:	79	82.5
Silty sand, light gray with small yellowish orange patches, sand very fine and quartzose, massive, a	82.5	87.5
State Geological Survey Maple Grove	School 2	
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little clay matrix makes the sediment coherent. Grades to:		
Silty clay, light gray, massive, moderately stiff, can be formed into balls. Grades to:	87.5	8
Silty sand, like next-to-last unit. Less silt and clay downward, grades to:	89	94.
Sand, light orange to yellowish gray, very fine to medium, coarser near base, like that at 60' at 82.5'. Grain size and colors vary, some intervals are silty. Rare quartz granules, near base. No mica or caly laminae as would be typical for McNairy. Sharp contact:	94.1	109.
Gravel, composed of subangular to well rounded pebbles to at least 1" across in a sand matrix, with a little clay binder. Pebbles largely light gray, opaque, tripolitic chert. Dark gray chert and silicified limestone (some colitic), white to red quartz pebbles less than 10% of total. Sand medium to coarse, dominantly rounded quartz grains. Mostly gravel-supported. No bedding evident. Only partial recovery; 6' recovered from 110' to 119'.	109.7	11
Gravel, as above? Drilled 9' but recovered only about 1' of gravel, as above. Last 2' was easier drilling, like sand or clay.	119	12
Sand; as below? Not sampled, but drilled like next 11'.	127	12
Sand, light gray to light yellowish gray, fine- grained, dominantly quartz with less than 1% very fine black grains and a few mica flakes. Massive to faintly laminated, weakly coherent (a little clay and silt binder). Basically the same as sands above the gravel. Recovered only 2.5' from 129' to 140', but easy drilling indicates consistent material. Nearly	129	179.
State Geological Survey Maple Grove	School 2 - 155 -	3E

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ILLINOIS STATE GEOLOGICAL SURVEY

complete recovery 140' - 150'; several thin white		
clay laminae in this interval dip 30-40 degrees. Near-vertical clay laminae or veinlets at 150' - 155'. Sharp contact:		
Clayey sand, light to medium gray, very fine grained, silty, laminated; as before the sand is dominantly quartz with less than 1% dark grains and a few mica flakes. Grades to:	179.7	180.9
Sand, upper 2' light gray, changing back to light yellowish or orange-gray, fine-grained, like next-to- last unit. Occasional clay laminae dipping 20-30 degrees. Grades to:	180.9	201
Sand, light gray, very fine to fine grained. As before, dominantly quartz with less than 1% black grains and sparse mica. many laminae and stringers (veinlets) of light gray plastic clay crisscross the core at various angles. The clay contains only scattered mica flakes and is unlike typical McNairy.	201	210.5
Sand, mostly yellowish-orange, some light gray, fine- grained, light gray clay laminae inclined 40-50 degrees.	210.5	213.5
Sand, light gray, fine grained, well sorted, dominantly quartz with silt-sized black grains, barely coherent (slightly silty), uniform, massive.	213.5	237
Sand, light orange to light gray, fine-grained, contains a few steeply dipping light gray clay veinlets, otherwise, as above. Small-scales faulting was visible on freshly extracted sample at about 275' and steeply dipping clay laminae or veins at 300' - 305'. Mica becomes more common downward, but still sparse.	237	304.7
Silty sand, light gray, very fine grained, clayey, slightly micaceous. Dominantly quartz as above.	304.7	320
State Geological Survey Maple Grove	School 2	2

Appears to be riddled with a network of light gray clay laminae. Gradational contact:		
Sandy clay, light gray and yellowish orange, mixture of fine quartz sand and plastic clay, yellowish orange color increases downward. Chert granules in lower 2'.	320	327
Pebbly sand and clay, yellowish orange to brownish orange, mostly granule-size, but some pebbles to 1" of dark gray to brown chert. Indistinct and irregular layering in places.	327	334
Chert, a few large angular fragments of bluish gray slightly translucent chert that is silicified, coarse-grained crinoidal grainstone, probably from bedrock. No sample from about 334' to 340'.	334	340
Pebbly sand and clay, like next-to-last unit. No large chunks of chert recovered. Only about 3' of sample recovered.	340	350
Pebbly sand and clay, as above, about 1.5' recovered for 9' run.	350	359
Limestone, medium to dark gray, coarse crinoid- bryozoan packstone with shaly partings and chert nodules; bryozoan fronds parallel with bedding. Bedding horizontal, probably Salem Limestone.	359	362
Interpretation by: Jack Masters & John Nelson on 04	AUG-99	
Silt, light yellowish brown, uniform color, clayey, sand-size iron-manganese pellets common. Soft, massive.	.5	2
Silt, similar to above but has dinstinct light gray mottling, pellets as above have orange rims. Gray zones are silty clay and appear to be steeply inclined fractures and/or burrows.	2	4.7
L State Geological Survey Maple Grove	School 2	2
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ILLINOIS STATE GEOLOGICAL SURVEY

Silt, medium yellowish brown, faintly mottled, slightly sandy with fine to medium white to pink quartz grains. Faint distorted grayish laminations, darker laminations more clayey. A few chert granules.	4.7	6.1
No sample - recovered 1.1 feet of core between 5' and 10'.	6.1	10
Sandy silt, strongly mottled in gray, brown and yellowish orange, gray zones are clay-rich. Scattered granules and small pebbles of brown chert probably derived from Mounds Gravel. Gradational contact:	10	11.5
Sany silt, strongly mottled in light orange-brown, yellowish gray, and gray. Intermixed silty clay, some of which is clay skins. Irregular lamination in lower part of interval. A few chert granules, as above.	11.5	13.5
Sandy silt and clay, darker than above; clay yellowish brown to gray, silt medium to dark orange- brown, all mottled. Two layers of chert granules and pebbles, as above. No lamination. Large chert pebbles at base.	13.5	15.1
No sample. core loss believed to be in lower 4.9' of interval from 10' to 20', because chert pebbles at base of sample may have plugged core barrel.	15.1	20
Silty sand, mottled orange-brown, sand is medium to coarse, several gray silty clay layers. Weakly layered, chert granules and pebbles (as above) common. Gradational contact:	20	21.4
Sandy silt, colors as above, clay-rich, clayey zones lighter gray to yellowish brown. Thick clay skins abundant. Massive to weakly laminated, stiff. Gradational contact:	21.4	23.4
State Geological Survey Maple Grove	School 2	2

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Sandy silt, mottled light brownish-gray to light brown, coarse silt to fine sand, scattered chert pebbles as above. Massive to weakly layered.	23.4	26.5
Clayey and sandy silt, strongly mottled in light gray and yellowish to brownish orange, sand content increases downward. Gray patches are clay-rich. Probably bioturbated, lower 3' appears brecciated but colors less distinct. Scattered chert granules. Sharp contact:	26.5	33.7
Pebbly sand, coarse to very coarse, dominantly quartz sand with pink grains common, pebbles a mixture of Mounds-type chert and quartz, subrounded to well rounded (quartz pebbles well rounded). Sand has a clay matrix. Sharp contact:	33.7	34.1
Silty sand, light orange-brown with yellowish gray mottling, clayey, contains iron oxide nodules (dark brown) and manganese (black). Pink to rose-colored quartz grains common. Largely bioturbated, a few silty clay laminations. Lower contact sharp.	34.1	39.9
Silty and clay, silt orange to brown, clay light to medium gray, clay and silt intermixed and mottled, no layering. Concentrated black iron/manganese stains near top, along with scattered pebbles (but this could be slop at top of core run). Material appears bioturbated. A hint of lamination. Scattered white to pink, fine to medium quartz sand grains and rare granules. Black iron/manganese stains and pellets common. Sand increases downward. Possible small fault dipping 40-50 degrees at 45.3'. Sharp contact:	39.9	48.2
Sand, pebbly, grayish to orange brown, fine to very coarse sand, dominantly quartz, with clay matrix, abundant shiny brown clay-skins; gravel dominantly reworked Mounds-type chert pebbles, some have patina,	48.2	48.6
State Geological Survey Maple Grove S	School 2	

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out many are bleached, sharp lower contact.		
Sand, red to orange with gray mottling, dominantly fine grain with scattered coarse grains, subrounded to well rounded, trace of muscovite mica, lower 0.5' has distorted banding (maybe liesegang) black iron manganese stains abundant, scattered granules and pebbles of reworked Mounds gravel. Sharp contact:	48.6	50.
Sand, light gray to light yellowish and reddish prange, fine to medium grain-size, almost entirely quartz, slightly silty, more silty at top, some sand nearly loose and water saturated when drilled, faint disturbed laminations, spots and patches of black iron manganese oxide, rare well-rounded quartz granules throughout, basal 0.1' is a concentration of well-rounded granules and small pebbles, of mostly quartz, with some reworked iron oxide and Mounds-type chert.	50.8	58.
Sand, light gray, yellowish orange stains at top diminish below upper 1', to nearly all light gray, nearly 100% quartz, rare pink to red quartz grains, few very fine grain black heavy minerals, upper part is silty, decreses downward to loose, clean sand, grades to fine to medium at base (fining upward interval), gradational contat.	58.8	7
Sand, light grayish orange, fine to medium grain- size, subrounded to rounded quartz, maybe 1% chert and black heavy mineral grains, less well sorted than above, loose (water saturated), contact gradational, possibly smeared out by sampling.	79	8
Sand, silty, light gray, coarse silt to very fine sand intermixed, massive, angular to hackly fractures and clay concentrations suggest paleosol, interval looks bleached, lower contact indistinct.	83	8

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Silt, clayey, medium light gray, massive, fractures more even than above, less paleosol-like than above, very fine sand in lower part and increases downward. Silt and sand interbedded, silt is medium light gray, sand is light gray, very fine grain, all quartz except for few heavies, faint laminations to thin beds inclined 40-60 degrees, gradational contact. Sand, light wellowish gray to grayish orange, very fine to fine grain size, becomes coarser downward with some medium sand in lower 2', mineralogy as above, except maybe 1% chert and heavies in lower 2', sand mostly clean and loose, but contains several silty intervals. Sharp contact: Gravel, light gray, composed mainly of chert pebbles, largest nearly 2" across, subrounded to rounded, light gray, tripolitic chert, few medium to dark gray chert (vitreous to bioclastic texture) granules to small pebbles of white to pink or rose colored chert, matrix fine to very coarse quartz sand with common pink grains, gravel largely grain supported, but some matrix supported intervals. Only 1' of loose gravel in 10' core run. Lower contact based on drilling rate with no recovery, but probably like underlying sand. Sand, light gray and light brownish gray very fine grain, dominantly quartz, but conspicuous mica and silt-size heavies (black), silt and clay lamination is common and coated with mica flakes, sand loose to weakly indurated, less than 3' recovery in 14' or coring (126'-140'), contact with gravel lost. Sand, light yellowish gray, light gray to yellowish orange, fine grain, subrounded to rounded, less than 1% black heavies, scattered mica flakes, loose to		
<pre>more even than above, less paleosol-like than above, very fine sand in lower part and increases downward. Silt and sand interbedded, silt is medium light gray, sand is light gray, very fine grain, all quartz except for few heavies, faint laminations to thin beds inclined 40-60 degrees, gradational contact. Sand, light wellowish gray to grayish orange, very fine to fine grain size, becomes coarser downward with some medium sand in lower 2', mineralogy as above, except maybe 1% chert and heavies in lower 2', sand mostly clean and loose, but contains several silty intervals. Sharp contact: Gravel, light gray, composed mainly of chert pebbles, largest nearly 2" across, subrounded to rounded, light gray, tripolitic chert, few medium to dark gray chert (vitreous to bioclastic texture) granules to small pebbles of white to pink or rose colored chert, matrix fine to very coarse quartz sand with common pink grains, gravel largely grain supported, but some matrix supported intervals. Only 1' of loose gravel in 10' core run. Lower contact based on drilling rate with no recovery, but probably like underlying sand. Sand, light gray and light brownish gray very fine grain, dominantly quartz, but conspicuous mica and silt-size heavies (black), silt and clay lamination is common and coated with mica flakes, sand loose to weakly indurated, less than 3' recovery in 14' or coring (126'-140'), contact with gravt lost. Sand, light yellowish gray, light gray to yellowish orange, fine grain, subrounded to rounded, less than</pre>		
<pre>sand is light gray, very fine grain, all quartz except for few heavies, faint laminations to thin beds inclined 40-60 degrees, gradational contact. Sand, light wellowish gray to grayish orange, very fine to fine grain size, becomes coarser downward with some medium sand in lower 2', mineralogy as above, except maybe 1% chert and heavies in lower 2', sand mostly clean and loose, but contains several silty intervals. Sharp contact: Gravel, light gray, composed mainly of chert pebbles, largest nearly 2" across, subrounded to rounded, light gray, tripolitic chert, few medium to dark gray chert (vitreous to bioclastic texture) granules to small pebbles of white to pink or rose colored chert, matrix fine to very coarse quartz sand with common pink grains, gravel largely grain supported, but some matrix supported intervals. Only 1' of loose gravel in 10' core run. Lower contact based on drilling rate with no recovery, but probably like underlying sand. Sand, light gray and light brownish gray very fine grain, dominantly quartz, but conspicuous mica and silt-size heavies (black), silt and clay lamination is common and coated with mica flakes, sand loose to weakly indurated, less than 3' recovery in 14' or coring (126'-140'), contact with gravel lost. Sand, light yellowish gray, light gray to yellowish orange, fine grain, subrounded to rounded, less than</pre>	88	9
<pre>fine to fine grain size, becomes coarser downward with some medium sand in lower 2', mineralogy as above, except maybe 1% chert and heavies in lower 2', sand mostly clean and loose, but contains several silty intervals. Sharp contact: Gravel, light gray, composed mainly of chert pebbles, largest nearly 2" across, subrounded to rounded, light gray, tripolitic chert, few medium to dark gray chert (vitreous to bioclastic texture) granules to small pebbles of white to pink or rose colored chert, matrix fine to very coarse quartz sand with common pink grains, gravel largely grain supported, but some matrix supported intervals. Only 1' of loose gravel in 10' core run. Lower contact based on drilling rate with no recovery, but probably like underlying sand. Sand, light gray and light brownish gray very fine grain, dominantly quartz, but conspicuous mica and silt-size heavies (black), silt and clay lamination is common and coated with mica flakes, sand loose to weakly indurated, less than 3' recovery in 14' or coring (126'-140'), contact with grave lost. Sand, light yellowish gray, light gray to yellowish orange, fine grain, subrounded to rounded, less than</pre>	90	9
<pre>largest nearly 2" across, subrounded to rounded, light gray, tripolitic chert, few medium to dark gray chert (vitreous to bioclastic texture) granules to small pebbles of white to pink or rose colored chert, matrix fine to very coarse quartz sand with common pink grains, gravel largely grain supported, but some matrix supported intervals. Only 1' of loose gravel in 10' core run. Lower contact based on drilling rate with no recovery, but probably like underlying sand. Sand, light gray and light brownish gray very fine grain, dominantly quartz, but conspicuous mica and silt-size heavies (black), silt and clay lamination is common and coated with mica flakes, sand loose to weakly indurated, less than 3' recovery in 14' or coring (126'-140'), contact with gravel lost. Sand, light yellowish gray, light gray to yellowish orange, fine grain, subrounded to rounded, less than</pre>	93	109.
<pre>grain, dominantly quartz, but conspicuous mica and silt-size heavies (black), silt and clay lamination is common and coated with mica flakes, sand loose to weakly indurated, less than 3' recovery in 14' or coring (126'-140'), contact with gravel lost. Sand, light yellowish gray, light gray to yellowish orange, fine grain, subrounded to rounded, less than</pre>	109.7	12
orange, fine grain, subrounded to rounded, less than	127	14
	140	179.
State Geological Survey Maple Grove Sch	chool 2	

wekaly indurated, some intervals slightly silty, scattered black spots of manganese oxide, local concentrated clay laminations (especially between 150'-153') are steeply inclined.		
Sand, light to medium gray, upper part contains several thin interbeds of light to medium gray plastic clay, otherwise similar to above.	179.6	182.8
Sand, light to medium grayish orange with few light gray streaks. Fine grained like next to last unit, concentrations of black iron-manganese oxides at base.	182.8	201
Sand, light gray and light brownish gray, very fine to fine grain, laminae and veins or stringers of light gray clay at various angles, possible microfault at top of unit, slightly micaceous (more mica than in clean fine-grain sands). Sharp contact:	201	210.8
Sand, yellowish orange with gray layers and veins that are more clayey, probable core loss through this unit, some black iron manganese stained spots.	210.8	215
Sand, light gray, fine grained, sugary texture, loose, well sorted, subround to rounded, +99% quartz, some siltsize black heavies and mica flakes.	215	237.1
Sand, light gray and light grayish orange, colors intermixed, near vertical color and textural boundaries (veins and possible Ophiomorphia).	237.1	239.5
Sand, medium grayish orange, fine to medium grain- size, otherwise like next to last unit.	239.5	251
Sand, light gray to light grayish orange, color intermixed, fine to medium grained, orange portions tend to be a little coarser grained, slightly micaceous, few steeply inclined light gray stringers or veinlets, loose to weakly indurated, gradational	251	280
State Geological Survey Maple Grove	School 2	

contact.

Sand, medium light gray and light brownish grain, 280 304.6 fine grained, more than 99% quartz, many grains sparkly, silt size heavies, mica flakes as above, mostly loose, liquified in core box, possibly little faint laminations in places, fairly sharp contact. Sand, very light gray to gray, very fine laminae of 304.6 320 silty clay, same color as sand, bedding planes lined with mica flakes, inclined 40 degrees plus/minus, gradiation contact. Sand, clayey to sandy clay, light gray and dark 320 328 yellowish brown mottling, more brown toward base, upper half of unit is contorted and broken laminations with blebs of sand cemented by limonite, lower part, structureless mix of sand, silt and clay, with few fragments broken chert, gradational contact. Sand, clay and gravel mixture, dark yellowish to 328 359 orange brown, with a little gray mottling in places, gravel fraction is rounded small pebbles, larger chunks of chert, largely bluish gray, at 334' was very large chunk of such chert, overall look of highly weathered and oxidized, all matrix supported (mud-like), poor core recovery. Limestone, medium to dark gray, coarse bryozoan and 359 362 crinoid wackestone, large fronds of fennestrate bryozoans define bedding, horizontal to gently dipping, numerous partings of dark gray, slightly silty shale, in lower part are nodules of dark gray chert. John Nelson & Jack Masters on 05 AUG-99 Interpretation by: This hole was drilled to investigate an apparent graben indicated by long of school water well and previous shallow ISGS boring (ISGS #1 Maple Grove IL State Geological Survey Maple Grove School 2 COUNTY Massac 10 - 15S - 3E API 121272096300

School).		
Peoria silt	o	4.7
Roxana silt	4.7	6.1
Core loss, may include Loveland silt	6.1	10
Metropolis Formation, silt and sand with much clay and reworked Mounds-type gravel. Laminations appear to dip 10 to 30 degrees in places.	10	58.8
Unidentified strata, about 51' and and minor silt overlying 17' of gravel. Two upward-fining sequences are present. These materials could be as young as Quarternary or as old as Cretaceous, but Eocene to Miocene age appears most likely based on absence of mica in sands (as would be tuypical for Cretaceous) and absence of brown Mounds-type chert pebbles.	58.8	127
McNairy Formation, clean quartz sand, minor silt and clay laminae and interbeds, some of which contain considerable mica. An unusually sandy McNairy section.	127	328
Post Creek Formation, clay and sand mixture, oxidized and weathered, mixed with chert gravel and fragments.	328	359
Salem Limestone, the lithology is fairly typical of this unit.	359	362
Rotal Depth Sore #C 14730 (0' - 10') Received: August 2, 1999 Sore #C 14730 (10' - 59') Received: August 2, 1999 Sore #C 14730 (59' - 127') Received: August 2, 1999 Sore #C 14730 (127' - 328') Received: August 2, 1999 Sore #C 14730 (328' - 359') Received: August 2, 1999 Sore #C 14730 (359' - 362') Received: August 2, 1999 Sore #C 14730 (359' - 362') Received: August 2, 1999		362
L State Geological Survey Maple Grove COUNTY Massac API 121272096300 10	School 2 - 155 -	3E

Electronic Filing: Received, Clerk's Office 11/22/2021 **AS 2021-05** ILLINOIS STATE GEOLOGICAL SURVEY

						Top	Bottom
Total Dept	Ъ						9(
Sample set	# 23753 (5' -	90') Rece	ived:	January	9, 19	952	
						i	
Permit Dat	ê:			Permit	# =		
COMPANY	Layne Western	<u> </u>			<u> </u>		
FARM	- Tinsteinel Te		(Jopp	a)			
DATE DRIL	LED			NO. 3			
ELEVATION	1 0	cc	UNTY	NO. 209	42		
LOCATION	37.204248	LONGT	אמווי	-88.8487	9		
COUNTY		API					155 - 3E

	Тор	Bottom
Total Depth		169
Core #C 4292 (145.5' - 149') Received: March 5, 196	:2	
Core #C 4292 (154' - 169') Received: March 5, 1962		
Permit Date: Permit #:		
COMPANY Layne Western		
FARM Missouri Portland Cement T.H.		
DATE DRILLED NO. 61-9(62	2)	
ELEVATION 0 COUNTY NO. 20934		
LOCATION 825'N 325'E SW/C NW		
LATITUDE 37.216334 LONGITUDE -88.875329		
COUNTY Massac API 121272093400	15 - 1	

Electronic Filing: Received, Clerk's Office 11/22/2021 **AS 2021-05** ILLINOIS STATE GEOLOGICAL SURVEY

						Тор	Bottom
Total Depth							105
Sample set	# 4192 0 (0' - 105	') Rece	ived:	March 5,	1962		
							ĺ
					ļ		
Permit Date	:			Permit #	:		
COMPANY	Layne Western		_				
FARM	Missouri Portland	d Cement	т.н.				
DATE DRILI	ED			10. 61-9(
ELEVATION			NTY N	O. 20933			
	825'N 325'E SW/c 37.216334	NW LONGITU	- ਸ	18.875329	1		
COUNTY I				7209330		15 - 1	

Page 1

Page 1

			Тор	Bottom
Total Dept	h			105
Sample set	# 41919 (O' -	105') Received: March 5	, 1962	
			ļ	
Permit Dat	e:	Permit	#:	
COMPANY	Layne Western			·
FARM	Missouri Port	land Cement T.H.		
DATE DRII	LLED	NO. 61-6		
BLEVATION	10	COUNTY NO. 2093	30	
	335'N 500'E S			
	37.214973			58 - 3E
COUNTY	Massac	API 1212720930	100 13 - 1	

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Page 1

			Тор	Bottom
Total Dept	h			138
Sample set	# 41921 (0' - 138') Received:	March 5, 1962		
-				
				1
Permit Dat	. .	Permit #:		
- JAL DAL		ESLULL ¶I	<u> </u>	<u> </u>
COMPANY	Layne Western			
FARM	Missouri Portland Cement T.H.			
DATE DRII		O. 61-7(62)		
ELEVATION	COUNTY N	0. 20929		
	570'N 740'E SW/c NW			
	37.215609 LONGITUDE -8	8.873938		<u>_</u>
	Massac API 1212		15 - 15	

ILLINOIS STATE GEOLOGICAL SURVEY

	Тор	Bottom
Total Depth		13
Sample set # 41922 (0' - 130') Received: March 5, 1962	:	
Permit Date: Permit #:		
COMPANY Layne Western FARM Missouri Portland Cement T.H.		
DATE DRILLED NO. 61-4		
ELEVATION 0 COUNTY NO. 20928		
LOCATION 442'N 395'E SW/c NW LATITUDE 37.215273 LONGITUDE -88.875145		
COUNTY Massac API 121272092800	15 - 19	55 - 3

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	Тор	Bottom
Total Depth		110
Sample set # 41685 (0' - 110') Received: December 20,	1961	
Permit Date: Permit #:		
COMPANY Layne Western		
FARM Missouri Portland Cement Co		
DATE DRILLED NO. 5		
ELEVATION 0 COUNTY NO. 20927		
LOCATION 173'N 288'E SW/c NW LATITUDE 37.214536 LONGITUDE -88.875555		
COUNTY Massac API 121272092700	15 - 15	S - 3E

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	Тор	Botte
Total Depth		:
Sample set # 41556 (0' - 136') Received: November 22,	1961	
Permit Date: Permit #:		
COMPANY Layne Western FARM Missouri Portland Cement Co		
DATE DRILLED NO. 2		
ELEVATION 0 COUNTY NO. 20926		
LOCATION 512'N 40'E SW/c NW LATITUDE 37.215484 LONGITUDE -88.876362		
		55 -

Electronic Filing: Received, Clerk's Office 11/22/2021 **AS 2021-05** ILLINOIS STATE GEOLOGICAL SURVEY

	Top	Bottom
Total Depth		451
Sample set # 41557 (160' - 451') Received: November	22, 1961	
Permit Date: Permit #:		
COMPANY Layne Western		
FARM Missouri Portland Cement Co		
DATE DRILLED NO. 1		
ELEVATION0COUNTY NO. 20919LOCATION489'N 143'E SW/c NW		
LATITUDE 37.215416 LONGITUDE -88.876007		
COUNTY Massac API 121272091900	15 - 1	5S - 3E

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	Тор	Bottom
topsoil	0	
brown clay	5	39
fine sand with gray clay	35	69
sand & gravel	65	98
Total Depth Casing: 16" STEEL 62.58#/FT from -2' to 72' 16" STNLESS STL SCREEN from 72' to 97' Screen: 2' of 16" diameter 80 slot Grout: CEMENT from 2 to 20.		98
Size hole below casing: 48"		
Water from sand & gravel at 72' to 97'. Static level 48' below casing top which is 2' above GL Pumping level 71' when pumping at 0 gpm for 8 hours Permanent pump installed at 90' on August 12, 1997, wi capacity of 325 gpm Address of well: same as above Location source: Location from permit		
Permit Date: July 8, 1997 Permit #:		
COMPANYStollhans, JeffFARMLafarge Corp.DATE DRILLED July 21, 1997NO. 5ELEVATION 0COUNTY NO. 20856LOCATIONNE NW SWLATITUDE37.213209LONGITUDE -88.873085		

COUNTY Massac

Stratigraphi	c Test	Тор	Bottom
Cotal Depth Core #C 14531 Core #C 14533 Core #C 14533 Core #C 14533 Core #C 14533	<pre>c Test (0' - 6.2') Received: August 25, 1997 (6.2' - 11') Received: August 25, 1997 (11' - 16') Received: August 25, 1997 (16' - 38.1') Received: August 25, 1997 (38.1' - 76') Received: August 25, 1997</pre>		Bottom
COMPANY T	Permit #:		
	L State Geological Survey aple Grove School		
	D NO. J-1		
DATE DRILLE			
DATE DRILLE ELEVATION 0	COUNTY NO. 20851		

API 121272085100

10 - 15S - 3E

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Private Water Well	Тор	Bottom
clay	0	76
sandy clay & yellow sand	76	120
gray clay	120	145
gray clay & sand	145	210
chert	210	280
Total Depth Casing: 6" PVC SDR 21 from -1' to 235' Grout: BENTONITE from 0 to 230.		280
Water from chert at 265' to 280'. Static level 120' below casing top which is 1' above GI Pumping level 160' when pumping at 12 gpm for 72 hours Permanent pump installed at 200' on February 10, 1996, Remarks: Well not completed at there of 7 gpm Location source: Location from permit		
incation source. Incation from permit		
· · · ·		
Permit Date: October 12, 1995 Permit #:		•
COMPANY Beanland, Ronald D.		
FARM		
DATE DRILLED November 10, 1995 NO.		
ELEVATION 0 COUNTY NO. 20699		
LOCATION NW NE NE		
LATITUDE 37.234715 LONGITUDE -88.842652		لين لي
COUNTY Massac API 121272069900	11 - 15	S - 3E

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Private Water Well	Тор	Bottom
lirt & clay	0	18
clay & scapstone	18	72
Drown pea gravel	72	94
Total Depth Casing: 6" SDR 21 from -1' to 88' 6" PVC SCREEN from 88' to 94' Screen: 6' of 6" diameter .02 slot Grout: BENSEAL/SLRY from 0 to 72. Grout: GRAVEL PACK from 72 to 94.		94
Size hole below casing: 6"		
Water from gravel at 85' to 94'. Static level 52' below casing top which is 1' above GL Pumping level 70' when pumping at 0 gpm for 24 hours Permanent pump installed at 80' on October 21, 1994, w: capacity of 10 gpm Address of well: Joppa, IL Location source: Location from permit	ith a	
Permit Date: October 7, 1994 Permit #:	I	
COMPANY Beanland, Leonard Ralph FARM DATE DRILLED October 9, 1994 NO. ELEVATION 0 COUNTY NO. 20675 LOCATION NE SE SW LATITUDE 37.223763 LONGITUDE -88.84962		

Page 1

light brown clay0dark brown clay10gray clay25gray k brown clay40brown fine sdy till55coarse sand & gravel60	Industrial Water Well	Тор	Bottom
dark brown clay10gray clay25gray & brown clay40brown fine sdy till55coarse sand & gravel60for street60for street60for street62.58LB from 0' to 20' 16" street11Casing:42" Streetfor street51.04Grout:READY MIX from 0 to 20.Size hole below casing:42"Water from alluvial at 71' to 94'.Static level 52' below casing top which is 3' above GLPumping level 62' when pumping at 300 gpm for 4 hoursPermanent pump installed at 65' on April 4, 1985, with a capacity of 300 gpmSample set # 64975 (0' - 105')	SS #64975 (0'-105')	0	
gray clay25gray & brown clay40brown fine sdy till55coarse sand & gravel60Total Depth60Casing:42" STEEL 166.71 LB from 0' to 20' 16" STEEL 62.58 LB from -3' to 71'Screen:25' of 16" diameter 5 slotGrout:READY MIX from 0 to 20.Size hole below casing:42"Water from alluvial at 71' to 94'.Static level 52' below casing top which is 3' above GL Pumping level 62' when pumping at 300 gpm for 4 hoursPermanent pump installed at 65' on April 4, 1985, with a capacity of 300 gpmSample set # 64975 (0' - 105')	light brown clay	0	1
gray & brown clay40brown fine sdy till55coarse sand & gravel60coarse sand & gravel60Total Depth11Casing:42" STEEL 166.71 LB from 0' to 20' 16" STEEL 62.58 LB from -3' to 71'Screen:25' of 16" diameter 5 slotGrout:READY MIX from 0 to 20.Size hole below casing:42"Water from alluvial at 71' to 94'.Static level 52' below casing top which is 3' above GLPumping level 62' when pumping at 300 gpm for 4 hoursPermanent pump installed at 65' on April 4, 1985, with a capacity of 300 gpmSample set # 64975 (0' - 105')	dark brown clay	10	2
brown fine sdy till 55 6 coarse sand & gravel 60 9 Total Depth 60 11 Casing: 42" STEEL 166.71 LB from 0' to 20' 16" STEEL 62.58 LB from -3' to 71' Screen: 25' of 16" diameter 5 slot Grout: READY MIX from 0 to 20. Size hole below casing: 42" Water from alluvial at 71' to 94'. Static level 52' below casing top which is 3' above GL Pumping level 62' when pumping at 300 gpm for 4 hours Permanent pump installed at 65' on April 4, 1985, with a capacity of 300 gpm Sample set # 64975 (0' - 105')	gray clay	25	4
coarse sand & gravel60Total Depth11Casing:42" STEEL 166.71 LB from 0' to 20' 16" STEEL 62.58 LB from -3' to 71'Screen:25' of 16" diameter 5 slotGrout:READY MIX from 0 to 20.Size hole below casing:42"Water from alluvial at 71' to 94'.Static level 52' below casing top which is 3' above GLPumping level 62' when pumping at 300 gpm for 4 hoursPermanent pump installed at 65' on April 4, 1985, with a capacity of 300 gpmSample set # 64975 (0' - 105')	gray & brown clay	40	5
Total Depth Casing: 42" STEEL 166.71 LB from 0' to 20' 16" STEEL 62.58 LB from -3' to 71' Screen: 25' of 16" diameter 5 slot Grout: READY MIX from 0 to 20. Size hole below casing: 42" Water from alluvial at 71' to 94'. Static level 52' below casing top which is 3' above GL Pumping level 62' when pumping at 300 gpm for 4 hours Permanent pump installed at 65' on April 4, 1985, with a capacity of 300 gpm Sample set # 64975 (0' - 105')	prown fine sdy till	55	6
Casing: 42" STEEL 166.71 LB from 0' to 20' 16" STEEL 62.58 LB from -3' to 71' Screen: 25' of 16" diameter 5 slot Grout: READY MIX from 0 to 20. Size hole below casing: 42" Water from alluvial at 71' to 94'. Static level 52' below casing top which is 3' above GL Pumping level 62' when pumping at 300 gpm for 4 hours Permanent pump installed at 65' on April 4, 1985, with a capacity of 300 gpm Sample set # 64975 (0' - 105')	coarse sand & gravel	60	9
	Casing: 42" STEEL 166.71 LB from 0' to 20' 16" STEEL 62.58 LB from -3' to 71' Screen: 25' of 16" diameter 5 slot Grout: READY MIX from 0 to 20. Size hole below casing: 42" Water from alluvial at 71' to 94'. Static level 52' below casing top which is 3' above GL Pumping level 62' when pumping at 300 gpm for 4 hours Permanent pump installed at 65' on April 4, 1985, with of 300 gpm Sample set # 64975 (0' - 105')	a capacity	11

Test Hole	Тор	Bottom
SS #64976 (0'-95')	O	
light brown clay	0	5
brown clay	5	25
gray clay	25	40
drk brn cl w/fine s	40	50
brn fine sand & gvl	50	65
coarse sand & gravel	65	75
fine to medium sand	75	80
coarse sand & gravel	80	95
fine sand	95	110
Total Depth Size hole below casing: 0"		110
Remarks: test hole for fm spls.sealed w/bentonite Sample set # 64976 (0' - 95') Received: March 5, 1985 Location source: Location from permit		
Permit Date: December 21, 1984 Permit #: 116	252	
COMPANY Ruester, John T.		
FARM Missouri Portland Cement Co.		

FARM Missouri Port	land Cement Co.	
DATE DRILLED January 3,	1985 NO.	
ELEVATION 0	COUNTY NO. 20519	
LOCATION 1800'N line,	700'W line of section	
LATITUDE 37.216462	LONGITUDE -88.874027	
COUNTY Massac	API 121272051900	15 - 15S - 3E

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Household - Livestock Watering Well	Тор	Bottom
clay	0	21
clay & fine sand	21	150
chert	150	175
Total Depth Casing: 6" FVC SDR-21 from -1' to 174' Grout: BENTONITE/SAND from 0 to 160.		175
		,
Size hole below casing: 0" Water from chert at 165' to 174'. Static level 50' below casing top which is 1' above GL Pumping level 90' when pumping at 20 gpm for 2 hours Permanent pump installed at 120' on May 16, 1987, with a of 20 gpm	a capacity	
Address of well: R.R. Joppa, IL		
Permit Date: April 23, 1987 Permit #: 13:	Ú156	
COMPANY Beanland, Ronald D. FARM NO. DATE DRILLED May 15, 1987 NO. ELEVATION COUNTY NO. 20471 LOCATION NE SE NW LATITUDE 37.231377 LONGITUDE -88.867889		
COUNTY Massac API 121272047100	10 - 15	S - 3E

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Water Well	Top Bottom
Total Depth	52
Driller's Log filed	
•	
Permit Date: Permit #	
COMPANY Horman, Paul	
FARM	
DATE DRILLED October 1, 1976 NO. 1	
ELEVATION 0 COUNTY NO. 20255	
LOCATION SW SE SW	
LATITUDE 37.222274 LONGITUDE -88.870363	
	0 10 - 15S - 3E

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Water Well	<u> </u>	Top	Bottom
Total Depth			11
Driller's Log filed			
			1
			1
		1	
· .			
Permit Date:	Permit #:	 	
COMPANY Luhr Broth			
FARM Mo Portland			
DATE DRILLED Septembe			
ELEVATION 355GL	COUNTY NO. 20220		
LOCATION 2220'N lin			
LATITUDE 37.215316	LONGITUDE -88.874782 API 121272022000	15 - 1!	
COUNTY Massac			

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ILLINOIS STATE GEOLOGICAL SURVEY

Water Well	Тор	Bottom
urface red clay	o	20
ig, red gravel	20	70
andy clay	70	120
ry sand	120	135
lue clay, dark	135	270
roken limerock	270	280
imerock	280	283
Cotal Depth Casing: 6" STEEL 20# from 0' to 280'		283
rout: DRILL CUTTINGS from 0 to 40.		
ize hole below casing: 6"		
Nater from broken lime at 280' to 283'. Static level 135' below casing top which is 1' above GL Pumping level 160' when pumping at 15 gpm for 4 hours		
Driller's Log filed Location source: Location from permit		
Permit Date: January 24, 1973 Permit #: NF		
COMPANY Horman, Paul FARM DATE DRILLED February 7, 1973 NO. 1 ELEVATION 0 COUNTY NO. 00198		
LOCATION NE NE SE LATITUDE 37.22736 LONGITUDE -88.840461		

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Water Well		Тор	Bottom
Total Depth			160
Driller's Log filed			
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			,
Permit Date:	Permit #:		ļ
COMPANY Geer, Alonzo			
FARM			
DATE DRILLED July 1, 1971	NO. 1		
ELEVATION 0	COUNTY NO. 00158		
LOCATION NW NW NE			
	LONGITUDE -88.847389		
COUNTY Massac	API 121270015800	14 - 1	5S - 3E

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Water Well				Top	Bottom
lay				0	20
ravel				20	130
and				130	150
-	7" NEW STEEL 2		0' to 104'		150
	elow casing: 6				
tatic leve	sand gravel at 1 60' below ca: el 100' when p	sing top whi			
ermanent p	ump installed	at 120' on ,	with a capac	ity of 15 gpm	
Driller's L	-	-			
ocation so	urce: Location	from permit	2		
	,				
Permit Date	:		Permit	#: 12094	
COMPANY	Sergent, Will	iam E.			
FARM	Kapley, Homer				
DATE DRIL	• -		NO.1		
ELEVATION		COL	NTY NO. 0014	6	
LOCATION					
LATITUDE		LONGITU	DE -88.84051	18	

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ellow clay 11 26 ravel 26 31 andy clay 38 45 ravel & sand 45 78 otal Depth 24" CONCRETE from 78' to 30' 78 rout: TILE 24" from 78 to 30. 78 rout: TILE 24" from 78 to 30. 78 rout: FVC 6" from 30 to -2. 78 atter from gravel & sand at 58' to 78'. 78 tatic level 20' below casing top which is 2' above GL 78 umping level 15' when pumping at 10 gpm for 1 hour 78 writler's Log filed 50 socation source: Location from permit 50 COMPANY Jennings, James E. 11 FARM 78 DATE DRILLED August 21, 1969 NO. 19 ELEVATION 0 COUNTY NO. 00111 LOCATION 50'N 60'W SE/c NE SE SW 10001110E -88.848699	Water Well	Тор	Bottom
ravel 26 31 andy clay 31 38 ravel & sand 38 45 otal Depth 78 78 daring: 6" PVC from 30' to -2' 78 coult FUC 6" from 30 to -2. 78 atter from gravel & sand at 58' to 78'. 78 tatic level 20' below casing top which is 2' above GL 78 umping level 15' when pumping at 10 gpm for 1 hour 78 bocation source: Location from permit 78 cortine suggist 11, 1969 Permit #: 06803 COMPANY Jennings, James E. FAR Country Mo. 00111 LOCATION 0 COUNTY NO. 00111 LOCATION 50'N 60'W SE/c NE SE SM 11 - 155 - 3E LATITUDE 37.222994 LONGITUDE -88.848699 COUNTY Massac API 121270011100 11 - 155 - 3E	oil	0	11
ellow clay 31 38 andy clay 31 38 ravel & sand 38 45 otal Depth 78 78 dains: 6" PVC from 30' to -2' 78 could bepth 78 78 rout: TILE 24" from 78 to 30. 78 rout: PVC 6" from 30 to -2. 31 ater from gravel & sand at 58' to 78'. 31 tatic level 20' below casing top which is 2' above GL 78 umping level 15' when pumping at 10 gpm for 1 hour 9 briller's Log filed 50 socation source: Location from permit 50 COMPANY Jennings, James E. 78 FAR 51 DATE DRILLED August 21, 1969 NO. 19 ELEVATION 0 COUNTY NO. 00111 LOCATION 50'N 60'W SE/C NE SE SM 10 LATITUDE 37.222994 LONGITUDE -88.848699 COUNTY Massac API 121270011100 11 - 155 - 3E	ellow clay	11	26
andy clay 38 45 ravel & sand 38 45 otal Depth 78 78 asing: 6" PVC from 30' to -2' 24" CONCRETE from 78' to 30' 78 rout: TILE 24" from 76 to 30. 78 78 rout: PVC 6" from 30 to -2. 300 78 ater from gravel & sand at 58' to 78'. 300 78 upping level 15' when pumping at 10 gpm for 1 hour 97 100 wriller's Log filed 38 45 occation source: Location from permit 97 100 company Jennings, James E. 98 98 FARM 100 100 100 DATE DRILLED August 21, 1969 NO. 19 100 ELEVATION 0 COUNTY NO. 00111 100 LOCATION 50'N 60'W SE/c NE SE SW 100 11 - 155 - 3E COUNTY Massac API 121270011100 11 - 155 - 3E	ravel	26	31
ravel & sand 45 78 otal Depth 78 78 fasing: 6" PVC from 30 to -2'. 78 rout: TILE 24" from 78 to 30. rout: TILE 24" from 30 to -2. 78 ater from gravel & sand at 58' to 78'. 1 1 tatic level 20' below casing top which is 2' above GL 78 wight level 15' when pumping at 10 gpm for 1 hour 78 wriller's Log filed 50 from permit cocation source: Location from permit 78 commit Date: August 11, 1969 Permit #: 06803 COMPANY Jennings, James E. FAR PAR DRILLED August 21, 1969 NO. 19 ELEVATION 0 COUNTY NO. 00111 LOCATION 50'N 60'W SE/c NE SE SW LATITODE 3'. 22294 LONGTIUDE -88.848699 COUNTY Massac API 121270011100 11 - 15S - 3E	ellow clay	31	38
otal Depth 78 dasing: 6" PVC from 30' to -2' 24" CONCRETE from 78' to 30' 78 rout: TILE 24" from 78 to 30. 78 rout: PVC 6" from 30 to -2. attrict level 20' below casing top which is 2' above GL 78 attrict level 20' below casing top which is 2' above GL attrict level 20' below casing top which is 2' above GL 78 wmping level 15' when pumping at 10 gpm for 1 hour priller's Log filed 78 ocation source: Location from permit 78 Permit Date: August 11, 1969 Permit #: 06803 COMPANY Jennings, James E. FARM 10 DATE DRILLED August 21, 1969 NO. 19 10 10 DATE DRILLED August 21, 1969 NO. 19 10 10 LOCATION 0 COUNTY NO. 00111 10 10 LOCATION 50'N 60'W SE/c NE SE SW LONGITUDE -88.848699 11 - 15S - 3E COUNTY Massac API 121270011100 11 - 15S - 3E	andy clay	38	45
Rasing: 6" PVC from 30' to -2' 24" CONCRETE from 78' to 30' rout: TILE 24" from 78 to 30. rout: PVC 6" from 30 to -2. Sater from gravel & sand at 58' to 78'. tatic level 20' below casing top which is 2' above GL umping level 15' when pumping at 10 gpm for 1 hour briller's Log filed location source: Location from permit Driller's Log filed location source: Location from permit COMPANY Jennings, James E. FARM Parmit Date: August 11, 1969 Permit #: 06803 COMPANY Jennings, James E. FARM Date DRILLED August 21, 1969 NO. 19 ELEVATION 0 COUNTY NO. 00111 LOCATION 50'N 60'W SE/c NE SE SW LATITUDE 37.222994 LONGITUDE -88.848699 COUNTY Massac API 121270011100 11 - 15S - 3E	ravel & sand	45	78
rout: PVC 6" from 30 to -2. Atter from gravel & sand at 58' to 78'. tatic level 20' below casing top which is 2' above GL umping level 15' when pumping at 10 gpm for 1 hour briller's Log filed cocation source: Location from permit briller's Log filed cocation source: Location from permit Permit #: 06603 COMPANY Jennings, James E. FARM Jennings, James F. FARM Jennings, James F. FARM Jennings, James F. FARM Jennings,			78
Atter from gravel & sand at 58' to 78'. tatic level 20' below casing top which is 2' above GL umping level 15' when pumping at 10 gpm for 1 hour briller's Log filed occation source: Location from permit company Jennings, James E. FARM DATE DRILLED August 21, 1969 NO. 19 ELEVATION 0 COUNTY Massac COUNTY Massac	Frout: TILE 24" from 78 to 30.		
Permit Date: August 11, 1969 Permit Date: August 11, 1969 Permit #: 06803 COMPANY Jennings, James E. FARM DATE DRILLED August 21, 1969 DATE DRILLED August 21, 1969 DATE DRILLED August 21, 1969 DATE DRILLED August 21, 1969 DATE DRILLED August 21, 1969 COUNTY NO. 00111 LOCATION 0 COUNTY NO. 00111 LOCATION 50'N 60'W SE/c NE SE SW LATITUDE 37.222994 LONGITUDE -88.848699 COUNTY Massac API 121270011100 11 - 15S - 3E	later from gravel & sand at 58' to 78'.		
COMPANY Jennings, James E. FARM DATE DRILLED August 21, 1969 NO. 19 ELEVATION 0 COUNTY NO. 00111 LOCATION 50'N 60'W SE/c NE SE SW LATITUDE 37.222994 LONGITUDE -88.848699 COUNTY Massac API 121270011100 11 - 15S - 3E	Driller's Log filed Socation source: Location from permit		
COMPANY Jennings, James E. FARM DATE DRILLED August 21, 1969 NO. 19 ELEVATION 0 COUNTY NO. 00111 LOCATION 50'N 60'W SE/c NE SE SW LATITUDE 37.222994 LONGITUDE -88.848699 COUNTY Massac API 121270011100 11 - 15S - 3E			
COMPANY Jennings, James E. FARM DATE DRILLED August 21, 1969 NO. 19 ELEVATION 0 COUNTY NO. 00111 LOCATION 50'N 60'W SE/c NE SE SW LATITUDE 37.222994 LONGITUDE -88.848699 COUNTY Massac API 121270011100 11 - 15S - 3E			
COMPANY Jennings, James E. FARM DATE DRILLED August 21, 1969 NO. 19 ELEVATION 0 COUNTY NO. 00111 LOCATION 50'N 60'W SE/c NE SE SW LATITUDE 37.222994 LONGITUDE -88.848699 COUNTY Massac API 121270011100 11 - 15S - 3E			
COMPANY Jennings, James E. FARM DATE DRILLED August 21, 1969 NO. 19 ELEVATION 0 COUNTY NO. 00111 LOCATION 50'N 60'W SE/c NE SE SW LATITUDE 37.222994 LONGITUDE -88.848699 COUNTY Massac API 121270011100 11 - 15S - 3E			
COMPANY Jennings, James E. FARM DATE DRILLED August 21, 1969 NO. 19 ELEVATION 0 COUNTY NO. 00111 LOCATION 50'N 60'W SE/c NE SE SW LATITUDE 37.222994 LONGITUDE -88.848699 COUNTY Massac API 121270011100 11 - 15S - 3E			
COMPANY Jennings, James E. FARM DATE DRILLED August 21, 1969 NO. 19 ELEVATION 0 COUNTY NO. 00111 LOCATION 50'N 60'W SE/c NE SE SW LATITUDE 37.222994 LONGITUDE -88.848699 COUNTY Massac API 121270011100 11 - 15S - 3E			
COMPANY Jennings, James E. FARM DATE DRILLED August 21, 1969 NO. 19 ELEVATION 0 COUNTY NO. 00111 LOCATION 50'N 60'W SE/c NE SE SW LATITUDE 37.222994 LONGITUDE -88.848699 COUNTY Massac API 121270011100 11 - 15S - 3E	Permit Date: August 11 1969 Permit #: 0	6803	
FARM Image: Constraint of the second sec			
LOCATION 50'N 60'W SE/C NE SE SW LATITUDE 37.222994 LONGITUDE -88.848699 COUNTY Massac API 121270011100 11 - 15S - 3E	FARM		
LATITUDE 37.222994 LONGITUDE -88.848699 COUNTY Massac API 121270011100 11 - 15S - 3E	EDEVRIION 5		
	COUNTY Massac API 121270011100	11 - 1	5S - 3E

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= Water Well Тор Bottom 65 Total Depth Driller's Log filed Survey Sample Study filed Sample set # 6595 (1' - 65') Received: September 25, 1941 Permit Date: Permit #: Smith & Cunningham COMPANY FARM DATE DRILLED January 1, 1941 NO. 1 COUNTY NO. 00055 ELEVATION 340GL LOCATION LONGITUDE -88.84879 LATITUDE 37.204248 API 121270005500 23 - 155 - 3E COUNTY Massac

Electronic Filing: Received, Clerk's Office 11/22/2021 **AS 2021-05**

ILLINOIS STATE GEOLOGICAL SURVEY

Water Well	L			Тор	Bottom
	log filed ple Study filed) Decoived	June 20 - 70	10	137
sampie set	# 4671 (O' - 137') Received:	June 20, 194	10	
Permit Date	ð:		Permit #:		
COMPANY	Smith & Cunningh	am			
FARM	Joppa Colored Sc				
DATE DRIL	LED June 1, 1940		NO. 1		
ELEVATION			NO. 00054		
LOCATION	500'N line, 600' 37.205054	E line of NW LONGITUDE			
COINTY	Massac	APT 12	1270005400	23 - 1	5S - 3B

Electronic Filing: Received, Clerk's Office 11/22/2021 **AS 2021-05** **ILLINOIS STATE GEOLOGICAL SURVEY**

Water Well	Тор	Bottom
otal Depth Driller's Log filed		23!
ample set # 21218 (0' - 235') Received: July 11, 19	51	
ermit Date: Permit #:		
COMPANY Layne Western Co., Inc.		
ARM Electric Energy Inc		
DATE DRILLED January 1, 1951 NO. 1		
COUNTY NO. 00053		
OCATION 675'N line, 400'E line of NE SE		
ATITUDE 37.211974 LONGITUDE -88.859164		<u>, ;] ;</u>
COUNTY Massac API 121270005300	15 - 1	5S - 3E

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AS 2021-05

Water Wel	.1		Тор	Bottom
Survey Sam	ch Log filed mple Study filed : # 4599 (5' - 138') F	eceived: June 4, 1940		138
Permit Dat	- . .	Permit #:		

COUNTY NO. 00052

ELEVATION 340GL

COUNTY Massac

LOCATION 1000'N line, 1150'W line of SE

LATITUDE 37.21092 LONGITUDE -88.8447

14 - 155 - 3E API 121270005200

Electronic Filing: Received, Clerk's Office 11/22/2021 **AS 2021-05** ILLINOIS STATE GEOLOGICAL SURVEY

Water Well	Тор	Bottom
Cotal Depth Driller's Log filed Survey Sample Study filed		403
Sample set # 21445 (0' - 405') Received: January 9,	1951	
		1
		1
Permit Date: Permit #:		
COMPANY Layne Western Co., Inc.		
ARM Electric Energy Inc		
ATE DRILLED January 1, 1951 NO. 3		
LEVATION 355GL COUNTY NO. 00051		
OCATION 2352'N line, 2088'E line of NE	<u> </u>	
ATITUDE 37.214512 LONGITUDE -88.84669		
	14 - 1	

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ILLINOIS STATE GEOLOGICAL SURVEY

Water Well	Тор	Bottom
Fotal Depth		350
Driller's Log filed		
Survey Sample Study filed		
Sample set # 21219 (0' - 350') Received: January 9, 1	951	
		1
		ļ
Permit Date: Permit #:		
	·	·
COMPANY Layne Western Co., Inc.		
FARM Electric Enrgy Inc		
DATE DRILLED January 1, 1951 NO. 2		
ELEVATION 0 COUNTY NO. 00050		
LOCATION 910'N line, 660'W line of NW SW		
LATITUDE 37.211275 LONGITUDE -88.855516		
COUNTY Massac API 121270005000	14 - 15	S _ 3R

Water Wel	1					_	Тор	Bottom
Total Dept Driller's	Log filed							166
_	ple Study filed # 20885 (0' - 166	') Rece	eived: .	July	11, 1	950		
						ļ		
								Ì
Permit Dat	e:			Perm	Lt #:		-	
COMPANY	Layne Western Co	., Inc.						
FARM	Joppa Compressor							
	LED October 1, 199		N NTY N	0.2 0.00	049			
	500'S line, 2200		of SE					
COUNTY	Massac		12127				10 - 15	S - 38

ILLINOIS STATE GEOLOGICAL SURVEY

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Water Well		Тор	Bottom
Total Depth Survey Sample Study filed Driller's Log filed			150
Sample set # 20884 (0' - 150') Received: July 1	1, 1950		
· · ·			ľ
			1
]	
			P.
Permit Date: Permi	t #:	l	
COMPANY Layne Western Co., Inc.			
FARM Joppa Compressor Station #7			
DATE DRILLED November 1, 1950 NO. 1			
ELEVATION 360GL COUNTY NO. 000	048		
LOCATION 250'S line, 2200'E line of SE	007		
	111		
LATITUDE 37.221953 LONGITUDE -88.865 COUNTY Massac API 121270004		10 10	5S - 3E

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Water Well		Тор	Bottom
Total Depth Driller's Log filed Survey Sample Study filed Sample set # 6594 (1' - 1	56') Received: September 2	5, 1941	156
		-	
Permit Date:	Permit #:		.
COMPANY Smith & Cunni			
FARM			
DATE DRILLED April 1, 1			
ELEVATION 340GL	COUNTY NO. 00031		
LOCATION LATITUDE 37.21372	LONGITUDE -88.848626		
COUNTY Massac	API 121270003100	14 - 1	.5 S - 3 B

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Water Well	Тор	Bottom
Total Depth Driller's Log filed		153
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		Ì
Permit Date: Perm:	it #:	
COMPANY Smith & Cunningham		
FARM		
DATE DRILLED January 1, 1941 NO.		
ELEVATION 0 COUNTY NO. 00	030	
LOCATION SW SW NE LATITUDE 37.214621 LONGITUDE -88.84'	7472	
COUNTY Massac API 12127000		55 - 3E

Electronic Filing: Received, Clerk's Office 11/22/2021 **AS 2021-05** Illinois state geological survey

Water Well	Тор	Bottom
Total Depth Driller's Log filed		140
	Ì	
Permit Date: Permit #:		ļ
COMPANY Layne Western Co., Inc.		
FARM Missouri Prtlnd Cemt		
DATE DRILLED November 1, 1961 NO. 1A		
ELEVATION 355GL COUNTY NO. 00023		
LOCATION NW SW		
LATITUDE 37.21218 LONGITUDE -88.874319 COUNTY Massac API 121270002300	15 _ 15	- -
COUNTY Massac API 121270002300	15 - 15	15 - JE

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Water Well		Тор	Bottom
Total Depth Driller's Log filed Survey Sample Study filed Sample set # 25675 (0' - 304') Receiv	ved: July 29, 1955		304
Permit Date:	Permit #:		
COMPANY Layne Western Co., Inc.			
FARM Bechtel Corp			
DATE DRILLED July 1, 1955	NO. 4		
LOCATION 4400'N line, 275'W line of	TY NO. 00001 section		
LATITUDE 37.208964 LONGITUD	E -88.856879		а <u>на</u> се
COUNTY Massac API 1	L21270000100	14 - 1	5S - 3E

Electronic Filing: Received, Clerk's Office 11/22/2021 MCCOY & MCCOY LABORATORIES, Inc.	Lexington, KY	Pikeville, KY 606.432.3104
	Louisville, KY	Paducah, KY
P.O. Box 907, 825 Industrial Road	502.961.0001	270.444.6547

P.O. Box 907, 825 Industrial Road Madisonville, KY 42431 270.821.7375 www.mccoylabs.com

"Providing Tomorrow's Analytical Capabilites Today"

Report Printed: 02/26/2013 15:34

Certificate of Analysis

Chris Skates Electric Energy Inc P O Box 165 Joppa IL, 62953

Project Name: Process Control Workorder: 3022088

Dear Chris Skates

Enclosed are the analytical results for samples received at the lab on 02/14/2013 15:15.

McCoy & McCoy Laboratories, Inc located in Madisonville, Kentucky is a National Environmental Laboratory Accreditation Program (NELAP) accredited laboratory and as such, certifies that all applicable test results meet the requirements of NELAP.

If you have any questions regarding this certificate of analysis, please contact us at (270) 821-7375.

Please visit us at www.mccoylabs.com for a listing of NELAP accreditations and Scope of Work, as well as other links to Water Quality documentation on the internet.

This laboratory report may not be reproduced, except in full, without the written approval of McCoy & McCoy Laboratories, Inc.



Grett Priz

This page is included as part of the Analytical Report and must be retained as a permanent record thereof.

Brett Davis, Project Manager

Electronic Filing: Received, Clerk's Office 11/22/2021	**AS 2021-05**
McCOY & McCOY	Lexington, KY
LABORATORIES, Inc.	859.299.7775

P.O. Box 907, 825 Industrial Road Madisonville, KY 42431 270.821.7375 www.mccoylabs.com

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 606.432.3104

 Louisville, KY
 Paducah, KY

 502.961.0001
 270.444.6547

Pikeville, KY

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SAMPLE SUMMARY

Lab ID	Client Sample ID/Alias	Matrix	Date Collected	Date Received	Sampled By
3022088-01	Groundwater/Well #1	Wastewater	02/12/2013 12:25	02/14/2013 15:15	Chris Skates
3022088-02	Groundwater/Well #2	Wastewater	02/12/2013 12:40	02/14/2013 15:15	Chris Skates
3022088-03	Groundwater/Well #3	Wastewater	02/12/2013 14:20	02/14/2013 15:15	Chris Skates
3022088-04	Groundwater/Well #4	Wastewater	02/12/2013 13:10	02/14/2013 15:15	Chris Skates

El El	ectroni	c Filin	g: Rece	ived, Clerk'	s Offi	ce 11/22/2	021 **AS 2021-05	5**	
McCO LABOR	1& Y	NCC	ÔΥ	,			Lexington, KY 859.299.7775	Pikeville, KY 606.432.3104	
	AIOF	NES, I	nc.				Louisville, KY	Paducah, KY	
P.O. Box 907, 825 Industrial Ro Madisonville, KY 42431 270.821.7375	ad						502.961.0001	270.444.6547	
www.mccoylabs.com							"Providing Tomorrow's	Analytical Capabilites To:	day"
				ANALYTIC	AL RE	SULTS			
Lab Sample ID: 3022088-01						Sample	Collection Date Time:	02/12/2013 12:25	
Description: Groundwater Well	l #1					Sample	Received Date Time:	02/14/2013 15:15	
Metais by EPA 200 Series Methods									
Analyte	Result	Flag	Units	MRL	MDL	Method	Prepared	Analyzed	Analyst
Boron	ND	11, U	mg/L	0.10	0.10	EPA 200.7	02/18/2013 08:14	02/18/2013 21:31	MLC
Conventional Chemistry Analyses_01									
Analyte	Result	Flag	Units	MRL	MDL	Method	Prepared	Analyzed	Analyst
Sulfate	6		mg/L	1	0.2	EPA 300.0	02/25/2013 18:03	02/25/2013 18:03	DMH
				ANALYTIC	AL RE	SULTS			
Lab Sample ID: 3022088-02							Collection Date Time:	02/12/2013 12:40	
Description: Groundwater Wel	l #2						Received Date Time:		
Metals by EPA 200 Series Methods									
Analyte	Result	Flag	Units	MRL	MDL	Method	Prepared	Analyzed	Analyst
Boron	ND	L1, U	mg/L	0.10	0.10	EPA 200.7	02/18/2013 08:14	02/18/2013 21:42	MLC
Conventional Chemistry Analyses_01									
Analyte	Result	Flag	Units	MRL	MDL	Method	Prepared	Analyzed	Analyst
Sulfate	6		mg/L	1	0.2	EPA 300.0	02/25/2013 18:26	02/25/2013 18:26	DMH
-				ANALYTIC	AL RE	SULTS			
Lab Sample ID: 3022088-03						Sample	Collection Date Time:	02/12/2013 14:20	
Description: Groundwater Wel	II #3					Sample	Received Date Time:	02/14/2013 15:15	
Metals by EPA 200 Series Methods									
Analyte	Result	Flag	Units	MRL	MDL	Method	Prepared	Analyzed	Analyst
Boron	ND	L1, U	mg/L	0.10	0.10	EPA 200.7	02/18/2013 08:14	02/18/2013 21:46	MLC
Conventional Chemistry Analyses_01			-						
Analyte	Result	Flag	Units	MRL	MDL	Method	Prepared	Analyzed	Anatyst
Sulfate	6		mg/L	1	0.2	EPA 300.0	02/25/2013 18:49	02/25/2013 18:49	DMH

	McCOY & LABORATO	ιMo	cCOY	eived, Clerk'	s Offi	ice 11/22/2	2021 **AS 2021-0. Lexington, KY 859.299.7775 Louisville, KY 502.961.0001	5** Pikeville, KY 606.432.3104 Paducah, KY 270.444.6547	
270.821.	ville, KY 42431 7375 oylabs.com						"Providing Tomorrow's	Analytical Capabilites To	day"
				ANALYTICA	LRE	SULTS			
Description	e ID: 3022088-04 1: Groundwater Well #4					•	Collection Date Time: Received Date Time:		
	A 200 Series Methods	I I - - - - - - - - - -		MDI		6 4 - 6 L - J	D	A set b mod	Anabud
Analyte	Resu			MRL		Method	Prepared	Analyzed	Analyst
Boron Conventional	I Chemistry Analyses_01	ND L1,	,u mg/L	0.10	0.10	EPA 200.7	02/18/2013 08:14	02/21/2013 14:09	MLC
Analyte	Resu	it Fla	ag Units	MRL	MDL	Method	Prepared	Analyzed	Analyst
Sulfate		6	mg/L	1	0.2	EPA 300.0	02/25/2013 19:11	02/25/2013 19:11	DMH
- All Waste - All Drinki - Unless of - The Chai	collected by MMLI personnel are Water analyses comply with me ng Water analyses comply with r therwise noted, all quantitative re n of Custody document is includ y Search analytes should be reg. Target analyte was analyzed for	thodolog nethodo sults for ed as pa arded as	gy requirements logy requiremen r soils are report art of this report. s tentative identif	of 40 CFR Part 130 ts of 40 CFR Part 1 ed on a dry weight t fication based on the	5. 141. Dasis. e presur	nptive evidence	e of the mass spectra.		
	laboratory method detection lin			on limit (the value a	SSOCIATE	a with the qua	uner is the		
L1	The associated blank splke rec	overy w	as above metho	d acceptance limits.					
J	Estimated value.								
Standard Q	uallifiers/Acronymns								
MDL	Method Detection Limit								
MRL	Minimum Reporting Limit								
ND	Not Detected								
LCS	Laboratory Control Sample								
MS	Matrix Spike								
MSD	Matrix Spike Duplicate								
DUP % Rec	Sample Duplicate Percent Recovery								
RPD	Relative Percent Difference								
2	Greater than permit limits								
- <	Less than permit limits								
Analyses	erformed at the Madisonville KY	location	unless specifie	d with the following	location	codes			
02	Pikeville, KY		runess specific		içonioi				
03	Paducah, KY								
04	Lexington, KY								
05	Louisville, KY								
	alyses included in this Report								
Analyte		Certific	ations	_					
EPA 200.7 in	Water								
Boron		VA NEL	AC (460210)						
EPA 300.0 in	Water								
Sulfate		KY Drin	nking Water (000	30) VA NELAC (460	0210)				

Surface Elevation: 28112 Datum mill Datum mill Datum mill Datum mill DeSCRIPTION OF MATERIAL Datum strift to stift booth and gray, stilly CLAY - (CL) Lis 2.8 x 10 ⁻ mik DESCRIPTION OF MATERIAL Description of material and gray, stilly CLAY - (CL) 24-45 SS1 24-45 SS1 24-45 SS1 24-45 SS1 24-45 SS1 24-45 SS1 24-45 SS1 24-45 SS1 24-45 SS1 24-46 SS			Elec	ctronic Filing: Received, Cle	<u>erk's Offic</u>	<u>e 11/22</u>	/202	2 <u>1 **AS 2021-05**</u>	
Medium suff to self, brown and gray, silly CLAY - (CL) 24.4-5 551 k = 2.8 x 10 ⁴ m/s 24.4-5 551 k = 2.8 x 10 ⁴ m/s 24.4-5 551 2.4-4-5 553 54-5-7 553 3.4-4-5 557 224-5 551 2.4-4-5 557 224-5 557 2.4-4-5 557 224-5 557 2.4-4-5 557 224-5 557 2.4-4-5 557 224-5 557 2.4-4-5 557 224-6 557 2.4-4-5 557 224-6 557 2.4-4-5 557 224-6 551 2.4-4-5 551 224-6 551 2.3-4 551 23-4 551 2.3-4 551 23-4 551 2.3-4 552 517 24-6 531 3.3-4 523 517 24-6 537 3.3-4 523 537 537 537 3.				Completion Date:	FOG	SHT (pcf) OUNTS ERY/ROD	S	WELL DIAGRAM	
Medium suff to self, brown and gray, silly CLAY - (CL) 24-4-5 SSI Concess 1.0 sso 10 44-5 SSI 2-3-4 SSI 2-4-5 SSI <		T				N N N N N N N N N N N N N N N N N N N	MPLE		
10 22-34 53 23-44 53 24-45 53 35-67.9 556 36-57.9 556 36-57.9 556 36-57.9 556 36-45.6 557 36-57.9 556 36-67.9 556 36-67.9 556 36-46.5 557 24-67.5 551 24-7.5 5516		DEPTH IN FEET	DESCR	IPTION OF MATERIAL	GRAF	DRY UNIT SPT BLO CORE REC	SA	Å	Į
22-34-5 5-5 10 24-5-6 10 24-5-7 10 24-5-7 10 24-5-7 10 24-5-7 10 24-5-7 10 24-5-7 10 24-5-7 10 24-5-7 24-5-7 556 24-5-7 551 24-5-7 551 24-5-7 551 24-5-7 551 24-5-7 551 24-5-8 551 24-5-7 551 24-5-8 551 24-5-8 551 24-5-8 551 24-5-8 551 24-5-8 551 24-5-8 551 24-5-8 551 24-5-8 551 23-5 5167 35 5167, brown and gray, sily CLAY, trace sand - CL 77-6-6 35 517, brown and gray, sily CLAY, trace sand - CL 23-44 14-6-7 522 <			Medium stiff to stiff,	brown and gray, silty CLAY - (CL)		2-4-4-5	SS1	Concrete 1.0 360).1
10 10<			k = 2.8 x 10 ⁻⁸ cm/s			2-2-3-4	SS2	2.6 35	3.6
10 3-56-7 SS 15 3-57-7 SS6 15 2-24-5 SS9 24-55 SS9 2-4-5 24-55 SS9 2-4-5 24-55 SS9 2-4-5 24-55 SS9 2-4-5 24-56 SS9 2-4-5 24-56 SS9 2-4-5 24-56 SS9 2-4-5 24-56 SS13 2-4-56 25- Frace gravel and weathered limestone 1-5-18-22 15- Medium stift, brown and gray, stily CLAY, trace sand - CL 7-7-6-6 12-24-15 SS16		5-				2-3-4-5	SS3		
10 3-5-7-9 556 3-4-4-5 557 22-4-5 558 2-4-5-5 558 2-4-5-7 551 3-57 557						5-4-5-6	SS4		1
3-57-0 S86 3-44-45 S87 15						3-5-6-7	SS5		
1-2-2-1 SS21 1-4-6-7 SS22 45- very stiff, with weathered limestone 417 319 Filter Send 417 319 Filter Send 50- 6 6 6 6 7 7 7 7 7 7 7 7 7 7	(2)	— 10 <i>—</i>				3-5-7-9	SS6		
1-2-2-1 SS21 1-4-6-7 SS22 45- very stiff, with weathered limestone 417 319 Filter Send 417 319 Filter Send 50- 6 6 6 6 7 7 7 7 7 7 7 7 7 7	TYPES ILY.					3-4-4-5	SS7		
1-2-2-1 SS21 1-4-6-7 SS22 45- very stiff, with weathered limestone 417 319 Filter Send 417 319 Filter Send 50- 6 6 6 6 7 7 7 7 7 7 7 7 7 7	SOIL .	— 15—				2-2-4-5	SS 8		
1-2-2-1 SS21 1-4-6-7 SS22 45- very stiff, with weathered limestone 417 319 Filter Send 417 319 Filter Send 50- 6 6 6 6 7 7 7 7 7 7 7 7 7 7	RPOS					2-4-5-5	SS9		
1-2-2-1 SS21 1-4-6-7 SS22 45- very stiff, with weathered limestone 417 319 Filter Send 417 319 Filter Send 50- 6 6 6 6 7 7 7 7 7 7 7 7 7 7	DN PU					2-4-6-7	SS10		
1-2-2-1 SS21 1-4-6-7 SS22 1-4-6-7 SS22 4-10-12-6 SS23 3-4-4-4 SS24 1-2-3-3 SS25 2-3-4-6 SS26 50 2-3-4-6 50 50 50 2-3-4-6 50 2-3-4-6 50 50 50 2-3-4-6 50 50 6 0.10 slotted 6 0.10 slotted 9 0.10	ARIE:	— 20 <i>—</i>				2-4-7-5	SS11		
1-2-2-1 SS21 1-4-6-7 SS22 1-4-6-7 SS22 4-10-12-6 SS23 3-4-4-4 SS24 1-2-3-3 SS25 2-3-4-6 SS26 50 2-3-4-6 50 50 50 2-3-4-6 50 2-3-4-6 50 50 50 2-3-4-6 50 50 6 0.10 slotted 6 0.10 slotted 9 0.10	ISU11					2-3-4-4	SS12		Ì
1-2-2-1 SS21 1-4-6-7 SS22 1-4-6-7 SS22 4-10-12-6 SS23 3-4-4-4 SS24 1-2-3-3 SS25 2-3-4-6 SS26 50 2-3-4-6 50 50 50 2-3-4-6 50 2-3-4-6 50 50 50 2-3-4-6 50 50 6 0.10 slotted 6 0.10 slotted 9 0.10	FOR I	25	trace sand			3-4-6-6	SS13	3	1
1-2-2-1 SS21 1-4-6-7 SS221 1-2-2-3 SS251 1-2-3-3 SS252 2-3-4-6 SS26 0-10 Soloted 0-10	SOXIM CLOG					2-4-5-8	SS14	4	
1-2-2-1 SS21 1-4-6-7 SS221 1-2-2-3 SS251 1-2-3-3 SS252 2-3-4-6 SS26 0-10 Soloted 0-10	APPE					2-3-4-6	SS15	5	
1-2-2-1 SS21 1-4-6-7 SS221 1-2-2-3 SS251 1-2-3-3 SS252 2-3-4-6 SS26 0-10 Soloted 0-10	VT THE	- 30-	trace gravel and we	eathered limestone		2-4-8-18	SS16	6	
1-2-2-1 SS21 1-4-6-7 SS221 1-2-2-3 SS251 1-2-3-3 SS252 2-3-4-6 SS26 0-10 Soloted 0-10	RESEA		Weathered LIMES	TONE with silty clay		15-18-22	SS17	7	
1-2-2-1 SS21 1-4-6-7 SS221 1-2-2-3 SS251 1-2-3-3 SS252 2-3-4-6 SS26 0-10 Soloted 0-10	s REPI BE GS	35-	Stiff, brown and gra	ay, silty CLAY with sand - CL		7-7-6-6	SS18	8	
1-2-2-1 SS21 1-4-6-7 SS221 1-2-2-3 SS251 1-2-3-3 SS252 2-3-4-6 SS26 0-10 Soloted 0-10	LINES		Medium stiff, brown	n and gray, silty CLAY, trace sand - CL		2-3-4-4	SS19	9	
1-2-2-1 SS21 1-4-6-7 SS22 1-4-6-7 SS22 4-10-12-6 SS23 3-4-4-4 SS24 1-2-3-3 SS25 2-3-4-6 SS26 50 2-3-4-6 50 50 50 2-3-4-6 50 2-3-4-6 50 50 50 2-3-4-6 50 50 6 0.10 slotted 6 0.10 slotted 9 0.10	ATION					3-3-4-4	SS20	0 39.7 32	21.5
45- very stiff, with weathered limestone 4-10-12-6 SS23 2" sch 40 PVC Filter Sand 45- 50- 3-4-4-4 SS24 1-2-3-3 SS25 2-3-4-6 SS26 Bottom cap 51.7 305 50- Boring terminated at 52 feet. 2-3-4-6 SS26 Drawn by: KA Checked by: Roe App'vd.	TRANS	40	soft			1-2-2-1	SS21	1 41.7 3	19.5
Boring terminated at 52 feet. 1-2-3-3 SS25 Boring terminated at 52 feet. 2-3-4-6 SS26 Bottom cap Sti 7 305 Bottom cap Sti 7 305 Sti 7 305 Sti 7 305 Bottom cap Sti 7 305 Sti 7 305 Sti 7 305 Bottom cap Sti 7 305 Bottom cap Sti 7 305 Sti 7 305 Sti 7 305 Bottom cap Sti 7 305 Sti 7 305 Sti 7 305 Bottom cap Sti 7 305 Bottom cap Sti 7 305 Sti 7 305 Sti 7 305 Bottom cap Sti 7 305 Bottom cap Sti 7 305 Sti 7 305 Sti 7 305 Bottom cap Sti 7 305 <t< td=""><td>STRA</td><td></td><td></td><td></td><td></td><td>1-4-6-7</td><td>SS22</td><td>2 [[]]</td><td></td></t<>	STRA					1-4-6-7	SS22	2 [[]]	
Boring terminated at 52 feet. 1-2-3-3 SS25 Boring terminated at 52 feet. 2-3-4-6 SS26 Bottom cap Sti 7 305 Bottom cap Sti 7 305 Sti 7 305 Sti 7 305 Bottom cap Sti 7 305 Sti 7 305 Sti 7 305 Bottom cap Sti 7 305 Bottom cap Sti 7 305 Sti 7 305 Sti 7 305 Bottom cap Sti 7 305 Sti 7 305 Sti 7 305 Bottom cap Sti 7 305 Bottom cap Sti 7 305 Sti 7 305 Sti 7 305 Bottom cap Sti 7 305 Bottom cap Sti 7 305 Sti 7 305 Sti 7 305 Bottom cap Sti 7 305 <t< td=""><td>10ANE</td><td>- 45-</td><td>very stiff, with weat</td><td>thered limestone</td><td></td><td>4-10-12-</td><td>68823</td><td></td><td></td></t<>	10ANE	- 45-	very stiff, with weat	thered limestone		4-10-12-	68823		
S0 2-3-4-6 SS26 Boring terminated at 52 feet. Bottom cap 51.7 305 GROUNDWATER DATA DRILLING DATA Checked by: Rop Applyd. by Rop AUGER HOLLOW STEM ENCOUNTERED AT 48 FEET F WASHBORING FROM FEET PH DRILLER BGF LOGGER DRILL RIG Ash Pond Evaluation EEI Facility DRILL RIG HAMMER TYPE Auto Ash Pond Evaluation EEI Facility Date: 71/10	9/22/					3-4-4-4	SS24		
	n GPJ		1			1-2-3-3	SS25		
	963830	- 50-	-			2-3-4-6	SS26	6 Bottom can 51.7 34	09.5
	TINC		Boring terminated	at 52 feet.				52.0.3)9.1
	o rag		1					Drawn by: KA Checked by: Rop App'vd. by B	P
).Aqqc		GROUNDWATER					Date: 7/14/10 Date: 9/20/10 Date: 9/20/	10_
	EELJ	FN	COUNTERED AT 48					GEOTECHNOLOGY	
	ZENV							FROM THE GLOUND UP	
	150.0								
REMARKS: LOG OF BORING: G-101				HAMME	ER TYPE <u>Au</u>	<u>to</u>			
LOG OF BORING: G-101	002 W	RE	MARKS:						<u> </u>
	RING 2							LOG OF BORING: G-101	
ā	JF BOF								
Project No. J017150.02	0.901					<u></u>	· •••••••	Project No. J017150.02	



Electronic Filing: Received, Clerk's Office 11/22/2021 **AS 2021-05**

Electronic Filing: Received, Clerk's Office 11/22/2021 ** AS 2021-05** Surface Elevation: 345.16 DRY UNIT WEIGHT (pcf) SPT BLOW COUNTS CORE RECOVERY/RQD 6/20/10 Completion Date: WELL DIAGRAM **GRAPHIC LOG** Datum <u>msi</u> SAMPLES Flushmount DEPTH IN FEET Centre Contraction Eler III DESCRIPTION OF MATERIAL Medium stiff to very stiff, brown silty CLAY - (CL) Concrete 2-3-5-6 SS1 1.0 344.2 2.5 342.7 3-5-9-11 SS2 Ì, 5 3-6-11-11 SS3 4-11-14 SS4 -15 6-8-9-10 SS5 10 2-5-5-6 SS6 SOIL TYPES 2-5-5-7 SS7 15 2-5-6-7 SS8 BETWEEN S Bentonite k = 9.2 x 10⁻⁹ cm/s 2-3-4-5 SS9 2" sch 40 PVC with coal DARIES BE 2-4-5-4 SS10 20 2-3-4-4 SS11 BOUNDAF SS12 1-2-3-4 APPROXIMATE PHIC LOG FOR 25 1-3-4-4 SS13 1-3-4-5 SS14 1-2-3-4 SS15 CIRC I 30 30.0 315.2 2-3-4-5 SS16 LINES REPRESENT MAY BE GRADUAL. 31.7 313.5 Soft to medium stiff, brown silty CLAY - CL 1-2-2-4 SS17 35 2-2-4-5 SS18 Filler Sand 2" sch 40 PVC 0-1-1-2 SS19 0.10 slotted STRATIFICATION I THE TRANSITION 2-2-2-2 SS20 40 2-4-4-8 SS21 41.7 303.5 42.0 303.2 Bottom cap Boring terminated at 42 feet. NOTE: 5 45 GPJ 0638301 50 GTINC IOPPA GP.I Checked by: ROP App'vd. by: ROY Drawn by: KA **GROUNDWATER DATA DRILLING DATA** Date: 7/14/10 Date: 9/20) 10 Date 9/21/10 X FREE WATER NOT ___ HOLLOW STEM AUGER Ē ENCOUNTERED DURING DRILLING GEOTE LOGYZ WASHBORING FROM ___ FEET J017150.02ENV -FROM THE GROUND UP PH DRILLER JPC LOGGER ___ DRILL RIG Ash Pond Evaluation HAMMER TYPE Auto **EEI Facility** Joppa, Illinois LOG OF BORING 2002 WL **REMARKS:** LOG OF BORING: G-112b Project No. J017150.02

	ce Elevation: <u>350.46</u> Datum <u>msl</u>	Completion Date:6/25/10	SRAPHIC LOG	DRY UNIT WEIGHT (pcf) SPT BLOW COUNTS CORE RECOVERY/ROD	SAMPLES	WELL DIAGRAM					
DEPTH IN FEET	DESCR	IPTION OF MATERIAL	GRAPH	DRY UNIT W SPT BLOW CORE RECC	SAM						
	FILL			2-2-3-4	SS1	Concrete 1.0 349.5					
	Medium stiff to stiff,	brown CLAY - CH		2-5-6-7	SS2	2.6 347.9					
- 5-				2-2-4-3	S S3						
	Soft, brown to brow	n and gray CLAY - CH		2-1-2-3	SS4						
- 10-	Modium stiff to stiff	brown and gray CLAY - CH	//	1-1-1-3	SS5						
				3-3-4-5	SS6						
				2-3-4-6	SS7	Bentonite					
- 15				2-3-4-5	SS8	2" sch 40 PVC					
				2-2-4-5 4-5-7-8							
- 20-				4-5-7-7							
				2-5-6-10	· · · · ·						
- 25-				2-8-10-10							
	Stiff, gray and brow k = 3.7 x 10°cm/s	n, silty CLAY - CL		3-6-8-9	+						
	× K = 3.7 X 10 GH/S			4-6-8-11	SS15	2" sch 40 PVC					
- 30-				4-4-7-19	SS16	0.10 slotted					
	Hard to very stiff, g	ray and brown, sandy CLAY - CL		8-17-16 -20	SS17	Filter Sand					
- 35-				6-8-9-9	SS18						
	Still, brown and gra	y, silty CLAY, trace sand - (CL)		3-4-6-8							
- 40-	Boring terminated a	at 40 feet.	///	4-4-6-9	SS20	Bottom cap					
- 45-											
- 45-											
- 50											
					<u> </u>	Drawn by: KA Checked by: KOP App'vd. by KOP					
				_		Date: 7/14/10 Date: 9/20), Date: 9/200, Date					
ENC	<u>X</u> FREE WATER N OUNTERED DURING	DRILLING WASHBORIN		FEET							
		<u>_PH_</u> DRILLE _ <u>CME 55</u>	R <u>JPC</u> LO 10X DRILL F			Ach Dond Evaluation					
			R TYPE <u>AL</u>			Ash Pond Evaluation EEI Facility					
RF	MARKS:					Joppa, Illinois					
T that						LOG OF BORING: G-113					
						Project No. J017150.02					

	ce Elevation: <u>360.9</u>	Completion Date:6/19/10	5010	IGHT (pcf) COUNTS 'ERY/RQD	ES	WELL DIAGRAM
DEPTH IN FEET	DESCR	IPTION OF MATERIAL	GRAPHIC LOG	DRY UNIT WEIGHT (pcf) SPT BLOW COUNTS CORE RECOVERY/RQD	SAMPLES	Flushmount
	GRAVEL				SS1	Concrete 1.0 3
	Medium stiff to stiff,	brown and gray, silty CLAY - (CL)		3-4-4-5	SS2	2.7 3
- 5-				2-3-3-5	SS3	
				3-3-4-4	SS4	
10	k = 1.6 x 10 ⁻⁸ cm/s			1-2-3-5	SS5	
				3-5-5-6	SS6	
				2-4-5-6	SS7	
- 15				2-3-4-5	SS8	Bentonite
	Medium stiff to stiff CL	brown and gray, silty CLAY, trace sand -		3-4-6-7	SS9	2" sch 40 PVC
- 20-				3-4-6-6	SS10	
				3-5-7-8	SS11	
				3-5-7-9		
- 25-				2-3-5-6		
				3-5-7-6		
— <u>30</u> —				3-5-8-8		29.7
				4-7-9-4		31.7
				4-4-6-7		
— 35— ———	Medium stiff to ver	stiff, brown and gray, sandy CLAY with	{////	2-4-3-5		2" sch 40 PVC
	silt - CL	,,, .		5-5-7-14 13-13-10		0.10 slotted
- 40-				-8	3320	
	Boring terminated	at 42 feet.		2-4-6-7	5521	Bottom cap
- 45	·					
45	l					
- 50-						
50						
	; 	······································				
	GROUNDWATER D	DATA DRILL	ING DATA	<u>!</u>		Drawn by: KA Checked by: R 1 / App'vd. by: R Date: 7/14/10 Date: 9/20/10 Date: 9/20
ENC REI	X FREE WATER N OUNTERED DURING			FEET		
			ORILL RIG R TYPE <u>Au</u>	<u>to</u>		Ash Pond Evaluation EEI Facility Joppa, Illinois
RE	MARKS:					LOG OF BORING: G-151
1						Project No. J017150.02

i	ce Elevation: <u>348.56</u> Datum <u>msl</u>	Completion Date: .	ceived_Clerk's C	GRAPHIC LOG		SAMPLES	WELL DIAGRAM
DEPTH IN FEET		PTION OF MA		GRAPH	DRY UNIT WEIGHT (pcf) SPT BLOW COUNTS CORE RECOVERY/RQD	SAMI	Flushmount
		CLAY with organics -			2-3-3-4	SS1	Concrete 1.0 347.6
	Medium stiff, brown	and gray, silty CLAY -	(CL)		1-1-2-3	SS2	2,6 345.9
- 5					1-2-3-5	SS3	
					2-3-4-5	SS4	Bentonite
10					1-3-4-4	SS5	
	- becoming stiff				2-3-5-5	SS6	
	< Decoming suit				2-5-8-9	SS7	
- 15-					2-5-3-6	SS8	
	trace sand to 25 feet	t			3-5-5-7	SS9	
- 20-	k = 1.1 x 10 ⁻⁸ cm/s		7		1	SS10	0.10 slotted
					3-61-1100-9	5511	
— 25—					2-4-5-5	SS12	2 Bottom cap 25.0 323.6
	Boring terminated at	t 25 feet.					25,0 323.6
- 30-							
— 35—							
40							
						1	
- 45-							
— — 50—							
ENC	GROUNDWATER D	ATA	DRILLING	DATA			Drawn by: KA Checked by: KG App'vd. by: KO Date: 7/14/10 Date: 9/20 10 Date: 9/20 10
					W STEM		
ENC	COUNTERED AT 20 F	EET ¥	WASHBORING FR				
			PH DRILLER B		OGGER		
			<u>ATV</u> DRIL HAMMER TYF		to_		Ash Pond Evaluation EEI Facility
							Joppa, Illinois
REN	ARKS:						LOG OF BORING: G-152
r.							Project No. J017150.02

		ce Elevation: <u>351.73</u> Datum <u>msl</u>	ronic Filing: Received, Cler Completion Date:6/18/10				WELL DIAGRAM				
	DEPTH IN FEET	DESCR	IPTION OF MATERIAL	GRAPHIC LOG	DRY UNIT WEIGHT (pcf) SPT BLOW COUNTS CORE RECOVERY/RQD	SAMPLES	Flushmount				
		Medium stiff, brown	and gray CLAY - CH		2-2-3-4	SS1	Concrete 1.0 350.)				
		Soft, brown and gra	y CLAY - CH		1-1-2-1	SS2	2.9 3				
	5	Medium stiff to stiff,	brown, silty CLAY, trace sand - (CL)		1-2-4-4	SS3	2.9				
					2-4-4-5	SS4					
	— 10—				2-3-6-6	SS5					
S					3-5-5-6	S \$6					
TYPE		- .			1-4-4-8	SS7					
N SOIL	— 15—	$k = 1.2 \times 10^{-6} \text{ cm/s}$			2-4-5-8	SS8	2" sch 40 PVC				
URPO					2-6-6-7	SS9					
ES BE FION P	— 20-				3-5-7-7	SS10					
VDARI STRAT					2-5-7-8	SS11					
BOUR					3-5-6-7	SS12					
IMATE OF FOF	25		own, silly CLAY - CL		4-4-6-6	SS13					
THE APPROXIMATE BOUNDARIES BETWEEN SOIL TYPES GRAPHIC LOG FOR ILLUSTRATION FURPOSES ONLY.		very sur to sur, or	JWH, SINY CLAY - CL		4-8-8-11	<u>+</u> {	27.7 324				
HE AF GRAPI	- 30-				3-4-7-9	╉───┪	1 29 7 322.				
SENT T		Stiff, brown, sandy	CLAY with silt - Cl		4-6-8-10	+					
GRAD		Sun, Drown, aanoy			5-6-6-8	┿╾╼┥	2" sch 40 PVC				
VES Ri AY BE	35				3-4-6-8	┤━━╍──┤					
CATION LINES REPRESENT INSITION MAY BE GRADUAL.		Stiff, brown clayey	SILT - ML		5-5-7-7						
FICATI ANSIT	- 40-	Boring terminated a			2-3-6-7	5520	Bottom cap				
STRATIFI THE TRA											
AND T	— 45~										
NOTE: S 9/22/10 ^{AND}	40			}	}						
GPJ 9											
38301.	- 50-										
INC 06											
21 GT											
PA.Gi		GROUNDWATER D	DATA DRIL	LING DATA	1		Drawn by: KA Checked by KO (App'vd. by: Kg (Date: 7/14/10 Date: 6/20 (Date: 9/20 (b)				
for ta:	ENC	X FREE WATER N	ODULINO	HOLLO			GEOTECHNOLOGY				
NV - E			WASHBORI								
50.025				<u>DRILL RIG</u>	JOOLN		Ash Pond Evaluation				
, 7, OL			HAMME	ER TYPE <u>Au</u>	to_		EEI Facility				
02 WL	PE	MARKS:					Joppa, Illinois				
06 OF BORING 2002 WL J017150 02ENV - EEI JOPPA.GPJ GTINC 9638301.GPJ	RE	WARNS.					LOG OF BORING: G-153				
1 06 DF							Project No. J017150.02				

Electronic Filing: Received, Clerk's Office 11/22/2021 ** AS 2021_05** SOIL BORING LOG INFORMATION



Hacu	ity/Pro	nent N	Jama			ti icencă/	Vermin	Mônito	nia Na	mbar		Horna	Pag Numb	-	of	2	
	-	-		ation ((FFI)	License/Permit/Monitoring Number							G11				
					f crew chief (first, last) and Firm	Date Dri	lling S	tarted		Dat	e Drilli				Dni	ling Method	
M	att Co	opei					•					Ũ	•			blow stem	
				g, Inc.				/2013				1/28/2	2013			iger	
					Common Well Name	Final Sta					e Elevat	-				Diameter	
	l Grid	0			G112C	319.4	Feet (NAVI)88)		.6 Fee			3)	7.8	inches	}
	e Plane	-	n l		timated:) or Boring Location in or Boring	La	t	•	•	н	Local C	na Lo				M	
Gui		/4 of			/4 of Section , T N, R	Long	r	o	1	City/ or Villa		26 Fe	N⊠ e⊡ s		188 33	⊠ E Feet □ W	
Facil	ity ID			•	,	State	·	Civil To	wn/Cit	y/ or V					000.00		
	_				Massac	Illinois		Joppa	L								
Sa	mple									du		Soil	Prop	erties			
	- w	Ē.	ا _د	ы с	Soil/Rock Description					Lai							
٩		- G	ij	I Fee	And Geologic Origin For				_	e V	ssive (tsf	0		.		Its	_
Typer	i E	δ, o	ŭ	th Ir	Each Major Unit		scs	hic	ram	10.6	pre:	stur6	ਸ਼ੂ . <u>ਜ</u>	x ici	0		
Number and Type	Length Att.	Kecovered	Blow Counts	Depth In Feet			U S	Graphic Log	Well Diagram	PID 10.6 eV Lamp	Compressive Strength (tsf)	Moisture Content	Liquid Limit	Plasticity Index	P 200	RQD/ Comments	
1	48			_	0 - 0.8' SILTY CLAY CL, LOAM, dark brown	n, high			38							soil samples	
	20	'		-	plasticity, soft, moist.		CL		38							collected with 1.5"	
				-1	0.8 - 24' SILTY CLAY CL, light yellowish bro (10YR 6/4), high plasticity, very soft to soft.	own					1.25					diameter macro core	
			Ē	_	(,,,,,,,,									Ì		sampler with	
		1		-2												lliners	
		ł		-													_
				-3			l									1	
				-									İ				
	_			-4					\mathbf{V}								-
2	60		Ē	_					÷				Ì				
				-5	4.5' stiff to very stiff, low to medium plasticity gray (10YR 7/1) with 10-25 % yellowish brow	/, light /n					4						
				-	(10YR6/8) mottling										1		
			İ	-							3.5			1			
				6										ļ			
			ł				CL				3.5						
				-7													
				-							3.5				,		-
			}	-8	8' light gray with <10% mottling, hard, dry.						4						
				-							4			[
3	- 60		- {	-9													
Ť	51			-	9.5' stiff, medium plasticity, moist.						2						
				-10	a.a sun, modum plasualy, moisi.						²						
			1	-							<u>a</u> -						
				-11							2.5						
			ļ	-													_
				-12							2.25		 				
	ebv ce	rtifv f	l hat t		rmation on this form is true and correct to the b	est of my b		l			I	1	L	1	<u> </u>		
		, t		mu		Storiny K	100 10	-60.									

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G112C

weight of the second			HNOLOGY Boring Number G112C						-	e 2	of	2
4 60 0.8 - 24' SILTY CLAY CL light yellowish brown (10YR 64), hish plasticity, very soft to soft. continue, isin plasticity, very soft to soft. 3 4 60 13.5' very stiff sily clay. 3.25 14 14' medium to stiff, medium to high plasticity. gray (10YR 64) with trace mottling. 3.25 16 16' no mottling. 2.5 17 1.5' very stiff sily clay. 1.5' 18 12.5' gray (10YR 7/1), no mottling. 1.5' 17 17.5' light gray (10YR 7/1), no mottling. 1.5' 18 19' 19' wet, soft to very soft, high plasticity. 1 20 21 2 21 22 2.5' very stiff silty clay. 22 2.5' very stiff to hard, low plasticity. light gray 1 23 22.5' very stiff to hard, low plasticity. light gray 3 24 24' - 25' CL. CL 24' - 25' CL.	Sample					amp		Soil	Prope	rties		-
4 60 0.8 - 24' SILTY CLAY CL, light yellowish brown (continued) 3 4 60 13.5' very stiff silty clay. 3.25 13.5' very stiff silty clay. 3.25 14' medium to stiff, medium to high plasticity, gray (10YR 6/1) with trace mottling. 2.5 -16 16' no mottling. -17 17.5' light gray (10YR 7/1), no mottling. -18 17.5' light gray (10YR 7/1), no mottling. -19 19' wet, soft to very soft, high plasticity. 20 21 -21 22 -22 22.5' very stiff to hard, low plasticity, light gray (10YR 7/1), no mottling. -19 19' wet, soft to very soft, high plasticity. -20 22.5' very stiff to hard, low plasticity. light gray -21 22.5' very stiff to hard, low plasticity. light gray -22 22.5' very stiff to hard, low plasticity. light gray -21 -22 -22 -22 -24 -24 - 25' CL. -24 -24 - 25' CL. -24 -24 - 25' CL.	Number and Type Length Att. & Recovered (in)	Blow Counts Depth In Feet	And Geologic Origin For	10	Graphic Log Well Diagram	PID 10.6 eV L	Compressive Strength (tsf)	Moisture Content	Liquid Limit	Plasticity Index	P 200	RQD/ Comments
	4 60	- - - - - - - - - - - - - - - - - - -	 (10YR 6/4), high plasticity, very soft to soft. (continued) 12.5' gray (10YR 5/1), no mottling. 13.5' very stiff silty clay. 14' medium to stiff, medium to high plasticity, gray (10YR 6/1) with trace mottling. 				3 3.25 2.5 3.25					
	5 60 50	- 19 - 20 - 21 - 22	 18.5' very stiff silty clay. 19' wet, soft to very soft, high plasticity. 22.5' very stiff to hard, low plasticity, light gray. 	CL			4 1 2 2.5					
		-24	24 - 25'CL.	cı.								PP 3.5 - 4. Auger and Clean hole 24' to 25'

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Facili	ty/Proje	ct Nan	ie		License/	Permit	Monito	ring Nu	mber-	i	Boring	Paj Numb			3	
	pa Pov			(EEI)	License/Permit/Monitoring Number				ľ	6	G15					
				of crew chief (first, last) and Firm	Date Dri	lling S	tarted		Dat	e Drillu	ng Con			Dril	ing Method	
	tt Cooj					-								hc	ollow stem	
_Bu	lldog Í	İrillir	ıg, Inc.				/2013				1/30/2	2013		au	iger	
				Common Well Name	Final Sta			1		e Elevat				rehole	Diameter	_
	~			G152B	312.3	Feet (NAVI	D88)		.2 Fee			3)	7.8	inches	j
	Grid Or Plane	rıgın		stimated:) or Boring Location inois East Zone N, E S/CAN	La	t	0	•	"	Local G	irid Lo			_		
State		c		, u				,				ØN			ΣE	_
Facili	1/4	of	1	I/4 of Section , T N, R	Long State	3	Civil T	own/Cit			.58 Fe	etLIS	8329	31.61	Feet 🗌 W	
racin	ly ID			Massac	Illinois		Joppa		y/ 01 V	mage						
Sa	mple		1	14103500	minois		laohhs	<u>а</u> Г Т	<u>p.</u>	1	Sail	Prop	artico		— — — — — — — — — — — — — — — — — — —)
									PID 10.6 eV Lamp					·	4	
	8 (E	ıts	g	Soil/Rock Description					N N	s Ç						_
۲g	Length Att. & Recovered (in)	Blow Counts	Depth In Feet	And Geologic Origin For		s	5	<u>е</u>	6 e	essi h (t	2 -		2		ants	_
- and F	igth	N C	E E	Each Major Unit		U U	phid 2	graı graı	010	npre	istur ten	uid ti	stici ex	200		
Number and Type	Ler Rec	Blo	Det			US	Graphic Log	Well Diagram	PID	Compressive Strength (tsf)	Moisture Content	Liquid	Plasticity Index	P 2(RQD/ Comments	
1	42		E	0 - 0.75' SILTY CLAY CL, disturbed with gra	avel,							1			PP 2 - 2.25	
	19		E	tree limbs, wood from clearing activities; dark	- corown,	CL	\swarrow	22				1				
				0.75 - 4.5' SILTY CLAY CL, light yellowish t												
			È –	(10YR 6/4), high plasticity, very soft to soft, s	silty clay											
			L 2	with organics (roots), soft, high plasticity, ligh yellowish brown (10YR 6/4), moist.	IL					i						
			Ę													
			E			CL										
			-3													
2	60		Ę							3.25						
-	56		4				1			0.20			ļ			-
			F	4' Silty Clay grading to a Clayey Silt, low pla stiff, light gray (10YR 7/1), with 50% reddish	sucity, brown –											
			F,	mottling, moist.												
			<u>–</u> 5	4.5 - 12.5' SILT: ML, non plastic, stiff, very p	bale					3						انتزر
			E	brown (10YR 8/2), dry.		-										
			<u>F</u> 6							3						
			F													
			E7													
			È	7.3' soil horizon with small rootlets, 50% red	dieb					2						
			F,	brown mottling.												
			-8 -	7.5' very pale brown (10YR 8/2), non plastic	, stiff,					1.75						
3	60	F	dry.		ML				4							
~	58		– 9		_1_											
			F	9' silt with clay, very stiff, non plastic, very p brown (10YR 7/3) with 10-25% reddish brown	ale n											
			F.,	mottling.	••]	
			F ¹⁰							3.5						_
			F									1				
																-
			E							2						_
			E-12											1		
	L bu comit		.	I		1	.]			I		1		<u> </u>	<u> </u>	
I nere		y mat		ormation on this form is true and correct to the be	est of my k	nowlea	ige.									-

Signature	Firm Natural Resource Technology 23713 W. Paul Road Suite D. Pewaukee, WI 53072	Tel: (262) 523-9000 Fax: (262) 523-9001
		W ADDRESS Project: GINT 2126 GBL

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		C1	52B	
ring	Number	- (T I	<u> 22</u> H	

					Boring Number G152B								ge 2	of	3
Sa	mple	_						ļ	dua		Soil	Prop	erties		1
Number and Type	Length Att. & Recovered (in)	נווו) איניטעטונים	Blow Counts	Depth In Feet	Soil/Rock Description And Geologic Origin For Each Major Unit	USCS	Graphic Log	Well Diagram	PID 10.6 eV Lamp	Compressive Strength (tsf)	Moisture Content	Liquid Limit	Plasticity Index	P 200	RQD/ Comments
		Τ		-						2					
4	60			-13	 12.5 - 28.5' SILTY CLAY CL, medium to stiff, low to medium plasticity, light gray (10YR 7/1), with 50% mottling, moist. 13.5' 10-50% reddish brown mottling. 					2					
	60			-14	15.5 To-50 A readistr brown metaling.					2.5					
i				15	15' light gray (10YR 7/1).					2.25					
										2.25					
			i	- 18						3.25					
					18' yellowish brown (10YR 6/8) mottling, moist.					1					PP 2.5 - 3.5
5	60 60			19	18.5' medium to stiff, medium to high plasticity, light gray (10YR 7/1), with 10-25% reddish brown mottling, moist.					2.25					
				20		CL				2.5					
				-21						1.75					
				-22 						1.75					
					00 Flandium to stiff, high stastists, light serve					1.75					
6	60 60			24	23.5' medium to stiff, high plasticity, light gray (10YR 7/1), with 25-50% reddish brown mottling, moist.					2					
				-25 						1.5					
				26						1.5					
				-27						2.5					
NR	12			29	28.5 - 29.5' CL.					2					stopped sampling for
_	Ĩ	ł		27		CL									the day (1/28/13),
7	60 44				29.5 - 44.5' SILTY CLAY CL, stiff, medium to high plasticity, gray with >75% light yellowish brown (10YR 6/4) mottling, moist.					2.75					cleaned hole with augers to 29.5'
					31.5° 25-75% mottling.	CL				3.25					resumed sampling on 1/30/2013
ļ		ļ		-32	•		</td <td>7</td> <td>9</td> <td> </td> <td> </td> <td></td> <td> </td> <td>1</td> <td></td>	7	9					1	

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	·			Boring Number G152B							Pag	e 3	of	3.	
Sar	nple				Τ			du		Soil	Prope				
	& in)	S	et	Soil/Rock Description				PID 10.6 eV Lamp	6					'	
ъ е́	Att. red (oun	In Fe	And Geologic Origin For	s			.6 eV	essiv h (ts:	ຍີ		Ę		tuts	
Number and Type	Length Att. & Recovered (in)	Blow Counts	Depth In Feet	Each Major Unit	us c	aphi g	Well Diagram	010	Compressive Strength (tsf)	Moisture Content	Liquid Limit	Plasticity Index	P 200	RQD/ Comments	
<u>z</u> ś	Le Re	B	<u>ă</u>	29.5 - 44.5' SILTY CLAY CL, stiff, medium to high	Þ	۲ ö		lld	ບິ <i>ນ</i> ີ 3.5	Ϋΰ	Lii	Pla Inc	_P_	<u> </u>	
			Ē	plasticity, gray with >75% light yellowish brown (10YR 6/4) mottling, moist. <i>(continued)</i>					3.5					1	
			-33	33' very stiff to hard, gray (10YR 6/1), with < 25% yellowish brown (10YR 6/8) mottling.					4.5						
				yellowish brown (10YR 6/8) mottling.											
			34 E						2.5						
8	60 57		-35	34.5' stiff to very stiff, high plasticity.											
			Ę						3.5						
			-36						2.5						
			-						2.5						
			-37						4.25					1	
			Ē											(
			-38 -	38' hard, < 10% mottling.	CL				2.5					,	
														1	
9	60			20 5' your stiff to hard high plasticity army (10VD										PP is >4.5	_
9	60 55		-40	39.5' very stiff to hard, high plasticity, gray (10YR 6/1) with < 10% yellowish brown (10YR 5/6) mottling, moist.			:目: : 目:		3					,	
			E	moist.					ľ						
			-41						3						
			-42						3						
			43						4						_
			Ē						4.5						
			-44						3.75						
L				44.5' End of Boring.		r	e, He.							1	
														.	
					1										
					1										
						I	1	İ						I	

NATURAL RESOURCE TECHNOLOGY

MONITORING WELL CONSTRUCTION

Joppa Power Station (EEI) Facility License, Permit or Monitoring No.	<u>198552.26 ft. S. 829088.33</u> Local Grid Origin ⊠ (estimated: □) of	ftW or Well Location		
·	Lat '' Long		G112C	
Facility ID	St. Plane Illinois East Zone ft. N,			
	Section Location of Waste/Source		01/29/2013	
Type of Well	1/4 of 1/4 of Sec, T		Well Installed By: (Person's Name a	ind l
Well Code 11/mw	Location of Well Relative to Waste/Source	Gov. Lot Number	Matt Cooper	
Distance from Waste/ State	u 🗆 Upgradient s 🗆 Sidegradie	ent		
ft. Illinois	d 🗆 Downgradient n 🗆 Not Know		Kelron Environmental	
A. Protective pipe, top elevation		1. Cap and lock? 2. Protective cover pi		<u>ن</u> ا
B. Well casing, top elevation3	25.82 ft. (NAVD88)	a. Inside diameter:	-	
C. Land surface elevation	323.6 fl. (NAVD88)	b. Length:		
		c. Material:	Steel	
D. Surface seal, bottom ft. (NA	VD88) or II.		Other	
12. USCS classification of soil near screen:	anaras i franca	d. Additional prote	ection?	
		If yes, describe:		
Bedrock		3. Surface seal:	Bentonite Concrete	
13. Sieve analysis attached?		\backslash	Other	
		4. Material between	well casing and protective pipe:	_
Hollow Stem Au			Bentonite	
	her 🗆		Other	· C
		5. Annular space sea	l: a. Granular/Chipped Bentonite	
5	Air 🗆 🛛 👹 👹		ud weight Bentonite-sand slurry	
Drilling Mud 🗍 0 3 No	ne 🖾 🛛 🗱	cLbs/gal m		
16. Drilling additives used?	′es 🖸 🔰 👹		ite Bentonite-cement grout	
			volume added for any of the above	-
Describe N		f. How installed:	Tremie Tremie pumped	
17. Source of water (attach analysis, if require	ed):		Gravity	
n/a		6. Bentonite seal:	•	
LD V	Tes \square No ury \square ger \boxtimes her \square Air \square me \boxtimes Tes \square VD88) or 1.0 ft. VD88) or 12.9 ft > 12.		$3/8$ in. $\Box 1/2$ in. Bentonite chips	
E. Bentonite seal, top322.6 ft. (NA	VD88 <u>) or 1.0</u> ft	/ c	Other	: C
		, 7. Fine sand materia	I: Manufacturer, product name & me	esh s
F. Fine sand, top ft. (NA	VD88).or ft. 🔪 📓 🖉	/ a		
			ft ³	
G. Filter pack, top 310.7 ft. (NA		8. Filter pack materi	al: Manufacturer, product name & m	iesh
11 Second Island to 308 6 A 014		a	Filter Sil Silica 6 ft ³	
H. Screen joint, top308.6 fl. (NA	VD88) or 15.0 ft.	b. Volume added 9. Well casing:	Flush threaded PVC schedule 40	1 15
I. Well bottom	VD88).or 25.3 ft.	9. Wen casing.	Flush threaded PVC schedule 40	
			Other	
J. Filter pack, bottom298.6 ft. (NA	VD88) or 25.0 ft.	10. Screen material:	Schedule 40 PVC	_
		a. Screen Type:	Factory cut	t 🗵
K. Borehole, bottom298.6 ft. (NA	VD88).or 25.0 ft.		Continuous slot	
			Other	r Ľ
L. Borehole, diameter 7.8 in.		b. Manufacturer	·	0.0
120	Casing depth (well bottom) is	c. Slot size:	-	<u>0.0</u> 1
M. O.D. well casing 2.38 in.	greater than borehole bottom because the bottom well cap was	d. Slotted length: 11. Backfill material		
N. I.D. well casing 2.07 in.	pushed into the soft material at the		Other	
N. I.D. well casing 2.07 in.	base of the borehole.			



MONITORING WELL CONSTRUCTION

Facility/Project Name	Local Grid Location of Well		Well Name	
Joppa Power Station (EEI)	<u>198094.58 ft. 🖾 N.</u> 83293	<u>31.61 ft. CIW.</u>		-
Facility License, Permit or Monitoring No.	Local Grid Origin 🛛 (estimated:) or Well Location		
	Lat Long.		<u>G152B</u>	
Facility ID	St. Plane Illinois East Zoneft. N,	ft.E. S/C/N	Date Well Installed	
	Section Location of Waste/Source		01/30/2013	
Type of Well	1/4 of 1/4 of Sec		Well Installed By: (Person's Name as	nd Firm)
Well Code 11/mw	Location of Well Relative to Waste/Sou	trce Gov. Lot Number	Matt Cooper	
Distance from Waste/ State	u 🗆 Upgradient 🛛 s 🗆 Side	•	Kalaan Cassionan astal	
ft. Illinois	d 🗆 Downgradient n 🗆 Not	Known 1. Cap and lock?	Kelron Environmental	
A. Protective pipe, top elevation	ft. (NAV D88)	2. Protective cover pi		
B. Well casing, top elevation34	17.48 fl. (NAVD88)	a. Inside diameter:		in
C. Land surface elevation3	45.2 ft. (NAVD88)	b. Length:		ft.
D. Surface seal, bottom ft. (NAV		c. Material.	Steel	
· · · · · · · · · · · · · · · ·			Other	
12. USCS classification of soil near screen:		d. Additional prote	cction?	⊠ No
	W□ SP□ L⊠ CH□	II yes, describe:		-
Bedrock		3. Surface seal:	Bentonite Concrete	_
13. Sieve analysis attached?	s □ No 🛛 🗱 👹		Other	
14. Drilling method used: Rotar	v 🗆 🔰 📓 📓	4. Material between	well casing and protective pipe:	–
Hollow Stem Aug			Bentonite	0 📁
Othe	er 🗆 🛛 🗱		Other	
	i 🕺 👹	5. Annular space seal	a. Granular/Chipped Bentonite	⊠
1 2	ir 🗆 🛛 📓 📓		ud weight Bentonite-sand slurry	
Drilling Mud 🗇 0 3 Nor	ne 🖾 🛛 🗱 👹	cLbs/gal m	ud weight Bentonite slurry	
16. Drilling additives used?	sп 📓 📓	d% Benton		
	~ _ 📓 📓		volume added for any of the above	_ 1
Describe N		f. How installed:	Tremie Tremie nume od	_
17. Source of water (attach analysis, if required	i):		Tremie pumped Gravity	
n/a		6. Bentonite seal:	a. Bentonite granules	
		/	$\frac{1}{2}$ bencome granutes	
E. Bentonite seal, top 344.2 ft. (NAV	1D88 <u>) or 1.0</u> ft.		Other	
		7. Fine sand material	: Manufacturer, product name & mes	h size
F. Fine sand, top ft. (NAV	c = c + c + c + c + c + c + c + c + c +	/ a	· _ · · · · · · · · · · · · · · · · · ·	
			ft ³	
G. Filter pack, top 313.1 fl. (NAV		8. Filter pack materia	I: Manufacturer, product name & me	sh size
210.9		a	Filter Sil Silica	_
H. Screen joint, top ft. (NAV	D88).or 34.4 ft.	b. Volume added	$- \frac{7}{6^3}$	_
I. Well bottom 300.6 ft. (NAV	D88) or 44.6 ft _	9. Well casing:	Flush threaded PVC schedule 40	
1. wen bouoth II. (NAV			Flush threaded PVC schedule 80 Other	
J. Filter pack, bottom 300.7 ft. (NAV	D88) or 44.5 ft.	10. Screen material:	Schedule 40 PVC	
		a. Screen Type:	Factory cut	
K. Borehole, bottom 300.7 ft. (NAV	D88).or.44.5 fl.		Continuous slot	
			Other	
L. Borehole, diameter7.8 in.		b. Manufacturer		
	Casing depth (well bottom) is	c. Slot size:		<u>0.010</u> in.
M. O.D. well casing 2.38 in.	greater than borehole bottom because the bottom well cap was	d. Slotted length:		<u>10.0</u> ft.
	pushed into the soft material at the	11. Backfill material (below filter pack): None Other	
N. I.D. well casing 2.07 in.	base of the borehole.		Shier	
I hereby certify that the information on this form	n is true and correct to the best of my kr	nowledge	Date Modified: 2/19/2013	— — ——
Signature	17:	rce Technology	Tel: (262) 523-9000	
	Inatural Resou	lice Technology load Suite D. Pewaukee, WI 5		

			SPRINGFIE	·				·	
		TAW	ER WELL	SEALING	FORM		DETUP	N ALL COPIE	S TO IDDU C
DF FILLABLE/S							LOCAL	HEALTH DEF	PARTMENT
ionitoring well is equirements in th	submitted to this De sealed Such wells e Illinois Water Well UST BE NOTIFIED	are to be se Construction	aled not mor	e than 30 d E LOCAL H	ays after EAL TH D	they are a	bandoned in	accordance w	vith the sealing
. Ownership (N	ame of Controlling F	Party) El	ectric Energ	ıy, Inc.					
2. Well Location:	Well Site Addres	s 2100 I	Portland Rd		City	Joppa	3	Zip	62953
Lot #	Land I.D.#			County	Massac			Township	15S
Range 3E	Section			Quarter of	the		Quarter of th	ie	Quarter
GPS: North Degre Report decima would be latitu 3. Year Drilled	al minutes to minutes a Ide 38 degrees 46 minu	nd seconds b utes 4.2 seco	Seconds ny multiplying ti nds (0.07 x 60	he decimal pa = 4.2) N. Re	art of the m port GPS	coordinates	s to the neares	 e 38 degrees 46.	nds 59.3 .07 minutes N
	Monitoring			F		Diame	eter (in.) 2		
	Monitoring ar of obstruction	Yes	6. Total Dept						
7. Formation de	ar of obstruction	Yes		rials)	42	to (ft.)		3	
7. Formation de 8. Detains of Plu	ar of obstruction	Yes	or other mate	rials)				3	
7. Formation de 3. Detains of Plu Filled with	ar of obstruction agging (bentonite, ne Chip Bentonite	Yes	or other mate	rials)	42	to (ft.)	[
7. Formation de 3. Detains of Plu Filled with Kind of plug	ar of obstruction agging (bentonite, ne Chip Bentonite	Yes	From (ft.) From (ft.)	rials)	42	to (ft.) to (ft.)			
 Formation de Detains of Plu Filled with Kind of plug Filled with 	ar of obstruction agging (bentonite, ne Chip Bentonite	Yes	From (ft.) From (ft.) From (ft.)	rials)	42	to (ft.) to (ft.) to (ft.)			
7. Formation de B. Detains of Plu Filled with Kind of plug Filled with Kind of plug	ar of obstruction agging (bentonite, ne Chip Bentonite	Yes	From (ft.) From (ft.) From (ft.) From (ft.) From (ft.)	rials)	42	to (ft.) to (ft.) to (ft.) to (ft.)			
 7. Formation de 3. Detains of Plu Filled with Kind of plug 9. CASING REC 	ar of obstruction agging (bentonite, ne Chip Bentonite	Yes pat cement of of casing re	From (ft.) From (ft.) From (ft.) From (ft.) From (ft.) From (ft.) From (ft.)	rials)	42	to (ft.) to (ft.) to (ft.) to (ft.) to (ft.) to (ft.) Date well y	was sealed		13
 Formation de Detains of Plu Filled with Kind of plug CASING REC Licensed wat 	ar of obstruction	Yes pat cement of of casing re	From (ft.) From (ft.) From (ft.) From (ft.) From (ft.) From (ft.) From (ft.)	rials)	42 3	to (ft.) to (ft.) to (ft.) to (ft.) to (ft.) to (ft.) Date well s	was sealed	0	13

		525 W. JEFF					
	WAT	ER WELL S	EALING FOR	8M			
FILLABLE/SAVABLE						ALL COPIE	S TO IDPH (PARTMENT
form shall be submitted to itoring well is sealed. Suc irements in the Illinois Wa ARTMENT MUST BE NO	th wells are to be sea ter Well Construction	aled not more n Code. THE	than 30 days a	after they are TH DEPART	abandoned in a	ccordance w	ith the sealin
Ownership (Name of Con	trolling Party) Ele	ectric Energy	, Inc.				
Well Location: Well Site	Address 2100 P	ortland Rd		City Jop	pa	Zip	62953
Lot#	d I.D.#		County Ma	ssac		Township	155
Range 3E Se	ection		Quarter of the		Quarter of the		Quarter
GPS: North Degrees 37 Report decimal minutes to n would be latitude 38 degree	Minutes 12 ninutes and seconds by s 46 minutes 4.2 secon	Seconds	39 C decimal part of	Vest Degrees 88 the minutes by GPS coordina	Minutes 5 ⁴ y 60, e.g. latitude 3 tes to the nearest 0		
	7						
Year Drilled 6/21/2010	4. Drilling Pe	ermit Number	(and date, if kn	own G-15	2		
		ermit Number . Total Depth			2 neter (in.)]	
Type of Well Monitoring	g 6. ction Yes	. Total Depth	(ft.) 25]	
Type of Well Monitoring	g 6. ction Yes	. Total Depth	(ft.) 25	Diar	neter (in.) 2	3	
Type of Well Monitorin Formation clear of obstruc Detains of Plugging (bento	g 6. ction Yes	. Total Depth	(ft.) 25	Diar	neter (in.) 2	3	
Type of Well Monitoring Formation clear of obstruct Detains of Plugging (bento Filled with Chip Bento	g 6. ction Yes	. Total Depth r other materia From (ft.)	(ft.) 25 als) 25	Diar	neter (in.) 2		
Type of Well Monitorin Formation clear of obstruc Detains of Plugging (bento Filled with Chip Bento Kind of plug Soil	g 6. ction Yes	. Total Depth r other materia From (ft.) From (ft.)	(ft.) 25 als) 25	Diar Diar	neter (in.) 2		
Type of Well Monitoring Formation clear of obstruct Detains of Plugging (bento Filled with Chip Bento Kind of plug Soil Filled with	g 6. ction Yes	. Total Depth r other materia From (ft.) From (ft.) From (ft.)	(ft.) 25 als) 25	Diar biar biar biar biar biar biar biar b	neter (in.) 2		
Type of Well Monitoring Formation clear of obstruct Detains of Plugging (bento Filled with Chip Bento Kind of plug Soil Filled with Kind of plug	g 6. ction Yes	Total Depth r other materia From (ft.) From (ft.) From (ft.) From (ft.)	(ft.) 25 als) 25	Diar Diar	neter (in.) 2		
Type of Well Monitoring Formation clear of obstruct Detains of Plugging (bento Filled with Chip Bento Kind of plug Soil Filled with Filled with Filled with Kind of plug CASING RECORD Uppe	g 6. ction Yes onite, neat cement of onite	Total Depth r other materia From (ft.) From (ft.) From (ft.) From (ft.) From (ft.) From (ft.)	(ft.) 25 als) 25	Diar Diar Diar	neter (in.) 2		3
Type of Well Monitoring Formation clear of obstruct Detains of Plugging (bento Filled with Chip Bento Kind of plug Soil Filled with Filled with Filled with	g 6. ction Yes 6. conite, neat cement or conite	Total Depth r other materia From (ft.) From (ft.) From (ft.) From (ft.) From (ft.) From (ft.)	(ft.) 25 als) 25	Diar Diar to (ft to (ft to (ft to (ft to (ft 10. Date we erforming we	neter (in.) 2 .)	0	3

cal health department or ер 217-782-5830, TTY (for hearing impaired only) 800-547-0466.



Appendix C. Groundwater Quality Results for August 2010 to May 2013

Hydrogeologic Assessment Joppa Generating Station, Joppa, IL Electric Energy Inc. and Ameren Energy Generating Company

Monitoring		Depth to	35 IAC 620	pH (SU)	TDS	Nitrogen, Nitrate	Arsenic	Barium	Beryllium	Boron	Cadmium	Chromium	Cobalt	Copper	Iron	Manganese	Nickel	Selenium	Silver	Zinc	Antimony			Mercury	1. 1. 1. 1. 1.	Sulfate	Fluoride	
Well	Date	GW ² (ft)	Standard ¹	6.5-9.0	1200	100	0.20	2.0	0,5	2.0	0.050	1.0	1.0	0.65	5,0	10.0	2.0	0.05	ns	10.0	0.024	0.10	0.020	0.010	0.60	400	4.0	200
G101	8/17/2010	45.25	-	7.13	344	2.1	<0.0250	0.103	<0.0010	<0.0200	<0.00200	<0.0100	<0.0100	<0.0100	1.34	0.0556	<0.010	< 0.050	<0.010	<0.010	<0.0050	0.0026	< 0.0020	<0.00020	< 0.0070	32	0.26	7.0
G101	11/5/2010	dry																				-0.0000		-0.00000	-0.0070	-	0.07	6.0
G101	03/15/11	44.88		6.63	294	1.72	<0.0250	0.09	<0.0010	<0.020	<0.0020	<0.0100	<0.0100	<0.0100	0.172	<0.0050	<0.010	<0.050	<0.010	<0,010	<0.0050	<0.0020	<0.0020	<0.00020		32 34	0.27	6.0 5.0
G101	06/16/11	39.64		7.18	276	1.6	<0.025	0.64	<0.0010	<0.020	<0.0020	<0.010	<0.010	<0.010	<0.020	<0.0050 <0.0050	<0.010	<0.050	<0.010	<0.010	<0.0050	<0.0020				28	0.32	3.0
G101 G101	09/13/11 11/29/11	46.24 46.32		6,88 7,19	222 268	1.6	<0.025 <0.025	0.061	<0.0010	<0.020	<0.0020	<0.010	<0.010	<0.010	<0.020	<0.0050	< 0.010	<0.050	<0.010	<0.010	<0.0050	<0.0020	<0.0020			35	0.28	4.0
G101	02/14/12	48.12		6.88	216	0.28	<0.025	0.58	<0.0010	<0.020	<0.0020	<0.010	<0.010	<0.010	<0.020	<0.0050	<0.010	<0.050	<0.010	<0.010	<0.0050			<0.00020		35	0.30	4.0
G101	05/15/12	45.59		7.31	208	0.82	<0.025	0.044	< 0.0010	<0.020	<0.0020	<0.010	<0.010	<0.010	<0.020	<0.0050	<0.010	<0.050	<0.010	<0.010	<0,0050	<0.0020	<0.0020	<0.00020	<0.0070	22	0.31	4.0
G101	08/07/12	dry			-																							
G101	03/06/13	47.40		7.06	214	1.7	< 0.010	0.069	< 0.0010	<0.020	<0.0020	< 0.010	<0.010	< 0.010	<0.020	<0.0050	<0.010	<0.050	<0.010	<0.010	<0.0050	<0.0070		<0.00020		33	0.33	<5.0
G101	05/13/13	49.68		6.81	272	1.4	<0.010	0.076	<0.0010	<0.020	<0,0020	< 0.010	<0.010	< 0.010	<0.020	<0.0050	< 0.010	<0.050	<0.010	< 0.010	<0.0060	<0.0070	< 0.0020	<0.00020	<0.0070	33	0.28	5.0
G111	8/17/2010	8.00		7.30	342	0.092	<0.025	0.15	<0.0010	<0.020	<0.0020	<0.010	<0.010	<0.010	0.45	<0.0050	<0.010	<0.050	<0.010	< 0.010	<0,0050	<0.0020	<0.0020	<0.00020	<0.0070	25	0.62	8.0
G111	11/5/2010	9.77		6.70	330	0.72	<0.025	0.15	< 0.0010	<0.020	<0.0020	< 0.010	<0.010	<0.010	<0.020	<0.0050	< 0.010	< 0.050	< 0.010	0.013	<0.0050	<0.0020	<0.0020			22	0,70	6.0
G111	03/15/11	4.90		7.07	322	0.10	<0.025	0.16	<0.0010	<0.020	<0.0020	< 0.010	<0.010	< 0.010	<0.020	<0.0050	<0.010	<0.050	<0.010	0.018	<0.0050	<0.0020				23	0.67	7.0
G111	06/16/11	6.42		7.11	372	0.17	<0.025	0.16	<0.0010	<0.020	<0.0020	<0.010	<0.010	<0.010	<0.020	< 0.0050	<0.010	<0.050	< 0.010	<0.010	<0.0050	<0.0020				27	0.63	6.0
G111	09/13/11	8.45		7.10	330	0.13	<0.025	0.18	<0.0010	<0.020	<0.0020	< 0.010	<0.010	<0.010	<0.020	<0.0050	<0.010	<0.050	<0.010	<0.010	<0.0050	<0.0020				24	0.63	6.0 6.0
G111	11/29/11	4.68		7.05	376	0.15	<0.025	0.18	<0.0010	<0.020	<0.0020	<0.010	<0.010	<0.010	<0.020	<0.0050	< 0.010	<0.050	<0.010	<0.010	<0.0050	<0.0020				19 27	0.62	7.0
G111	02/14/12	4.55		7.23	354	0.093	<0.025	0.16	<0.0010	<0.020	<0.0020	<0.010	<0.010	<0.010	<0.020	<0.0050 <0.0050	<0.010	<0.050 <0.050	<0.010	<0.010	<0.0050	<0.0020	<0.0020			30	0.67	7.0
G111	05/15/12	6.68		7.14	324 394	0.12 0.052	<0.025 <0.025	0.17	<0.0010 <0.0010	<0.020	<0.0020	<0.010	<0.010	<0.010 <0.010	<0.020	<0.0050	<0.010	<0.050	<0.010	<0.010	<0.0050	<0.0020				26	0.69	5.0
G111 G111	08/07/12 03/07/13	9.22 5.20		7.02	394	0.052	<0.025	0.15	<0.0010	<0.020	<0.0020	<0.010	<0.010	<0.010	<0.020	<0.0050	<0.010	<0.050	<0.010	<0.010	<0.0050	<0.0070				20	0.63	6.0
GIII	05/14/13	4.68		7.05	374	<0.050	<0.010	0.17	<0.0010	<0.020	<0.0020	< 0.010	<0.010	<0.010	<0.020	<0.0050	<0.010	<0.050	<0.010	<0.010	<0.0060	<0.0070				19	0.71	7.0
CELUI AND		a Latitudes	_		2011		a contractory		a training of a loss	a registrerer -	CONTRACTOR AND INCOME.	haven		Contraction of	1000		<0.010	<0.050	<0.010	<0.010	<0.0050	<0.0070	<0.0020	<0.00020	<0.0070	63	0.74	<5.
G112C	03/07/13	5.25		6.79	412	0.34	<0.010	0.062	<0.0010	3.3	<0.0020	<0.010	<0.010	<0.010	0.048	0.18	<0.010	<0.050	<0.010	<0.010	<0.0050	<0.040	<0.0020			66	0.80	<5.
G112C G112C	04/17/13 05/14/13	5.31 2.64		6.92 6.73	476 432	<0.050 <0.050	<0.010	0.059	<0.0010 <0.0010	3.1 3.1	<0.0020	<0.010	<0.010	<0.010	<0.039	0.15	<0.010		<0.010	<0.010	<0.0060	<0.0070				60	0.81	<5.
				1.001/0					and the second states		- and the second						California (15.91	174765	The sort	and the second second	101120000	1.		The state of the	61	0.43	27
G113	8/17/2010	15.40		6.89	542	0.84	< 0.025	0.35	< 0.0010	<0.020	<0.0020	<0.010	< 0.010	<0.010	0.040	0.092	<0.010	<0.050	<0.010	<0.010	<0.0050	<0.0020		<0.00020		35	0.45	29
G113	11/5/2010 03/15/11	15.80		6.57 6.57	524 540	0.14 0.33	<0.025	0.40	<0.0010	<0.020 <0.020	<0.0020	<0.010 <0.010	<0.010	<0.010 <0.010	<0.020 <0.020	0.0064	<0.010		<0.010	<0.010	<0.0050	<0.0020				36	0.44	29
G113 G113	06/16/11	13.66		6.60	590	0.35	<0.025	0.45	<0.0010	<0.020	<0.0020	<0.010	<0.010	<0.010	<0.020	<0.0050	<0.010		< 0.010	< 0.010	< 0.0050	<0.0020		<0.00020		32	0.39	29
G113	09/13/11	14.90		6.54	554	0.40	<0.025	0.49	< 0.0010	<0.020	<0.0020	< 0.010	< 0.010	< 0.010	<0.020	<0.0050	<0.010		<0.010	<0.010	<0.0050	<0.0020	<0.0020	<0.00020	<0.0070	30	0.40	29
G113	11/29/11	11.50		6,44	636	0.68	<0.025	0.51	<0.0010	<0.020	<0.0020	<0.010	<0.010	<0.010	<0.020	<0.0050	<0.010	<0.050	<0.010	<0.010	<0.0050	<0.0020		<0.00020		34	0.39	28
G113	02/14/12	12.05		6.56	590	0.48	<0.025	0.50	< 0.0010	<0.020	<0.0020	< 0.010	<0.010	<0.010	<0.020	<0.0050	<0.010	<0.050	<0.010	<0.010	<0.0050	<0.0020		<0.00020		35	0.42	31
G113	05/15/12	14.25		6,71	586	0.57	<0.025	0.53	<0.0010	< 0.020	<0.0020	<0.010	<0.010	<0.010	<0.020	<0.0050	< 0.010		< 0.010	<0.010	<0.0050	< 0.0020		< 0.00020		32	0.43	34
G113	08/07/12	16.65		6.50	666	0.48	<0,025	0.47	<0.0010	<0.020	<0.0020	< 0.010	<0.010	< 0.010	<0.020	<0.0050	< 0.010		<0.010	< 0.010	<0.0050	<0.0020		<0,00020		30 37	0.45	29
G113	03/07/13	12.65		6.82	606	0.53	<0.010	0.54	<0.0010	<0.020	<0.0020	< 0.010	<0.010	< 0.010	<0.020	0.0076	<0.010		<0.010	<0.010	<0.0050	<0.0070		<0.00020		50	0.42	30
G113	05/14/13	12.12		6.65	706	0.38	<0.010	0.55	<0.0010	<0.020	<0.0020	<0.010	<0.010	<0.010	<0.020	<0.0050	<0.010										and the second	
G151	8/17/2010	42.70		6.70	348	1.0	<0.025	0.52	0.0025	8,3	<0.0020	0.023	0.033	0.028	18	0.47	0.021	<0.050	<0.010	0.061	<0.0050	0.027	< 0.0020	<0.00020	<0.0070	93	0.17	16
G151	11/5/2010	dry									-		and sector	-					-0.010	-0.040	-0.0050	-0.0000	-0.0000	-0.00000	<0.0070	100	<0.10	6.0
G151	03/16/11	38.10		5,89	236	1.1	<0.025	0.11	< 0.0010	< 0.020	<0.0020	<0.010	<0.010	<0.010	<0.020	0.062	<0.010		<0.010	<0.010	<0.0050	<0.0020		<0.00020		103	<0.10	5.0
G151	06/17/11	36.83		6,13	242	1,1	<0.025	0,79	<0.0010	<0.020	<0.0020	< 0.010	<0,010	<0.010	0.038	0.036	<0.010		<0.010	<0.010	<0.0050	<0.0020		<0.00020		103	0.10	5.0
G151	09/13/11	41.45 42.20		5,99 6.20	228 256	1.2	<0.025 <0.025	0.086	<0.0010 <0.0010	<0.020	<0.0020	<0.010	<0.010	0.011	1.8	0.045	<0.010		<0.010	0.017	<0.0050	<0.0020		<0.00020		98	0.95	5.0
G151 G151	11/29/11 02/14/12	37.80		6.03	254	0,62	<0.025	0.074	<0.0010	<0.020	<0.0020	<0.010	<0.010	<0.010	<0.020	0.022	<0.010		<0.010	0.017	<0.0050	<0.0020		<0.00020		110	<0.10	5.0
G151	05/15/12	41.82		6.00	232	0.63	<0.025	0.081	<0.0010	<0.020	<0.0020	<0.010	<0.010	<0.010	0.060	0.011	<0.010		<0.010	0.014	<0.0050	<0.0020		<0.00020		111	<0.10	5.0
G151	08/07/12	dry		(Constant)		and the second	Constant.	area.	NAME AND A DESCRIPTION OF A DESCRIPTIONO		COLUMN .	1001201201	and the	- 3070205														
G151	03/06/13	39.49		6.02	288	2.0	<0.010	0.069	<0.0010	<0.020	<0.0020	< 0.010	<0.010	<0.010	<0.020	0.015	< 0.010		<0.010	<0.010	<0.0050	<0.0070		<0.00020		99	<0.10	6.0
G151	05/13/13	37.13		5.96	282	1.6	< 0.010	0.068	< 0.0010	< 0.020	<0.0020	<0.010	<0.010	<0.010	<0.020	0.011	<0.010	< 0.050	< 0.010	<0.010	<0.0050	<0.0070	<0.0020	<0.00020	<0.0070	102	<0.10	6.0
G152B	03/07/13	33.80		6.81	478	0.87	< 0.010	0.51	<0.0010	<0.020	<0.0020	<0.010	<0.010	< 0.010	<0.020	0.015	< 0.010	< 0.050	< 0.010	<0.010	<0.0050	<0.0070	<0.0020	<0.00020	<0.0070	18	0.58	48
G152B	05/14/13	17.08		6.81	488	0.82	< 0.010	0.51	<0.0010	< 0.020	<0.0020	<0.010	<0.010	<0.010	<0.020	<0.0050	<0.010	<0.050	<0.010	< 0.010	<0.0050	<0.0070	<0.0020	<0.00020	<0.0070	16	0.60	49
Contraction of the	· · · · · · · · · · · · · · · · · · ·	and the second second		and the second second	1.1.1.1.1	-	and the second	set les		1.	and the second second				15	0.22	0.012	<0.050	<0.010	0.025	<0.0050	0.019	<0.0020	<0.00020	<0.0070	102	0.64	18
G153	8/17/2010	38,13		6.90	462	0.30	<0.025	0.63	0.0024	0.034	<0.0020	0.025	0.025	0.019	1.5	0.22	0.012	-0.030	40.010	0.020	40.0000	0.010	-0.0010			199	or states	18
G153 G153	11/5/2010 03/16/11	dry 37.82		6.70	434	0.46	<0.025	0,31	<0.0010	<0.020	<0.0020	< 0.010	<0,010	<0.010	<0.020	<0.0050	<0.010	<0.050	<0.010	<0.010	<0.0050	<0.0020	<0.0020	<0.00020	<0.0070	110	0.82	20
G153	06/17/11	32.62		6.94	484	0.37	<0.025	0.27	<0.0010	0.047	<0.0020	<0.010	<0.010	<0.010	<0.020	<0.0050	<0.010		<0.010	<0.010	<0.0050	<0.0020		<0.00020		104	0.76	20
G153	09/13/11	39.55		6.91	408	0.31	<0.025	0.28	<0.0010	<0.020	<0.0020	<0.010	<0.010	<0.010	0.029	<0.0050	<0,010		<0.010	<0.010	<0.0050	<0,0020		<0.00020	<0.0070	104	0.75	2
G153	11/29/11	40.17		6.92	432	0.27	<0.025	0.24	< 0.0010	0.055	<0.0020	<0.010	<0.010	<0.010	0,029	0.056	<0.010		<0.010	<0.010	<0.0050	<0.0020		<0.00020	<0.0070	107	0.77	2
G153	02/14/12	32.9		6.92	434	0.29	<0.025	0.24	<0.0010	<0.020	<0.0020	<0.010	<0,010	< 0.010	<0.020	<0.0050	< 0.010		< 0.010	<0.010	<0.0050	<0.0020		<0.00020		99	0.82	2
G153	05/15/12	38.92		6.95	406	0.21	<0.025	0.21	<0.0010	<0.020	<0.0020	<0.010	<0.010	<0.010	<0.020	<0.0050	< 0.010	<0.050	<0.010	<0.010	<0.0050	<0,0020	<0.0020	<0.00020	<0.0070	111	0.87	24
G153	08/07/12	dry																					0.0000	-0.00000	-0.0070	24	0.07	
G153	03/06/13	39.95		6.98	392	0.28	<0.010	0.23	< 0.0010	<0.020	<0.0020	<0.010	<0.010	< 0.010	0.040	<0.0050	< 0.010		< 0.010	< 0.010	<0.0050			<0.00020		94	0.87	21
G153	05/13/13	33.37		6,93	454	0.28	<0.010	0.23	< 0.0010	< 0.020	< 0.0020	<0,010	<0.010	<0.010	0.022	< 0.0050	<0.010	<0.050	<0.010	<0.010	<0.0050	<0.0070	<0.0020	<0.00020	~0.0070	93	0.94	2

ns indicates no standard for the listed parameter

Notes: Unless otherwise noted, all results are in mg/L. ¹ 35 IAC 620.420 Groundwater Quality Standards for Class II Potable Resource Groundwater, ns indicates no sta ² Depth to water as measured from top of well casing (in feet). Yellow highlighted cells represent results exceeding 35 IAC 620.420 Groundwater Quality Standards for Class II General Resource Groundwater,

Appendix C. Groundwater Quality Results for August 2010 to May 2013

Hydrogeologic Assessment Joppa Generating Station, Joppa, IL Electric Energy Inc. and Ameren Energy Generating Company

Monitoring Well	Date	Depth to GW ² (ft)	35 IAC 620 p Standard ¹	H (SU) ns*	TDS ns*	Nitrogen, Nitrate 100	Arsenic 0.20	Barium ns*	Beryllium 0.5	Boron ns*	Cadmium 0.05	Chromium 1.0	Cobalt	Copper ns*	Iron ns*	Manganese ns*	Nickel ns*	Selenium ns*	Silver	Zinc ns*	Antimony 0.024	Lead 0.1	Thallium 0.020	Mercury 0.010	Cyanide 0.60	Sulfate	Fluoride 4.0	Chlorid
G112B	8/17/2010	26.42		6.05	744	0.95	<0.025	0.086	<0.0010	3.5	<0.0020	<0.010	0.065	<0,010	13	4.3	0.035	<0.050	<0.010	0.055	<0.0050	<0.0020	<0.0020	<0.00020	<0.0070	298	0.29	56
G112B	11/5/2010	26.18		6.33	754	<0.050	< 0.025	0,12	< 0.0010	1.6	<0.0020	<0.010	0.032	< 0.010	22	4.1	0.020	<0.050	< 0.010	0.015	<0.0050	<0.0020	<0.0020	<0,00020	<0.0070	129	0.49	49
G112B	03/15/11	15,50		5.80	856	0.055	0.037	0.082	<0.0010	4.4	<0.0020	<0.010	0.081	< 0.010	53	5,5	0.043	<0.050	<0.010	0.043	<0.0050	<0.0020	<0.0020	<0,00020	<0.0070	352	0.29	56
G112B	06/16/11	22.03		6.60	776	0.12	<0.025	0.10	< 0.0010	3.5	<0.0020	< 0.010	0.067	< 0.010	45	5.1	0.037	< 0.050	< 0.010	0.022	<0.0050	< 0.0020	< 0.0020	< 0.00020	<0.0070	302	0.28	55
G112B	09/13/11	26.05		6.51	778	0.15	0.058	0.20	< 0.0010	0.44	< 0.0020	<0.010	0.020	< 0.010	75	4.6	0.013	<0.050	<0.010	0.022	<0.0050	<0.0020	< 0.0020	<0.00020	< 0.0070	37	0.63	40
G112B	11/29/11	20.80		6.35	804	< 0.050	0.054	0.17	< 0.0010	2.0	<0.0020	< 0.010	0.037	<0.010	68	4.3	0.024	<0.050	< 0.010	0.014	<0.0050	<0.0020	<0.0020	< 0.00020	<0.0070	176	0.46	56
G112B	02/14/12	9.72		6.33	860	< 0.050	0.058	0.17	< 0.0010	1.9	<0.0020	< 0.010	0.042	<0.010	71	4.7	0.025	<0.050	< 0.010	0.020	< 0.0050	<0.0020	< 0.0020	< 0.00020	<0.0070	147	0.52	50
G112B	05/15/12	24.01		6.64	778	< 0.050	0.066	0.21	< 0.0010	0.35	<0.0020	< 0.010	0.016	< 0.010	77	4.5	<0.010	<0.050	<0.010	0.020	<0.0050	<0.0020	<0.0020	< 0.00020	<0.0070	21	0.78	52
G112B	08/07/12	28.45		6.50	860	<0.050	0.060	0.20	<0.0010	0.051	<0.0020	<0.010	0.010	<0.010	62	4.2	<0.010	<0.050	< 0.010	<0.010	<0.0050	<0.0020	<0.0020	<0.00020	<0.0070	15	0.83	67
G152	8/17/2010	9.21		6.41	1110	0.92	<0.025	0.019	< 0.0010	12	<0.0020	< 0.010	<0.010	<0.010	0.045	0.19	< 0.010	<0.050	<0.010	<0.010	<0.0050	<0.0020	<0.0020	< 0.00020	<0.0070	768	0.12	21
G152	11/5/2010	5.42		6.03	1090	0.070	<0.025	0.017	< 0.0010	12	< 0.0020	< 0.010	<0.010	< 0.010	<0.020	0.17	< 0.010	<0.050	<0.010	<0.010	<0.0050	<0,0020	<0.0020	<0.00020	< 0.0070	692	0.16	22
G152	03/16/11	2.20		5.98	1080	<0.050	<0.025	0.015	< 0.0010	11	<0.0020	< 0.010	<0.010	< 0.010	<0.020	0.0050	< 0.010	<0.050	< 0.010	<0.010	<0.0050	<0.0020	<0.0020	<0.00020	<0.0070	731	0.12	22
G152	06/17/11	3.92		5.97	1020	<0.050	<0.025	0.012	<0.0010	11	<0.0020	< 0.010	< 0.010	< 0.010	<0.020	0.0068	<0.010	<0.050	<0.010	< 0.010	<0.0050	< 0.0020	< 0.0020	< 0.00020	<0.0070	593	0.11	21
G152	09/13/11	5.34		5.91	922	<0.050	<0.025	0.013	<0.0010	12	<0.0020	< 0.010	<0.010	<0.010	<0.020	0.014	< 0.010	< 0.050	< 0.010	<0.010	<0.0050	<0.0020	<0.0020	<0.00020	<0.0070	570	0.14	21
G152	11/29/11	22.50		6.04	910	0.10	<0.025	0.016	<0.0010	11	<0.0020	< 0.010	<0.010	< 0.010	<0.020	0.0083	< 0.010	<0.050	< 0.010	<0.010	<0.0050	< 0.0020	< 0.0020	< 0.00020	<0.0070	565	0.12	20
G152	02/14/12	18.20		6.25	878	<0.050	<0.025	0.012	<0.0010	11	<0.0020	< 0.010	<0.010	<0.010	<0.020	< 0.0050	<0.010	< 0.050	< 0.010	<0.010	<0.0050	<0.0020	< 0.0020	<0.00020	<0.0070	605	0.14	24
G152	05/15/12	5.07		6.03	866	0.14	<0.025	0.012	< 0.0010	11	<0.0020	< 0.010	<0.010	<0.010	<0.020	<0.0050	< 0.010	< 0.050	<0.010	<0.010	<0.0050	<0.0020	<0.0020	<0.00020	<0.0070	572	0.13	25
G152	08/07/12	8.03		5.81	956	<0.050	<0.025	0.011	< 0.0010	11	<0.0020	< 0.010	<0.010	< 0.010	<0.020	0.014	< 0.010	< 0.050	<0.010	<0.010	< 0.0050	< 0.0020	< 0.0020	<0.00020	< 0.0070	451	0.15	21

ns*

 Notes:

 Unless otherwise noted, all results are in milligrams per Liter (mg/L).

 1
 35 IAC 620.420 Groundwater Quality Standards for Class II Potable Resource Groundwater.
 ns
 indicates no s

 2
 Depth to water as measured from top of well casing (in feet).
 Yellow highlighted cells represent results exceeding 35 IAC 620.420 Groundwater Quality Standards for Class II General Resource Groundwater.

ns indicates no standard for the listed parameter

indicates no standard for monitored points meeting criteria of 35 IAC 620.420(a)(3): applies to G112B and G152

Page 2 of 2

Exhibit C

	1	9350	IL00041	.71			ctric Energy, Inc.		ON	AB No. 2
Form 2F NPDES	9	epa	STODMM		ation for	NPDES	ental Protection Permit to Disch SSOCIATED W	arge Wastew		
SECTIO			TION (40 CFR 122.21		ISCHAP	IOLS A	SSOCIATED W		RIAL ACTIN	////
OLONO	1.1	Provide inf	ormation on each of th	e facility's	outfalls i	n the tab	e below		and the second second	-9
		Outfall Number	Receiving Water N			Lati			Longitud	e
_		011	UnName Trib to Ohio	River	37.00°	12.00′	40.00″	-88.00°	52.00′ 5	.00″
Outfall Location		012	UnName Trib to Ohio	River	37.00°	12.00′	37.00″	-88.00°	51.00′7	.00″
ıtfall L		013	UnName Trib to Ohio	River	37.00°	12.00′	37.00"	-88.00°		.00″
õ					•	,	n n	•	,	"
						,	"	0	,	"
SECTION	N 2. IMPI	ROVEMENTS	(40 CFR 122.21(g)(6))						1
	2.1	upgrading,	esently required by any or operating wastewate ischarges described in	er treatme	nt equipn	nent or p	ractices or any o	ther environm	ental program	s that o
	2.2		ify each applicable proj	ject in the	table bel	OW.				
			<u>, , , , , , , , , , , , , , , , , , , </u>	1					1	
			dentification and	27.0 0000 Million 200 Million	d Outfalls		Source(s) of Di	scharge	Final Com	pliance
			dentification and iption of Project	27.0 0000 MSC MID 2810 MSD 0	d Outfalls		Source(s) of Di	scharge	Final Com Required	
				27.0 0000 MSC MID 2810 MSD 0			Source(s) of Di	scharge		
				27.0 0000 MSC MID 2810 MSD 0			Source(s) of Di	scharge		
lents				27.0 0000 MSC MID 2810 MSD 0			Source(s) of Di	scharge		
orovements				27.0 0000 MSC MID 2810 MSD 0			Source(s) of Di	scharge		
Improvements				27.0 0000 MSC MID 2810 MSD 0			Source(s) of Di	scharge		
Improvements	-			27.0 0000 MSC MID 2810 MSD 0			Source(s) of Di	scharge		
Improvements				27.0 0000 MSC MID 2810 MSD 0			Source(s) of Di	scharge		
Improvements				27.0 0000 MSC MID 2810 MSD 0			Source(s) of Di	scharge		
Improvements				27.0 0000 MSC MID 2810 MSD 0			Source(s) of Di	scharge		
Improvements	2.3	Descr		(list outfa	all numbers				Required	Pro

	120001	979350	IL00041	Number 71	Ele	Facility Name Form Ap ctric Energy, Inc. OM	B No. 2040-0
ECTIO	N 3. S	ITE DRAINA	GE MAP (40 CFR 122.26	(c)(1)(i)(A))			
Drainage Map	3.	riave ye	ou attached a site drainage guidance.)	e map containing	all require	d information to this application? (See instruc	tions for
Dra		12 Y	′es		No		
CTIO	N 4. P	OLLUTANT S	SOURCES (40 CFR 122.2	26(c)(1)(i)(B))			
	4.1		information on the facility's		es in the ta	ble below.	
		Outfal		ous Surface Area		Total Surface Area Drained	
		Numbe	er (within a mile	e radius of the facility		(within a mile radius of the facility)	specify un
		011	0	sp	ecify units	160	acres
					acres		
		012	0.01	· · · · ·	ecify units	3	specify un
		012	0.01		acres	3	acres
				spe	ecify units	27	specify un
		013	0.1		acres	37	acres
				spe	cify units		specify un
				spe	cify units		specify uni
				spec	cify units		specify un
							, ,
				y to control weed uses a Storm Wat	ls. EEI use er Pollutio	coal combustion byproducts. Outfalls have s s Spill Control and Countermeasure Plan to n Prevention Plan to minimize storm water and chemicals.	o minimiz
	4.3	storm wate	r exposure to spills. EEI u location and a descriptior	y to control weed ises a Storm Wat materials, by	ds. EEI use er Pollutio products, tural and r	s s Spill Control and Countermeasure Plan to n Prevention Plan to minimize storm water	o minimiz exposure
	4.3	storm wate	r exposure to spills. EEI u	to control weed ises a Storm Wat materials, by of existing structor or specific guidar	ds. EEI use er Pollutio y products, ctural and r nce.)	s s Spill Control and Countermeasure Plan to n Prevention Plan to minimize storm water and chemicals.	o minimiz exposure
	4.3	storm wate	r exposure to spills. EEI u location and a descriptior	to control weed ises a Storm Wat materials, by of existing structor or specific guidar	ds. EEI use er Pollutio products, tural and r	s s Spill Control and Countermeasure Plan to n Prevention Plan to minimize storm water and chemicals.	o minimiz exposure ollutants i
	4.3	storm wate	r exposure to spills. EEI u location and a descriptior	to control weed ises a Storm Wat materials, by of existing struc or specific guidar Storm	ds. EEI use er Pollutio products, ctural and r nce.) nwater Trea	s s Spill Control and Countermeasure Plan to n Prevention Plan to minimize storm water and chemicals.	o minimiz exposure ollutants i from Exhibi
		storm wate Provide the stormwater i	r exposure to spills. EEI u location and a descriptior runoff. (See instructions fo	y to control weed ises a Storm Wat materials, by n of existing struc or specific guidar Storm Control M	ds. EEI use er Pollutio y products, ctural and r nce.) nwater Trea	s s Spill Control and Countermeasure Plan to n Prevention Plan to minimize storm water and chemicals. non-structural control measures to reduce p atment	o minimiz exposure ollutants i from Exhibi 2F-1 (list)
	c	Provide the stormwater Outfall Number	r exposure to spills. EEI u location and a descriptior runoff. (See instructions fo NaturalVegetation&Gra NaturalVegetation&Gra	y to control weed ises a Storm Wat materials, by n of existing struc or specific guidar Storm Control M ivelUsed forStorr velUsed forStorr	ds. EEI use er Pollutio y products, ctural and r nce.) nwater Trea leasures an mWaterMi mWaterMi	s s Spill Control and Countermeasure Plan to n Prevention Plan to minimize storm water and chemicals. non-structural control measures to reduce p atment nd Treatment gmt(SeeRef Infomation forOutfallLocation) gmt(SeeRef Infomation forOutfallLocation)	o minimiz exposure ollutants i from Exhibi 2F-1 (list)
	0	storm water Provide the stormwater Outfall Number	r exposure to spills. EEI u location and a descriptior runoff. (See instructions fo NaturalVegetation&Gra NaturalVegetation&Gra	y to control weed ises a Storm Wat materials, by n of existing struc or specific guidar Storm Control M ivelUsed forStorr velUsed forStorr	ds. EEI use er Pollutio y products, ctural and r nce.) nwater Trea leasures an mWaterMi mWaterMi	s s Spill Control and Countermeasure Plan to n Prevention Plan to minimize storm water and chemicals. non-structural control measures to reduce p atment nd Treatment gmt(SeeRef Infomation forOutfallLocation)	o minimiz exposure ollutants i from Exhibi 2F-1 (list)
	0	storm water Provide the stormwater i Outfall Number	r exposure to spills. EEI u location and a descriptior runoff. (See instructions fo NaturalVegetation&Gra NaturalVegetation&Gra	y to control weed ises a Storm Wat materials, by n of existing struc or specific guidar Storm Control M ivelUsed forStorr velUsed forStorr	ds. EEI use er Pollutio y products, ctural and r nce.) nwater Trea leasures an mWaterMi mWaterMi	s s Spill Control and Countermeasure Plan to n Prevention Plan to minimize storm water and chemicals. non-structural control measures to reduce p atment nd Treatment gmt(SeeRef Infomation forOutfallLocation) gmt(SeeRef Infomation forOutfallLocation)	o minimiz exposure ollutants i from Exhibi 2F-1 (list)

		Identificati		NPDES Permit Number IL0004171		cility Name c Energy, Inc.	Form Approved 03/05/19 OMB No. 2040-0004
\sim	SECTIC	NIS NO	N STORMWAY	TER DISCHARGES (40 CFR 122.26	(c)(1)(i)(C))		
(CEGIIC	5.1	I certify und presence o discharges i	der penalty of law that the outfall(s f non-stormwater discharges. More are described in either an accompan or type first and last name)	s) covered by th eover, I certify t	that the outfalls identified a	as having non-stormwater
			Signature			Date signed	
	les	5.2	Dravida that	testing information requested in the	table below		
	r Discharg	5.2	Outfall Number	Description of Testing M		Date(s) of Testing	Onsite Drainage Points Directly Observed During Test
(~	Non-Stormwater Discharges						
	SECTIO	and the second second	and the second second second second second second second second second second second second second second second	KS OR SPILLS (40 CFR 122.26(c))			
	Significant Leaks or Spills	6.1	Describe any	significant leaks or spills of toxic or	hazardous pollut	ants in the last three years.	
	SECTION	N 7. DISC	HARGE INFO	RMATION (40 CFR 122.26(c)(1)(i)(I	E))		
	Discharge Information	7.1	e. Not all applic Is this a new s Yes ➔	determine the pollutants and parameters and search table. ants need to complete each table. source or new discharge? See instructions regarding submissive data.		uired to monitor and, in turn No → See instructions reg actual data.	
	cha	7.2		pleted Table A for each outfall?			
C	Dis		✓ Yes			No	

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ALV. W. 4.

7.3 Is the facility subject to an effluent limitation guideline (ELG) or effluent limitations in an NPDES permit for its process watewater? Yes No → SKIP to item 7.5. 7.4 Have you completed Table B by providing quantitative data for those pollutants that are (1) limited either directly or indirectly in an ELG and/or (2) subject to effluent limitations in an NPDES permit for the facility's process wastewater? Pes No 7.5 Do you know or have reason to believe any pollutants in Exhibit 2F-2 are present in the discharge? Yes No 7.6 Have you used all pollutants in Exhibit 2F-2 that you know or have reason to believe are present in the discharge and provided quantitative data or an explanation for those pollutants in Table C? Pes No 7.7 Do you know or have reason to believe any pollutants in Exhibit 2F-3 are present in the discharge? Yes No 7.8 Do you know or have reason to believe any pollutants in Exhibit 2F-3 are present in the discharge? Yes No 7.8 Do you know or have reason to believe any pollutants in Exhibit 2F-3 that you know or have reason to believe are present in the discharge? Yes No 7.10 Do you expect any of the pollutants in Exhibit 2F-3 that you know or have reason to be discharged in concentrations of 10 ppb or greater? Yes No		Identificatio LD00197		NPDES Permit Number IL0004171		cility Name C Energy, Inc.	Form Approved 03/05/19 OMB No. 2040-0004
7.4 Have you completed Table B by providing quantitative data for those pollutants that are (1) limited either directly or indirectly in an ELG and/or (2) subject to effluent limitations in an NPDES permit for the facility's process wastewate? Pres No 7.5 Do you know or have reason to believe any pollutants in Exhibit 2F-2 are present in the discharge? Pres No → SKIP to tem 7.7. 7.6 Have you listed all pollutants in Exhibit 2F-2 that you know or have reason to believe are present in the discharge and provided quantitative data or an explanation for those pollutants in Table C? Pres No 7.7 Do you qualify for a small business exemption under the criteria specified in the Instructions? Pres No 7.8 Do you know or have reason to believe any pollutants in Exhibit 2F-3 are present in the discharge? Pres No 7.8 Do you know or have reason to believe any pollutants in Exhibit 2F-3 are present in the discharge? Pres No 7.0 Do you cove or have reason to believe are present in the discharge? Pres No 7.10 Do you know or have reason to believe are present in the discharge? Pres No 7.10 Do you expect any of the pollutants in Exhibit 2F-3 that you expect to be discharged in concentrations of 10 ppb or greater? <td></td> <td>7.3</td> <td></td> <td>subject to an effluent limitation guide</td> <td>line (ELG) or ef</td> <td>fluent limitations in ar</td> <td>NPDES permit for its process</td>		7.3		subject to an effluent limitation guide	line (ELG) or ef	fluent limitations in ar	NPDES permit for its process
Indirectly in an ELG and/or (2) subject to effluent limitations in an NPDES permit for the facility's process wastewater? Yes No 7.5 Do you know or have reason to believe any pollutants in Exhibit 2F-2 are present in the discharge? Yes No 7.6 Have you listed all pollutants in Exhibit 2F-2 that you know or have reason to believe are present in the discharge and provided quantitative data or an explanation for those pollutants in Table C? Yes No 7.7 Do you wow or have reason to believe any pollutants in Table C? Yes No 7.7 Do you wow or have reason to believe any pollutants in Exhibit 2F-3 are present in the discharge? Yes No 7.8 Do you wow or have reason to believe any pollutants in Exhibit 2F-3 are present in the discharge? Yes No 7.8 Do you wow or have reason to believe any pollutants in Exhibit 2F-3 that you know or have reason to believe are present in the discharge? Yes No 7.9 Have you listed all pollutants in Exhibit 2F-3 that you know or have reason to believe are present in the discharge in concentrations of 10 ppb or greater? Yes No 7.10 Do you expect any of the pollutants in Exhibit 2F-3 that you expect to be discharged in concentrations of 10 ppb or greater?							
7.5 Do you know or have reason to believe any pollulants in Exhibit 2F-2 are present in the discharge? Yes No → SKIP to Item 7.7. 7.6 Have you listed all pollutants in Exhibit 2F-2 that you know or have reason to believe are present in the discharge and provided quantitative data or an explanation for those pollutants in Table C? Yes No 7.7 Do you qualify for a small business exemption under the oriteria specified in the Instructions? Yes SKIP to Item 7.18. 0 yes No 7.8 Do you know or have reason to believe any pollutants in Exhibit 2F-3 are present in the discharge? Yes No 7.9 Have you listed all pollutants in Exhibit 2F-3 that you know or have reason to believe are present in the discharge? Yes No 7.10 Do you expect any of the pollutants in Exhibit 2F-3 that you know or have reason to believe are present in the discharge in Table C? 7.10 Do you expect any of the pollutants in Exhibit 2F-3 that you expect to be discharged in concentrations of 10 ppb or greater? Yes No 7.11 Have you provided quantitative data in Table C for those pollutants in Exhibit 2F-3 that you expect to be discharged in concentrations of 10 ppb or greater? Yes No 7.12 Do you expect acrolein, acrylonitrile, 2,4-dinitrophenol,		7.4	indirectly in a			NPDES permit for the	
Yes No → SKIP to Item 7.7. 7.6 Have you listed all pollutants in Exhibit 2F–2 that you know or have reason to believe are present in the discharge and provided quantitative data or an explanation for those pollutants in Table C? Yes No 7.7 Do you qualify for a small business exemption under the criteria specified in the Instructions? Yes No 7.8 Do you know or have reason to believe any pollutants in Exhibit 2F–3 are present in the discharge? Yes No 7.9 Have you listed all pollutants in Exhibit 2F–3 that you know or have reason to believe are present in the discharge? Yes No 7.9 Have you listed all pollutants in Exhibit 2F–3 that you know or have reason to believe are present in the discharge in Table C? Yes No 7.10 Do you expect any of the pollutants in Exhibit 2F–3 that you know or have reason to believe are present in the discharge in Table C? Yes No 7.11 Have you provided quantitative data in Table C for those pollutants in Exhibit 2F–3 that you expect to be discharged in concentrations of 10 ppb or greater? Yes No 7.12 Thave you provided quantitative data in Table C for those pollutants in Exhibit 2F–3 that you expect to be discharged in concentrations of 100 ppb or greater? Yes No <							- diashaana?
7.6 Have you listed all pollutants in Exhibit 2F-2 that you know or have reason to believe are present in the discharge and provided quantitative data or an explanation for those pollutants in Table C? Yes 7.7 Do you qualify for a small business exemption under the criteria specified in the Instructions? Yes → SKIP to Item 7.18. No 7.8 Do you know or have reason to believe any pollutants in Exhibit 2F-3 are present in the discharge? Yes No 7.10 Do you expect any of the pollutants in Exhibit 2F-3 to be discharged in concentrations of 10 ppb or greater? Yes Yes Yes <td></td> <td>1.5</td> <td></td> <td>or have reason to believe any polluta</td> <td></td> <td></td> <td>-</td>		1.5		or have reason to believe any polluta			-
Provided quantitative data or an explanation for those pollutants in Table C?		7.0					
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Image: SkiP to item 7.18. Image: No 7.8 Do you know or have reason to believe any pollutants in Exhibit 2F-3 are present in the discharge? Image: SkiP to item 7.10. No → SKIP to item 7.10. 7.9 Have you listed all pollutants in Exhibit 2F-3 that you know or have reason to believe are present in the discharge in Table C? Image: SkiP to item 7.10 Do you expect any of the pollutants in Exhibit 2F-3 to be discharged in concentrations of 10 ppb or greater? Image: SkiP to item 7.10 Do you expect any of the pollutants in Exhibit 2F-3 to be discharged in concentrations of 10 ppb or greater? Image: SkiP to item 7.12 T.11 Have you provided quantitative data in Table C for those pollutants in Exhibit 2F-3 that you expect to be discharged in concentrations of 10 ppb or greater? Image: Yes Image: No 7.12 Do you expect acrolein, acrylonitrile, 2,4-dinitrophenol, or 2-methyl-4,6-dinitrophenol to be discharged in concentration of 100 ppb or greater? Image: Yes Image: No 7.13 Have you provided quantitative data in Table C for the pollutants identified in item 7.12. 7.14 Have you provided quantitative data or an explanation in Table C for pollutants you expect to be discharge? Image: Yes Image: No 7.15 Do you know or have reason to believe any pollutants in Exhibit 2F-4 are present in the discharge?							
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E	PA Identifica		NPDES Permit Number IL0004171	Facility Name Electric Energy, Inc.	Form Approved 03/05/19 OMB No. 2040-0004
	Used	d or Manufactured Toxic	<u>s</u>		
Discharge Information Continued	7.18	Is any pollutant listed		a substance or a component of a sub product?	
matio	7.19	List the pollutants belo	ow, including TCDD if applicable.		
e Infoi		1.	4.	7.	
charg		2.	5.	8.	
Dis		3.	6.	9.	
Biological Toxicity Testing Data	8.1	Do you have any know any of your discharge	s or on a receiving water in relati	g)((11)) any biological test for acute or chron ion to your discharge within the last t	three years?
ty Te	8.2	Identify the tests and the		Submitted to NPDES	
oxicit		Test(s)	Purpose of Test(s) Permitting Authority?	Date Submitted
jical T				Yes No	
Biolog				Yes No	
				Yes No	
SECT	ION 9. ÇC 9.1		ORMATION (40 CFR 122.21(g) es reported in Section 7 (on Tab	(12)) les A through C) performed by a cor	ntract laboratory or
100		Yes		No → SKIP to Sec	tion 10.
	9.2	Provide information for	each contract laboratory or cons		
			Laboratory Number	1 Laboratory Number 2	Laboratory Number 3
ormation	1	Name of laboratory/firm	TekLab		
Contract Analysis Information		Laboratory address	5445 Horseshoe Lake Roa Collinsville, IL 62234	d	
Contra		Phone number	(618) 344-1004		
		Pollutant(s) analyzed	All Samples analyzed by La	ıb	

	Identificati	on Number '9350	NPDES Perm			acility Name ic Energy, Inc.	Form Approved 03/05/19 OMB No. 2040-0004
SECTIO	N 10. CI 10.1	each section, sp all applicants are	ow, mark the sec ecify in Column e required to con	ctions of Form 2F	that you have s that you are	completed and are su enclosing to alert the achments,	Jbmitting with your application. For permitting au thority. Note that not
		Column	1			Column 2	
		Section 1] w/ attachmen	ts (e.g., respo	nses for additional ou	tfalls)
		Section 2] w/ attachmen	ts		
		Section 3	E] w/ site draina	ge map		
		Section 4		w/ attachmen	ts		
		Section 5	C	w/ attachmen	ts		
It		Section 6	C	w/ attachmen	ts		
ateme		Section 7	L ا	Table A		w/ small business e	exemption request
on Sta			E	Table B		w/ analytical results	s as an attac hment
Checklist and Certification Statement			L	Table C	V	Table D	
d Cert		Section 8		w/attachments	5		
ist an		Section 9		w/attachments	s (e.g., respon	ses for additional con	tact laboratories or firms)
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0	10.2	Certification Sta	tement				
-		accordance with submitted. Based for gathering the	a system desig l on my inquiry o information, the ware that there a	ned to assure the f the person or pe information subn are significant per	at qualified pe ersons who ma nitted is, to the	rsonnel properly gat mage the system or t best of my knowled	der my direction or supervision in her and evaluate the information hose persons directly responsible ge and belief, true, accurate, and on, including the possibility of fine
		Name (print or typ	pe first and last r	name)	0	fficial title	
		Stephen Wait			Pla	ant Manager, Electric	Energy, Inc.
			ti N.	at	Di	ate signed	520


Exhibit D

BEFORE THE ILLINOIS POLLUTION CONTROL BOARD

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IN THE MATTER OF:	
Petition of Electric Energy, Inc.	
For a Finding of Inapplicability or, in the	
Alternative, an Adjusted Standard from	
35 Ill. Adm. Code Part 845	

AS 2021-005 (Adjusted Standard)

AFFIDAVIT OF LYNN E. DUNAWAY

I, Lynn E. Dunaway, certify under penalty of perjury pursuant to Section 1-109 of the Illinois Code of Civil Procedure, 735 ILCS 5/1-109, that the statements set forth in this affidavit are true and correct, and further state that if called upon to testify in this matter, I would competently testify as follows:

1. I am an Illinois Licensed Professional Geologist employed by the Illinois Environmental Protection Agency ("Illinois EPA" or "Agency") as an Environmental Protection Specialist IV in the Hydrogeology and Compliance Unit ("HCU") within the Groundwater Section of the Bureau of Water, and I am located in Springfield, Illinois. I have been employed by the Illinois EPA since February of 1988.

2. As a Geologist in the HCU, I work on the development and implementation of rules and regulations related to protecting, monitoring, and restoring groundwater in Illinois, and I provide technical expertise to the Bureau of Water Permit Section on groundwater issues. As part of these duties, I served as a witness on behalf of the Groundwater Section in support of Illinois EPA's proposed Part 845 throughout the Illinois Pollution Control Board's rulemaking proceedings in R2020-019.

3. I have reviewed the Petition of Electric Energy, Inc. for a Finding of Inapplicability or, in the Alternative, an Adjusted Standard from 35 Ill. Adm. Code Part 845 ("Petition").

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4. I have personal knowledge of the facts set forth in Illinois EPA's Recommendation to the Board as stated below.

5. Petitioner cites my testimony in support of its Petition. *See* Pet. Ex. 18. At hearing in R2020-019, when questioned whether Part 845 was intended to apply to the same ponds that are subject to requirements under Part 257, I responded: "In the Agency's opinion, they will be the same ones." Pet Ex. 18 at lines 17-24. To further explain my testimony, Part 257 is a self-implementing program, so the United States Environmental Protection Agency ("USEPA") neither selected nor approved which CCR surface impoundments should appropriately be regulated – that decision was left entirely to owners and operators of CCR surface impoundments, based on their interpretation of Part 257 and its Preamble. Therefore, Illinois EPA has maintained that the universe of regulated CCR surface impoundments is the same in both Part 845 and Part 257, but the Agency's interpretation of Part 257 and its Preamble may be different than some owners and operators.

6. I assisted in the drafting and review of Illinois EPA's comments submitted to USEPA on its proposed definition of "legacy ponds" in February 2021, provided as Petitioner's Exhibit 10. The in-depth review of aerial photos presented in Paragraphs 36 through 44 of the Recommendation and Petitioner's Exhibit 2 demonstrate that the Joppa West Ash Pond ("JWAP") does contain CCR and liquids and should be regulated by Part 257, by Petitioner's own interpretation of the Part 257 requirements. We used Petitioner's interpretation and application of the Part 257 requirements to the JWAP, which has been echoed by other owners and operators in Illinois, to demonstrate the number of CCR surface impoundments that may never be properly closed if the United States Environmental Protection Agency required legacy ponds to have obviously impounded water within them. The information contained in Petitioner's Exhibit 2, as

well as the extensive review of aerial photography and other documents discussed in Illinois EPA's Recommendation, showing areas of ponded water, sediment disposal within the JWAP and continued saturation of CCR, was not available at the time the Agency submitted its comments. That information demonstrates that the JWAP does contain CCR and liquids and should be considered regulated by Part 257 under Petitioner's own interpretation of the federal rules, contrary to the Agency's statements made at the time it submitted its comments to USEPA.

FURTHER AFFIANT SAYETH NOT

NN E DUNA

DATE

State of Illinois County of Sangamon

Subscribed and Sworn to before me this for day of November 2021.

OFFICIAL SEAL DAWN A. HOLLIS NOTARY PUBLIC. STATE OF ILLINOIS MY COMMISSION EXPIRES 03-21-2025

Exhibit E

Geochemistry and Reactive Transport of Metal Contaminants in Ground Water, Pinal Creek Basin, Arizona

James G. Brown, Pierre D. Glynn, and R.L. Bassett

ABSTRACT

Activities related to more than a century of large-scale copper mining in the Pinal Creek Basin in central Arizona have contaminated the regional alluvial aquifer and perennial streamflow with acidity and metals. Water-chemistry and solid-phase analyses and computer-aided geochemical modeling were used to understand the evolution of the ground-water plume between 1984 and 1998. The ground-water plume consists of three hydrochemical zones: (1) an acidic zone, which contains large concentrations of metals and has a pH that ranges from 3.6 to about 5; (2) a transition zone where carbonate-mineral dissolution causes pH to increase to above 5, which results in the precipitation of iron hydroxide and the adsorption of trace metals such as nickel and zinc; and (3) a neutralized zone, which contains large concentrations of manganese, calcium, and sulfate, and has a pH of about 6 to 7. Inverse geochemical modeling using NET-PATH revealed that, in addition to calcite dissolution, silicate dissolution was required to account for the mass transfers of calcium and magnesium across the transition zone. Analysis of the measured changes in plume geochemistry was aided by PHREEQC reactive-transport modeling, which helped determine that oxidation-reduction reactions were significant in the acidic zone of the plume through the late 1980's. The local equilibrium assumption required by reactive-transport modeling probably was invalid for oxidationreduction reactions that involved manganese and, to a lesser extent, neutralization reactions that involved calcite. Sensitivity analyses indicated that the rate of advance of the pH front was highly sensitive to the initial calcite concentration, and that ground water along a flow path near the base of the alluvium was in partial or indirect contact with the atmosphere, possibly through mixing with shallower water.

INTRODUCTION

Activities related to more than a century of large-scale copper mining in the Pinal Creek Basin in central Arizona (fig. 1) have contaminated the regional aquifer and perennial streamflow. Potential contaminant sources include mine tailings, unlined surface-water impoundments of mine-process water, heap-leach areas, and occasional spills of contaminated water into streambeds. Acidic ground-water contamination has a pH of about 3.6 to 5, and neutralized-contaminated water has a pH that ranges from about 6 in the aquifer to 8 in perennial streamflow. Contaminants that occur in large concentrations are iron (Fe), sulfate (SO_4) , manganese (Mn), copper (Cu), cobalt (Co), nickel (Ni), zinc (Zn), and other metals. Investigations by the U.S. Geological Survey (USGS) at the site have been ongoing since 1984 and are a collaborative effort among USGS scientists and investigators at several universities.

The purpose of this paper is to give an overview of recent and ongoing ground-water investigations at the site with a focus on the results of inverse modeling and reactive-transport geochemical modeling that were used to help understand the important processes that control the movement and distribution of contaminants in ground water. Information gained from these investigations should provide insight into processes that occur at other sites similarly contaminated.

The regional aquifer includes two distinct lithologic units. The older of the two is semiconsolidated to consolidated basin fill that is Tertiary in age. The unit has a maximum thickness of more than 1,000 meters (m) and consists of conglomerates, sand, silt, and fine-grained lakebed sediments. Incised into the basin fill in the major drainages is an unconsolidated alluvium that is less



Figure 1. Pinal Creek Basin, Arizona

than 50 m thick and contains more than 90 percent sand and gravel. Detailed discussions of the geology and hydrogeology of the basin have been published in Peterson (1962), Brown and Eychaner (1996), and Neaville and Brown (1994).

METHODS

From 1984 to 1996, 37 monitor wells and 6 test holes were drilled into the alluvium and shallow basin fill at 12 locations in or near contaminated areas. Aquifer materials collected at the time of drilling were analyzed by particle-size analysis, macroscopic- and microscopic-mineralogical identification (Eychaner and others, 1989), x-ray diffraction (Lind and Stollenwerk, 1996), sequential extractions (Ficklin and others, 1991a, b), column and batch experiments (Stollenwerk, 1994, 1996), and other methods. Water samples were collected from most monitor wells one or two times a year and analyzed for major ions and trace elements to characterize the distribution and movement of contaminants. Less frequently, ground water from selected wells was analyzed for stable isotopes, tritium, chlorofluorocarbons, and dissolved gases. Ongoing investigations include the examination of changes in aquifer materials that have been exposed to contaminated water in wells for periods ranging from 6 to18 months. The purpose of these investigations is to examine changes in mineralogy and the rates of selected geochemical reactions in acidic and neutralized ground water.

Several computer geochemical models have been used in the analysis of contaminant movement at the site. Stollenwerk (1994) used PHRE-EOE (Parkhurst and others, 1980) and MINTOA2 (Allison and others, 1980) to analyze the important reactions that controlled the evolution of the plume through the mid-1980's using laboratory batch and column experiments, and geochemical modeling. Glynn and Brown (1996) used NETPATH (Plummer and others, 1991) and PHREEOC (Parkhurst, 1995) to refine Stollenwerk's findings and examine the possible effects of reactions not considered by Stollenwerk. Brown and others (1998) used PHRE-EQC's transport capabilities to help examine the changes observed in the ground-water plume from 1984-94. This paper provides an overview of the analysis of Glynn and Brown (1996), extends the model of Brown and others (1998) through 1998, and summarizes the major findings.

DISTRIBUTION OF HYDROCHEMICAL ZONES IN THE AQUIFER

The ground-water plume in the Pinal Creek Basin can be separated into three major zones (fig. 2) on the basis of aqueous and solid-phase geochemistry. An acidic zone in which the pH of the ground water was between 4 and 5 in 1998 extends from Miami Wash to well 561.

The acidic zone contains large concentrations of dissolved metals and other contaminants. In 1984, concentrations of dissolved Fe, Mn, and aluminum (Al) at well 51 were 57, 1.3, and 11.1 mmol/L, respectively (table 1). Metals, such as Cu, Co, Ni, and Zn, occurred in the acidic zone at concentrations that ranged from 0.02 to more than 2 mmol/L.

Downgradient from the acidic zone is a transition zone characterized by steep pH and redox gradients and the precipitation and adsorption of metals. In 1984, this zone was about 1.5 km south of the future location of well 451. In this zone, calcite (CaCO₃) and, to a lesser extent, dolomite (CaMg(CO₃)₂), react with and partially neutralize acidic ground water according to the reactions:

and

$$CaCO_3 + H^+ = Ca^{2+} + HCO_3^-,$$

$$CaMg(CO_3)_2 + 2H^+ = Ca^{2+} + Mg^{2+} + 2HCO_3^-.$$

Oxidation and reduction reactions are important as well. The reductive dissolution of Mn oxide is coupled to the oxidation and precipitation of Fe hydroxide (Stollenwerk, 1994). The overall reaction can be written as:

$$MnO_{2(s)} + 2Fe^{2+} + 4H_2O \longrightarrow 2Fe(OH)_{3(a)} + 2H^+ + Mn^{2+}.$$

Although this last reaction produces protons, the net result of reactions in the transition zone was to raise the pH from about 5 to about 6. Metals, such as Cu, Co, Ni, and Zn, are adsorbed to Fe hydroxide and possibly other surfaces in the transition zone because of the increase in pH (Stollenwerk, 1994).

Advective flow moves through the alluvium at an average velocity of 5 meters per day (m/d), which is about 7 times the rate of movement of the acidic front (Eychaner, 1991). As a result, contaminants that remain in solution as the pH increases move beyond the transition zone into the neutralized zone (fig. 2), and eventually surface in the perennial reach of Pinal Creek. Neutralized water generally contains large concentrations of calcium (Ca), Mn, and SO₄; other contaminants, including Fe, Cu, Co, Ni, and Zn, occur at concentrations less than 1 mmol/L (table 1).

Mineral species and other solid phases in the regional aquifer were characterized by the examination and analysis of drill cores and cuttings. Calcite and Mn oxide are present in uncontaminated alluvium, the basin fill, and the neutralized zone of the plume. Sequential extractions of aquifer material and the measured water chemistry indicate that in the acidic zone of the plume most if not all the Mn oxide and carbonate minerals have been dissolved by reaction with the acidic ground-water plume. Minerals present throughout the aquifer include Fe hydroxide and the silicate minerals orthoclase and plagioclase feldspar, muscovite, biotite, and tremolite. The degree to which each reacts with contaminated ground water varies.



Figure 2. Generalized longitudinal section indicating hydrochemical zones in aquifer.

[Values are in millimoles per liter (mmol/L) except for pH. At most locations, earliest available analysis is shown. Dashes indicate no data; km, kilometer; m, meter; <, less than; PCID, Pinal Creek at Inspiration Dam; Depth, depth of well below land surface]

Well number	flow path (km)	Date of sample	Well depth (m)	Hď	Dis- solved oxygen (DO as O)	Calcium (Ca)	Magne- sium (Mg)	Sodium (Na)	Potassium (K)	Alkalinity	Total inorganic carbon (TIC)	Sulfate (SO ₄)
51	0	11 - 84	33.4	3.6	<0.02	12	16	10	0.24	1	1	100
101	Γ.	11 - 84	36.1	3.6	<.02	12	12	8.3	.25		-	74
202 ¹	ł	03-85	12.3	7.2	.46	1.2	.37	96.	.036	2.3	1	Ľ.
302	2.1	11 - 84	35.8	3.5		17	12	7.0	.21		ł	72
402	5.8	11 - 84	20.9	4.2	<.02	13	5.8	3.5	.19		1	27
451	10.1	03 - 89	24.4	4.9	<.006	15	5.5	3.6	.28		4.7	25
503	11.4	07 - 86	25.3	6.2	.01	15	5.8	3.4	.11	2.0	1	21
542	11.4	05 - 97	19.8	4.3	.01	T.T	3.3	2.4	.16		1.3	14
561	11.8	05 - 97	15.3	5.0	.01	7.6	3.1	2.5	.17		1.7	13
601	14.2	11 - 92	8.6	6.4	.04	13	4.5	3.3	.11	2.9	-	18
702	16.3	05 - 90	7.3	7.0	.006	14	5.1	3.0	.16	3.5	1	18
PCID ¹	ł	01 - 93	1	T.T	.64	1.4	.31	.33	.087	.93	1	1.5
Well number	Distance along flow path (km)	Chloride (CI)	Fluoride (F)	Silica (Si)	lron (Fe)	Manga- nese (Mn)	Aluminum (Al)	Copper (Cu)	Cobalt (Co)	Nickel (Ni)	Strontium (Sr)	Zinc (Zn)
51	0	11	1	1.7	57	1.3	11.1	2.4	0.18	0.065	0.017	0.29
101	Γ.	10	1	1.6	39	1.0	8.54	1.7		.054	.018	.18
202 ¹	-	.48	-	.36	.00072	<.0006	<.003	.00016	<.00034	<.0085	.0023	<.00023
302	2.1	8.7	1	1.8	32	1.1	6.69	1.5		.051	.034	.14
402	5.8	4.0	-	1.4	6.3	.91	.409	.30		.019	.020	.046
451	10.1	5.1	.53	1.1	2.5	1.9	1.53	.18		.020	.018	.53
503	11.4	3.7	.021	1.0	.0032	.82	.000	.0005		.007	.240	.0029
542	11.4	1.3	.19	1.1	1.1	.81	.213	.075		.005	.013	.037
561	11.8	1.3	.25	1.1	.00016	1.0	.13	.076		.012	.013	.039
601	14.2	2.4	.01	.72	.00072	.031	<.0004	<.0005		<.0005	.024	.00038
702	16.3	2.3	.013	.46	.019	.052	.186	<.002		<.008	.027	.00026
PCID ¹		11.	.02	1	.000	86000.	-	.00047				<.00005

INVERSE GEOCHEMICAL MODELING

Inverse geochemical modeling has been used at Pinal Creek to help identify and understand the important chemical reactions and physical processes that controlled the evolution of the contaminant plume. Glynn and Brown (1996) used the geochemical codes NETPATH and PHREEQC to examine some plausible reaction models that might have been responsible for the changes in ground-water chemistry that have been measured across the transition zone.

Inverse modeling uses a mass-balance approach to determine the reactions responsible for observed changes in water chemistry between two wells along a flow path. Inverse modeling requires that the system be in a chemically steady-state condition if the wells are sampled at the same time. Because contaminated ground water at the study site was not at steady state, Glynn and Brown (1998) considered the chemical changes between wells that occurred over a period of time equal to the estimated ground-water travel time between the two wells. The inverse-modeling approach also assumes that all potentially important reactions were considered and that the important existing and potential solid phases in the aquifer were known. The assumption of a steady-state flow field also is required. The computer codes do not require that the postulated reactions be thermodynamically feasible, although the thermodynamics of any postulated reaction should be considered when evaluating potential models.

Required input for inverse modeling includes chemical analyses for the selected wells, the chemical composition of solid phases (minerals or amorphous solids) and dissolved gases in the aquifer, and some knowledge about which minerals and gases have the potential to react with the ground water. NETPATH and PHREEQC allow for the initial water to be mixed with one or more waters along the flow path to produce the final water.

Glynn and Brown (1996) examined dozens of models using different combinations of plausible and not so plausible solid- and gas-phase reactants and different assumptions concerning the degree to which the flow path was in contact with gases in the unsaturated zone. Space limitations here preclude a detailed discussion of particular models. Instead, this paper focuses on the common characteristics shared by the more plausible models and will summarize major conclusions.

The analysis of Glynn and Brown (1996) considered a flow path across the transition zone from well 402 (sampled on January 12, 1989) to well 503 (sampled on November 22, 1991). Mixing with uncontaminated water along the flow path was represented by water from well 504 (sampled on November 22, 1991), which is perforated in uncontaminated basin fill. The chemical composition of water from these wells during 1989–91 was similar to that during 1984–89 (table 1); although contaminant concentrations generally decreased from 1984–89. Three minerals were required to be included in all models: calcite, geothite (FeOOH), and gypsum (CaSO₄).

For most models, the system was considered closed to atmospheric oxygen because the flow path across the transition zone was more than 7 m below the water table during 1989–91. Dissolved-oxygen concentrations of water from shallow wells at both sites indicated that essentially all the oxygen moving downward from the unsaturated zone into the plume was consumed near the water table. Although the well openings were not in contact with the unsaturated zone, the degassing of carbon dioxide (CO₂) was allowed in some models because CO₂ had the potential of leaving the flow path through diffusion or mixing processes.

The NETPATH models considered to be most plausible shared several characteristics—the dissolution of calcite and dolomite (CaMg(CO₃)₂), and the precipitation of rhodochrosite (MnCO₃) and gypsum. The results of the PHREEQC simulations were similar, except that accounting for analytical uncertainty (a feature unavailable in NETPATH) resulted in some significantly different results. When a 5-percent relative uncertainty was assumed for SO₄, the precipitation of gypsum was not necessary. This was because SO₄ occurred at concentrations more than 5 times that of Ca, and the uncertainties in the SO₄ concentrations were large in relation to the measured mass transfer of Ca between wells 402 and 503.

A significant conclusion from the NETPATH and PHREEQC inverse modeling was that in order to satisfy the mass-balance constraints on Ca and Mg, the dissolution of Ca-Mg silicates was required. The measured increase in dissolved strontium (Sr) along the flow path was additional evidence of silicate dissolution along the flow path (Glynn, 1991). Solid-phase mass transfers of rhodochrosite and Al were significant particularly in models that allowed no CO_2 exsolution.

GROUND-WATER REACTIVE TRANSPORT, 1984–98

From 1984 to 1998, the concentrations of most contaminants in the acidic zone decreased primarily because of the drainage of an unlined surface-water impoundment that contained acidic mine-process water, other source control measures. remedial pumping that began in the mid-1980's, and recharge of uncontaminated ground water from record high streamflow in 1993. This paper focuses on the most contaminated well at each monitor well group. At each site, this generally was the well perforated closest to the contact with the alluvium and the underlying basin fill. The wells were located along, or reasonably close to, an assumed flow path near the base of the alluvium. Lithologic evidence of a boulder zone near the base of the alluvium was additional evidence that the zone near the base of the alluvium was a preferred pathway for contaminants.

A one-dimensional reactive-transport model was developed using PHREEQC (Parkhurst, 1995) to help characterize the reactions and processes that were responsible for the measured changes in plume geochemistry from 1984 to 1994 (Brown and others, 1998). Equilibrium reactive-transport modeling requires some of the same assumptions as inverse modeling. One such assumption was that the wells in the model were located along a flow path; another was that all important reactions were accounted for. Unlike inverse modeling, equilibrium reactive-transport modeling assumes that water along the flow path reacts to a local equilibrium with selected solid phases in the aquifer. As a result, some of the reactions considered for inverse modeling (silicate dissolution, for example) were not included in the reactive-transport model because these reactions were known to be slow in relation to the travel time of water through contaminated alluvium.

PHREEQC uses a mixing-cell approach (Appelo and Postma, 1993) to simulate contaminant transport. In this approach, a series of mixing cells is set up in which geochemical reactions are calculated. In this simulation, these reactions involve water, minerals, and surfaces to which selected constituents may adsorb or desorb. Before each transport step, the aqueous and solid-phase equilibrium condition is calculated. Water is then shifted to the next adjacent cell where equilibrium is then re-established through the precipitation or dissolution (if the solid phase is present) of the required solid phases. For this analysis, dispersion was simulated using the mixing option. A dispersivity of 30 m was used for this analysis on the basis of a review of field estimates of dispersivities made by Gelhar and others (1992). Glynn and Brown (1996) found that varying the dispersivity from 0 to 10 percent of the length of the flow path had little effect on movement of the acidic front except where the initial calcite concentration was <0.03 mol/kg H₂O. This concentration was less than half the initial calcite concentration used in the neutralized zone of the present model.

For this report, the reactive-transport model of Brown and others (1998) was extended to June 1998. Water from well 51, the monitor well closest to upgradient contaminant sources, was used as inflow to the model. The flow path from well 51 to well 702 (fig. 1) was divided into 82 cells, which were each 200 m long. The earliest available water-chemistry analysis for each well (table 1) along the flow path was used to define the initial conditions for the model. Simulated input for missing constituents were estimated from the earliest available analysis. For example, total inorganic carbon (TIC) was first measured in 1987 and was used to represent 1984 conditions in the model. Between wells, initial water chemistry in each cell consisted of water from a nearby well, or a mixture of water from the nearest upgradient and downgradient wells, as appropriate. The minerals included in the model (table 2) in each cell were determined on the basis of solid-phase analyses. Gypsum and Fe hydroxide were assumed to be initially present along the entire flow path. Adsorption along the flow path was assumed to occur on the Fe hydroxide that is present throughout the aquifer (Stollenwerk, 1994). Calcite was assumed to be initially present in the neutralized zone and absent in the acidic zone where calcite would have been substantially depleted or completely consumed by acidic ground water. Sequential extractions by Ficklin and others (1991a, b) indicated that extractable Mn was present at much lower concentrations

Mineral	Reaction	LogKsp
Calcite	$CaCO_{3(c)} = Ca^{2+} + CO_3^{2-}$	-8.48
Gypsum	$CaSO_{4(c)} * 2H_2O = Ca^{2+} + SO_4^{2-} + 2H_2O$	-4.58
Iron hydroxide	$Fe(OH)_{3(a)} + 3H^+ = Fe^{3+} + 3H_2O$	4.89
Manganese oxide	$MnO_{2(c)} + 4H^+ + e^- = Mn^{2+} + 2H_2O$	41.38
Aluminum-mineral equilibria: Al(OH) _{3(a)}	$AI(OH)_{3(a)} + 3H^+ = AI^{3+} + 3H_2O$	10.8
AlOHSO ₄	$AlOHSO_{4(s)} + H^+ = Al^{3+} + SO_4^{2-} + H_2O$	-3.23
Rhodochrosite	$MnCO_{3(c)} = Mn^{2+} + CO_3^{2-}$	-11.13

 Table 2. Mineral reactions and solubility-product constants used in simulation of reactive transport
 [logKsp, log of the solubility- product constant]

in the acidic zone than in the neutralized zone. Because of this, most if not all of the reactive Mn oxide in aquifer material was assumed to be reductively dissolved with the passage of the transition zone, and the simulated concentration of Mn oxide in the acidic zone was set to 0 in the model. Under these conditions, simulated Fe behaved as a conservative constituent in the acidic zone and reacted with Mn only in cells where Mn oxide was present.

Conservative Transport

Chloride (Cl) is a conservative constituent at Pinal Creek (Stollenwerk, 1994) and was used to measure the degree to which contaminated water was diluted by uncontaminated water along the flow path. Uncontaminated ground water from the underlying basin fill and tributary alluvium was represented in the model by water from well 202, which is in Pinal Creek alluvium about 1 km upstream from the mouth of Miami Wash. Dilution from flood-related recharge was represented in the model by a sample of water from Pinal Creek at Inspiration Dam obtained during a flood in January 1993. Both sources of uncontaminated inflow were mixed with contaminated ground water in each cell in amounts necessary to match measured Cl concentrations in wells along the flow path.

In 1984, the Cl concentration of water decreased from 11.0 mmol/L at km 0 to 3.95 mmol/L at km 5.8 (fig. 3). From km 5.8 to the end of the flow path (km 16.3), Cl decreased only slightly to 2.34 mmol/L in 1990. Because of contaminantsource removal, remedial pumping, and significant ground-water recharge in the early 1990's, Cl concentrations decreased along the entire flow path from 1984 to 1998. By 1998, the trend observed in 1984 had disappeared, and Cl concentrations were about equal along the flow path. Distribution of Cl simulated with PHREEQC matched measured concentrations reasonably well using mixing fractions that ranged from 0.06 at the upstream end of the model to 0.01 at the downstream end. (Water resulting from a mixing fraction of 0.06 consisted of 94-percent contaminated water and 6-percent uncontaminated water.) For 1993, the fraction of water mixed with contaminated water in each cell was increased slightly from km 3 to 11.4 to account for recharge of uncontaminated water from the 1993 flood.

Acidity and Related Equilibria

Unlike Cl, pH and other species, including Al, Ca, inorganic carbon, SO₄, Mn, and Fe, were affected by chemical reactions with solids in the aquifer or gases in the unsaturated zone. The pH along the flow path defined the acidic, transition, and neutralized zones in the aquifer. In 1984, the pH in the acidic zone was about 3.8, and by 1998, the pH had risen slightly to about 4 (fig. 4). Stollenwerk (1994) attributed the persistence of low pH in the aquifer to the gradual desorption of protons from Fe hydroxide surfaces in the aquifer. Several reactions acting in combination controlled the pH in the plume. The dissolution of calcite and mixing of contaminated ground water with uncontaminated ground water increased the pH. The



Figure 3. Measured and simulated concentrations of chloride along the flow path in the aquifer, 1984, 1991, and 1998, and locations of wells.

reductive dissolution of Mn oxide and the consequent oxidation and precipitation of Fe hydroxide decreased the pH, as did the gradual desorption of protons from Fe hydroxide surfaces.

Concentrations of Ca in the aquifer were controlled by equilibrium with calcite and gypsum, and by mixing of contaminated ground water with uncontaminated ground water. Calculations using PHREEQC indicated that water in the acidic part of the flow path was slightly supersaturated or in equilibrium with gypsum from 1984 until 1991 and was increasingly undersaturated from 1992 to 1998 (fig. 5). Gypsum equilibria can be expressed by the following reaction:

 $Ca^{2+} + SO_4^{2-} + 2H_2O = CaSO_{4\bullet}2H_2O.$

Although this reaction does not directly affect the pH, the increase in dissolved Ca that results from the redissolution of precipitated gypsum increases the calcite saturation index and indirectly plays a role in acidity equilibria.

Concentrations of Ca in water at km 0 decreased slightly from 12 mmol/L in 1984 to 11 mmol/L in 1992 and then decreased abruptly to 3.9 mmol/L in 1994 after the aquifer received recharge from flooding in 1993. Ca increased to 7.8 mmol/L by 1998 (fig. 6). During the same period, Cl decreased by a factor of 3.6, which indicates that dissolution of gypsum was responsible for the small decreases in measured Ca concentrations relative to Cl concentrations.

As previously mentioned, carbonate mineral dissolution in the transition zone increased the pH



Figure 4. Measured and simulated ph along the flow path in the aquifer, 1984, 1991, and 1998.

from about 4 to greater than 6. Calcite saturation indices were between -0.2 and -1.0 at km 14.2 in the neutralized zone (fig. 7), which indicated that calcite dissolution in the transition zone was not sufficient to bring partially neutralized water into equilibrium with calcite. Ground water was undersaturated with calcite at km 14.2, and equilibrium with calcite was established by km 16.3. The saturation indices indicate that calcite dissolution in the neutralized zone was responsible for the measured increase in Ca along the flow path from km 10 to km 16 through 1998.

From 1984 to 1998, simulated concentrations of Ca generally were larger than measured concentrations (fig. 6). The measured decreases in Ca from 1991 to 1998 were not reflected in the model, probably because simulated gypsum dissolution was greater than that in the aquifer. Beginning in 1991 (figs. 5 and 6), acidic water became undersaturated with respect to gypsum; however, the model maintained equilibrium through dissolu-



Figure 5. Saturation indices for gypsum in water from wells in the acidic part of the flow path, 1984–1998.

tion with gypsum. The simulated concentration of gypsum initially in the acidic part of the aquifer estimated from sequential extractions done by Ficklin (1991a, b) probably was unreasonably large.

Iron, Manganese, and Oxidation-Reduction Reactions

As previously mentioned, concentrations of Fe and Mn were controlled in part by oxidationreduction reactions in the transition zone and mixing of contaminated ground water with uncontaminated ground water along the flow path. Mn also may sorb to Fe hydroxide surfaces under certain conditions. In 1984, concentrations of dissolved Fe decreased from 57 mmol/L at km 0 to less than 10 mmol/L at km 5.8 (fig. 8), which is a factor of about 6. Over the same interval, Cl decreased by a factor of 3 (fig. 3) and Mn decreased by less than half, from 1.3 mmol/L to 0.9 mmol/L (fig. 9). These differences suggest that oxidation-reduction reactions in part controlled the concentrations of Fe and Mn more than 2 km upgradient from the transition zone. In addition, the simulated and measured concentrations of dissolved Fe and Mn at km 6 differed significantly in the late 1980's. In 1987 at km 5.8, the simulated concentration of Fe was greater than the measured concentration, and the simulated concentration of Mn was less than the measured concentration. Because the initial modeled concentration of Mn oxide was 0 in the acidic zone, simulated Fe moved conservatively through the acidic zone to the transition zone where reaction with Mn oxides occurred. The differences between measured and simulated concentrations of Mn and Fe at km 5.8 provided additional evidence for the continued reductive dissolution of Mn oxides and oxidation and precipitation of Fe in the acidic zone.

In the transition zone, simulated Mn concentrations were unreasonably large (fig. 9) probably because the reductive dissolution of Mn is kinetically controlled. The simulated attainment of equilibrium with each transport step caused excessive Mn dissolution in the transition zone. Although Stollenwerk (1994) observed a peak of similar magnitude in a column experiment using acidic ground water and alluvium from the site, such a peak has not been observed in the field. The slight decrease in concentrations of dissolved Mn



Figure 6. Measured and simulated concentrations of dissolved calcium along the flow path in the aquifer, 1984, 1991, and 1998.



Figure 7. Saturation indices for calcite in the transition and neutralized zones of the plume, 1984–98.

between km 12.1 and km 16.2 was attributed to rhodochrosite precipitation on the basis of measured saturation indices near 0 at km 16.2 (Brown and others, 1998).

Aluminum Equilibria

Inverse modeling indicated that the measured attenuation of Al across the transition zone was in part controlled by mineral reactions. The determination of the solubility controls on dissolved Al over the range in pH measured in the plume, however, remains problematic. Stollenwerk (1994) used amorphous aluminum hydroxide (Al(OH)_{3(a)}; table 2) as the solubility control above a pH of 4.5, and a mineral with the formula



Figure 8. Measured and simulated concentrations of dissolved iron along the flow path in the aquifer, 1984, 1987, and 1998.

AlOHSO₄ below a pH of 4.5, but changed the equilibrium constant by more than an order of magnitude to obtain a reasonable fit between his simulation and measured concentrations of dissolved Al.

Because the precipitation of each mineral releases protons to solution, Al mineral reactions could have a significant effect on pH in the plume. Because of the uncertainties related to the control on dissolved Al concentrations below a pH of 4.5, however, no controls were placed on Al solubility in the present simulation.

SENSITIVITY ANALYSES

As is the case with many field studies, the physical and chemical characteristics of the ground-water flow system in the Pinal Creek Basin were determined on the basis of sparse or incomplete data. Similarly, the reactions that control the movement and transformation of the plume have not been determined with absolute certainty. Sensitivity analyses are useful, therefore, to examine the effects of uncertainty on reactive transport in the plume. Uncertainties considered below are the calcite content, the nature of reactions with gases in the unsaturated zone, and Al-mineral equilibria. Not discussed here because of space limitations are the uncertainties in initial solid-phase concentrations, other than calcite, and slow reactions that may nonetheless be significant.



Figure 9. Measured and simulated concentrations of dissolved manganese along the flow path in the aquifer, 1984, 1991, and 1998.

Calcite Content

The calcite content of 0.075 mol/kg H₂O used to simulate transport from 1984 to 1998 was estimated on the basis of a mass balance of Ca done on Stollenwerk's (1994) column experiment. At this concentration, the movement of the simulated pH front had a retardation factor of 7. A calcite concentration of 0.038 mmol/kg H₂O was used as the lower limit in this sensitivity analysis. Other measurements have yielded larger concentrations. Stollenwerk (1994) measured 0.17 mol/kg H₂O of calcite in the uncontaminated alluvium used in his experiment. Buffer-capacity measurements done by Hydro Geo Chem, Inc. (1989) yielded carbonate content estimates that ranged from 0.125 mol/kg H₂O in sand and gravel to 0.76 mol/kg H₂O in calcareous clay. Adjusting these values for the average particle size of sediments at monitor well group 500 yielded a value of 0.29 mol/kg H₂O, which was used as the upper limit in this sensitivity analysis.

Increasing the calcite content in the neutralized zone from 0.075 to 0.29 mol/kg H_2O reduced the rate of movement of the acidic front from by a factor of 9 (fig. 10). Decreasing the calcite content to 0.038 mol/kg H_2O increased the rate of movement by a factor of 1.7 and created a zone from km 11 to km 12 where Mn oxide dissolution occurred in the absence of calcite dissolution. Such a zone (and pH's associated with those conditions) has not been observed in the field. Glynn and Brown (1996) noted a similar zone when the initial carbonate-mineral to Mn oxide ratio was greater than 3:2.

Carbon Dioxide Exchange

The simulation of the plume at Pinal Creek was made with the assumption that the plume was closed to the in-gassing of oxygen from the unsaturated zone and the out-gassing of CO₂ to the unsaturated zone. Field values of dissolved oxygen suggest that the system is closed, but the extent to which CO₂ does or does not decrease along the flow path through mixing or diffusion cannot be known with complete certainty. Opening the system to CO₂ at a constant pCO₂ of $10^{-1.33}$ atmospheres (calculated from measured concentrations of total inorganic carbon, TIC) decreased by less than 0.25 km the distance traveled by the pH front from 1984 to 1998. For both simulations, the 1993 decrease in simulated TIC marked the point at which carbonate dissolution was complete upgradient from km 11.4). The simulations indicate that when carbonate dissolution is ongoing, keeping the system closed allowed for unreasonable buildup of TIC in the neutralized zone (fig. 11). After all the simulated calcite had dissolved, the closed system simulated that the TIC concentrations were in good agreement. These results indicate that the water along the flow path was in partial or indirect contact with the atmosphere possibly through mixing with shallower water that is in direct contact with the unsaturated zone. More realistic simulation of this (and other gas-exchange processes) will require the use of a two-dimensional model.



Figure 10. Simulated pH for selected concentrations of calcite in aquifer material, 1984 and 1998.

Aluminum Equilibria

Because of the uncertainty regarding the solid-phase controls on Al solubility, no controls were placed on dissolved Al in the model. The effects of Al solid phases on the movement of the pH front were explored by a sensitivity analysis that allowed for the control of dissolved Al concentrations by Al(OH)_{3(a)} and AlOHSO₄. Initial concentrations of these minerals were set to 0. By allowing for the precipitation and redissolution of these minerals, the simulated pH from km 0 to km 10 was as much as one unit less in 1998. Between km 9 and km 10, the pH decreased by as much as one unit. These changes had little effect on the rate of movement of the simulated acidic front of the plume. Glynn and Brown (1996) simulated flow between wells 402 and 503 and found that allowing AlOHSO₄ to precipitate rather than $Al(OH)_{3(a)}$ increased the retardation factors of the rhodochrosite and Al solid-phase dissolution fronts, which are associated with the breakthrough of the low pH front.

CONCLUSIONS

From 1984 to 1998, concentrations of contaminants in the alluvial aquifer in Pinal Creek Basin, Arizona, decreased as a result of mixing, recharge, source removal, remedial pumping, and chemical reactions. Inverse and reactive-transport geochemical modeling were used to help understand the important reactions and processes that controlled the measured changes in chemistry. The major conclusions of this analysis are as follows.



Figure 11. Measured and simulated concentrations of total inorganic carbon in water at km 11.4, 1984–98.

NETPATH and PHREEQC inverse modeling indicated that in order to satisfy the mass-balance constraints on Ca and Mg, the dissolution of Ca-Mg silicates were required. Rhodochrosite and Al solid-phase mass transfers were significant, particularly in models that allowed no CO_2 exsolution.

Simulated and measured concentrations of Fe, Mn, and Ca differed mainly because water along the flow path appeared not to be in a state of local equilibrium. The lack of equilibrium is related at least in part to slow reaction kinetics, but an apparent lack of equilibrium also could result from diffusion processes that limit the interaction of solid-phase surfaces with solutes in the aquifer. Distinguishing reaction kinetics from diffusion limitations in the subsurface is difficult if not impossible at the present time.

Because of the apparent lack of equilibrium, the primary usefulness of the model was as a means of comparing the system at Pinal Creek with a system in local equilibrium. Although the equilibrium approach provided insight as to which processes at the site were kinetically controlled and which were not, future work will require a kinetic modeling approach to more thoroughly characterize selected reactions between the plume and aquifer materials and will require the use of a two- or three-dimensional reactive-transport model.

From 1984 to 1990, water along the flow path was supersaturated or in equilibrium with gypsum, and gypsum equilibria controlled dissolved concentrations of Ca and SO_4 . Beginning in 1991, water in the acidic part of the plume became increasingly undersaturated with gypsum indicating that the gypsum available for dissolution in the aquifer became limited beginning in about 1991.

Rhodochrosite precipitation probably was responsible for the measured attenuation in dissolved Mn in the neutralized zone. For reactions involving gypsum and rhodochrosite, the assumption of a local geochemical equilibrium generally was valid.

For oxidation-reduction reactions, the local equilibrium assumption generally was not valid. Reaction kinetics appear to control the measured concentrations of dissolved Fe and Mn in the acidic and transition zones.

For reactions involving calcite, the local equilibrium assumption did not appear valid. Although dissolution of calcite in the transition zone was not sufficient to establish equilibrium, calcite undersaturation decreased along the flow path in the neutralized zone, and equilibrium was reached by the end of the flow path.

Sensitivity analysis indicated that the rate of advance of the pH front was highly sensitive to the initial calcite concentration. Increasing the calcite content from 0.075 to 0.29 mol/kg H₂O reduced the calculated rate of advance of the pH front by a factor of 9. Decreasing the calcite content to 0.038 mol/kg H₂O increased the rate of the pH front advance by a factor of 1.7.

Opening the system to CO_2 at a constant pCO_2 of $10^{-1.33}$ atmospheres produced a better agreement between measured and simulated concentrations of dissolved TIC when calcite dissolution was occurring. After simulated calcite was completely consumed, better agreement between measured and simulated concentrations of dissolved TIC was achieved when the exsolution of CO₂ was not allowed. The simulations indicate that when calcite dissolution is ongoing, keeping the system closed allowed for unreasonable buildup of dissolved carbon in the neutralized zone. After all the simulated calcite had dissolved, the simulated carbon concentrations in the closed system were in good agreement. Water along the flow path was in partial or indirect contact with the atmosphere possibly through mixing with shallower water that is in direct contact with the unsaturated zone. More realistic simulation of this (and other gas-exchange processes) will require the use of a twodimensional model.

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Exhibit F

Heavy Metals Toxicity and the Environment

Paul B Tchounwou, Clement G Yedjou, [...], and Dwayne J Sutton

Abstract

Heavy metals are naturally occurring elements that have a high atomic weight and a density at least 5 times greater than that of water. Their multiple industrial, domestic, agricultural, medical and technological applications have led to their wide distribution in the environment; raising concerns over their potential effects on human health and the environment. Their toxicity depends on several factors including the dose, route of exposure, and chemical species, as well as the age, gender, genetics, and nutritional status of exposed individuals. Because of their high degree of toxicity, arsenic, cadmium, chromium, lead, and mercury rank among the priority metals that are of public health significance. These metallic elements are considered systemic toxicants that are known to induce multiple organ damage, even at lower levels of exposure. They are also classified as human carcinogens (known or probable) according to the U.S. Environmental Protection Agency, and the International Agency for Research on Cancer. This review provides an analysis of their environmental occurrence, production and use, potential for human exposure, and molecular mechanisms of toxicity, genotoxicity, and carcinogenicity.

Keywords: Heavy metals, production and use, human exposure, toxicity, genotoxicity, carcinogenicity

Introduction

Heavy metals are defined as metallic elements that have a relatively high density compared to water [1]. With the assumption that heaviness and toxicity are inter-related, heavy metals also include metalloids, such as arsenic, that are able to induce toxicity at low level of exposure [2]. In recent years, there has been an increasing ecological and global public health concern associated with environmental contamination by these metals. Also, human exposure has risen dramatically as a result of an exponential increase of their use in several industrial, agricultural, domestic and technological applications [3]. Reported sources of heavy metals in the environment include geogenic, industrial, agricultural, pharmaceutical, domestic effluents, and atmospheric sources [4]. Environmental pollution is very prominent in point source areas such as mining, foundries and smelters, and other metal-based industrial operations [1, 3, 4].

Although heavy metals are naturally occurring elements that are found throughout the earth's crust, most environmental contamination and human exposure result from anthropogenic activities such as mining and smelting operations, industrial production and use, and domestic and agricultural use of metals and metal-containing compounds [4–7]. Environmental contamination can also occur through metal corrosion, atmospheric deposition, soil erosion of metal ions and leaching of heavy metals, sediment re-suspension and metal evaporation from water resources to soil and ground water [8]. Natural phenomena such as weathering and volcanic eruptions have also been reported to significantly contribute to heavy metal pollution [1, 3, 4, 7, 8]. Industrial sources include metal processing in refineries, coal burning in power plants, petroleum combustion, nuclear power stations and high tension lines, plastics, textiles, microelectronics, wood preservation and paper processing plants [9–11].

It has been reported that metals such as cobalt (Co), copper (Cu), chromium (Cr), iron (Fe), magnesium (Mg), manganese (Mn), molybdenum (Mo), nickel (Ni), selenium (Se) and zinc (Zn) are essential nutrients that are required for various biochemical and physiological functions [12]. Inadequate supply of these micro-nutrients results in a variety of deficiency diseases or syndromes [12].

Heavy metals are also considered as trace elements because of their presence in trace concentrations (ppb range to less than 10ppm) in various environmental matrices [13]. Their bioavailability is influenced by physical factors such as temperature, phase

association, adsorption and sequestration. It is also affected by chemical factors that influence speciation at thermodynamic equilibrium, complexation kinetics, lipid solubility and octanol/water partition coefficients [14]. Biological factors such as species characteristics, trophic interactions, and biochemical/physiological adaptation, also play an important role [15].

The essential heavy metals exert biochemical and physiological functions in plants and animals. They are important constituents of several key enzymes and play important roles in various oxidation-reduction reactions [12]. Copper for example serves as an essential co-factor for several oxidative stress-related enzymes including catalase, superoxide dismutase, peroxidase, cytochrome c oxidases, ferroxidases, monoamine oxidase, and dopamine β -monooxygenase [16–18]. Hence, it is an essential nutrient that is incorporated into a number of metalloenzymes involved in hemoglobin formation, carbohydrate metabolism, catecholamine biosynthesis, and cross-linking of collagen, elastin, and hair keratin. The ability of copper to cycle between an oxidized state, Cu(II), and reduced state, Cu(I), is used by cuproenzymes involved in redox reactions [16–18]. However, it is this property of copper that also makes it potentially toxic because the transitions between Cu(II) and Cu(I) can result in the generation of superoxide and hydroxyl radicals [16-19]. Also, excessive exposure to copper has been linked to cellular damage leading to Wilson disease in humans [18, 19]. Similar to copper, several other essential elements are required for biologic functioning, however, an excess amount of such metals produces cellular and tissue damage leading to a variety of adverse effects and human diseases. For some including chromium and copper, there is a very narrow range of concentrations between beneficial and toxic effects [19, 20]. Other metals such as aluminium (Al), antinomy (Sb), arsenic (As), barium (Ba), beryllium (Be), bismuth (Bi), cadmium (Cd), gallium (Ga), germanium (Ge), gold (Au), indium (In), lead (Pb), lithium (Li), mercury (Hg), nickel (Ni), platinum (Pt), silver (Ag), strontium (Sr), tellurium (Te), thallium (Tl), tin (Sn), titanium (Ti), vanadium (V) and uranium (U) have no established biological functions and are considered as non-essential metals [20].

In biological systems, heavy metals have been reported to affect cellular organelles and components such as cell membrane, mitochondrial, lysosome, endoplasmic reticulum, nuclei, and some enzymes involved in metabolism, detoxification, and damage repair [21]. Metal ions have been found to interact with cell components such as DNA and nuclear proteins, causing DNA damage and conformational changes that may lead to cell cycle modulation, carcinogenesis or apoptosis [20–22]. Several studies from our laboratory have demonstrated that reactive oxygen species (ROS) production and oxidative stress play a key role in the toxicity and carcinogenicity of metals such as arsenic [23, 24, 25], cadmium [26], chromium [27, 28], lead [29, 30], and mercury [31, 32]. Because of their high degree of toxicity, these five elements rank among the priority metals that are of great public health significance. They are all systemic toxicants that are known to induce multiple organ damage, even at lower levels of exposure. According to the United States Environmental Protection Agency (U.S. EPA), and the International Agency for Research on Cancer (IARC), these metals are also classified as either "known" or "probable" human carcinogens based on epidemiological and experimental studies showing an association between exposure and cancer incidence in humans and animals.

Heavy metal-induced toxicity and carcinogenicity involves many mechanistic aspects, some of which are not clearly elucidated or understood. However, each metal is known to have unique features and physic-chemical properties that confer to its specific toxicological mechanisms of action. This review provides an analysis of the environmental occurrence, production and use, potential for human exposure, and molecular mechanisms of toxicity, genotoxicity, and carcinogenicity of arsenic, cadmium, chromium, lead, and mercury.

Arsenic

Environmental Occurrence, Industrial Production and Use

Arsenic is a ubiquitous element that is detected at low concentrations in virtually all environmental matrices [33]. The major inorganic forms of arsenic include the trivalent arsenite and the pentavalent arsenate. The organic forms are the methylated metabolites – monomethylarsonic acid (MMA), dimethylarsinic acid (DMA) and trimethylarsine oxide. Environmental pollution

by arsenic occurs as a result of natural phenomena such as volcanic eruptions and soil erosion, and anthropogenic activities [33]. Several arsenic-containing compounds are produced industrially, and have been used to manufacture products with agricultural applications such as insecticides, herbicides, fungicides, algicides, sheep dips, wood preservatives, and dye-stuffs. They have also been used in veterinary medicine for the eradication of tapeworms in sheep and cattle [34]. Arsenic compounds have also been used in the medical field for at least a century in the treatment of syphilis, yaws, amoebic dysentery, and trypanosomaiasis [34,35]. Arsenic-based drugs are still used in treating certain tropical diseases such as African sleeping sickness and amoebic dysentery, and in veterinary medicine to treat parasitic diseases, including filariasis in dogs and black head in turkeys and chickens [35]. Recently, arsenic trioxide has been approved by the Food and Drug Administration as an anticancer agent in the treatment of acute promeylocytic leukemia [36]. Its therapeutic action has been attributed to the induction of programmed cell death (apoptosis) in leukemia cells [24].

Potential for Human Exposure

It is estimated that several million people are exposed to arsenic chronically throughout the world, especially in countries like Bangladesh, India, Chile, Uruguay, Mexico, Taiwan, where the ground water is contaminated with high concentrations of arsenic. Exposure to arsenic occurs via the oral route (ingestion), inhalation, dermal contact, and the parenteral route to some extent [33,34,37]. Arsenic concentrations in air range from 1 to 3 ng/m³ in remote locations (away from human releases), and from 20 to 100 ng/m³ in cities. Its water concentration is usually less than 10μ g/L, although higher levels can occur near natural mineral deposits or mining sites. Its concentration in various foods ranges from 20 to 140 ng/kg [38]. Natural levels of arsenic in soil usually range from 1 to 40 mg/kg, but pesticide application or waste disposal can produce much higher values [25].

Diet, for most individuals, is the largest source of exposure, with an average intake of about 50 µg per day. Intake from air, water and soil are usually much smaller, but exposure from these media may become significant in areas of arsenic contamination. Workers who produce or use arsenic compounds in such occupations as vineyards, ceramics, glass-making, smelting, refining of metallic ores, pesticide manufacturing and application, wood preservation, semiconductor manufacturing can be exposed to substantially higher levels of arsenic [39]. Arsenic has also been identified at 781 sites of the 1,300 hazardous waste sites that have been proposed by the U.S. EPA for inclusion on the national priority list [33,39]. Human exposure at these sites may occur by a variety of pathways, including inhalation of dusts in air, ingestion of contaminated water or soil, or through the food chain [40].

Contamination with high levels of arsenic is of concern because arsenic can cause a number of human health effects. Several epidemiological studies have reported a strong association between arsenic exposure and increased risks of both carcinogenic and systemic health effects [41]. Interest in the toxicity of arsenic has been heightened by recent reports of large populations in West Bengal, Bangladesh, Thailand, Inner Mongolia, Taiwan, China, Mexico, Argentina, Chile, Finland and Hungary that have been exposed to high concentrations of arsenic in their drinking water and are displaying various clinico-pathological conditions including cardiovascular and peripheral vascular disease, developmental anomalies, neurologic and neurobehavioural disorders, diabetes, hearing loss, portal fibrosis, hematologic disorders (anemia, leukopenia and eosinophilia) and carcinoma [25, 33, 35, 39]. Arsenic exposure affects virtually all organ systems including the cardiovascular, dermatologic, nervous, hepatobilliary, renal, gastro-intestinal, and respiratory systems [41]. Research has also pointed to significantly higher standardized mortality rates for cancers of the bladder, kidney, skin, and liver in many areas of arsenic pollution. The severity of adverse health effects is related to the chemical form of arsenic, and is also time- and dose-dependent [42,43]. Although the evidence of carcinogenicity of arsenic in humans seems strong, the mechanism by which it produces tumors in humans is not completely understood [44].

Mechanisms of Toxicity and Carcinogenicity

Analyzing the toxic effects of arsenic is complicated because the toxicity is highly influenced by its oxidation state and solubility, as well as many other intrinsic and extrinsic factors [45]. Several studies have indicated that the toxicity of arsenic depends on the

exposure dose, frequency and duration, the biological species, age, and gender, as well as on individual susceptibilities, genetic and nutritional factors [46]. Most cases of human toxicity from arsenic have been associated with exposure to inorganic arsenic. Inorganic trivalent arsenite (As^{III}) is 2–10 times more toxic than pentavalent arsenate (As^V) [5]. By binding to thiol or sulfhydryl groups on proteins, As (III) can inactivate over 200 enzymes. This is the likely mechanism responsible for arsenic's widespread effects on different organ systems. As (V) can replace phosphate, which is involved in many biochemical pathways [5, 47].

One of the mechanisms by which arsenic exerts its toxic effect is through impairment of cellular respiration by the inhibition of various mitochondrial enzymes, and the uncoupling of oxidative phosphorylation. Most toxicity of arsenic results from its ability to interact with sulfhydryl groups of proteins and enzymes, and to substitute phosphorous in a variety of biochemical reactions [48]. Arsenic *in vitro* reacts with protein sulfhydryl groups to inactivate enzymes, such as dihydrolipoyl dehydrogenase and thiolase, thereby producing inhibited oxidation of pyruvate and betaoxidation of fatty acids [49]. The major metabolic pathway for inorganic arsenic in humans is methylation. Arsenic trioxide is methylated to two major metabolites via a non-enzymatic process to monomethylarsonic acid (MMA), which is further methylated enzymatically to dimethyl arsenic acid (DMA) before excretion in the urine [40, 47]. It was previously thought that this methylation process is a pathway of arsenic detoxification, however, recent studies have pointed out that some methylated metabolites may be more toxic than arsenite if they contain trivalent forms of arsenic [41].

Tests for genotoxicity have indicated that arsenic compounds inhibit DNA repair, and induce chromosomal aberrations, sisterchromatid exchanges, and micronuclei formation in both human and rodent cells in culture [50–52] and in cells of exposed humans [53]. Reversion assays with *Salmonella typhimurium* fail to detect mutations that are induced by arsenic compounds. Although arsenic compounds are generally perceived as weak mutagens in bacterial and animal cells, they exhibit clastogenic properties in many cell types *in vivo* and *in vitro* [54]. In the absence of animal models, *in vitro* cell transformation studies become a useful means of obtaining information on the carcinogenic mechanisms of arsenic toxicity. Arsenic and arsenical compounds are cytotoxic and induce morphological transformations of Syrian hamster embryo (SHE) cells as well as mouse C3H10T1/2 cells and BALB/3T3 cells [55, 56].

Based on the comet assay, it has been reported that arsenic trioxide induces DNA damage in human lymphophytes [57] and also in mice leukocytes [58]. Arsenic compounds have also been shown to induce gene amplification, arrest cells in mitosis, inhibit DNA repair, and induce expression of the *c-fos* gene and the oxidative stress protein heme oxygenase in mammalian cells [58, 59]. They have been implicated as promoters and comutagens for a variety of toxic agents [60]. Recent studies in our laboratory have demonstrated that arsenic trioxide is cytotoxic and able to transcriptionally induce a significant number of stress genes and related proteins in human liver carcinoma cells [61].

Epidemiological investigations have indicated that long-term arsenic exposure results in promotion of carcinogenesis. Several hypotheses have been proposed to describe the mechanism of arsenic-induced carcinogenesis. Zhao et al. [62] reported that arsenic may act as a carcinogen by inducing DNA hypomethylation, which in turn facilitates aberrant gene expression. Additionally, it was found that arsenic is a potent stimulator of extracellular signal-regulated protein kinase Erk1 and AP-1 transactivational activity, and an efficient inducer of *c-fos* and *c-jun* gene expression [63]. Induction of *c-jun* and *c-fos* by arsenic is associated with activation of JNK [64]. However, the role of JNK activation by arsenite in cell transformation or tumor promotion is unclear.

In another study, Trouba et al. [65] concluded that long-term exposure to high levels of arsenic might make cells more susceptible to mitogenic stimulation and that alterations in mitogenic signaling proteins might contribute to the carcinogenic action of arsenic. Collectively, several recent studies have demonstrated that arsenic can interfere with cell signaling pathways (e.g., the p53 signaling pathway) that are frequently implicated in the promotion and progression of a variety of tumor types in experimental animal models, and of some human tumors [66, 68]. However, the specific alterations in signal transduction pathways or the actual targets that contribute to the development of arsenic-induced tumors in humans following chronic consumption of arsenic remains uncertain.

Recent clinical trials have found that arsenic trioxide has therapeutic value in the treatment of acute promyelocytic leukemia, and there is interest in exploring its effectiveness in the treatment of a variety of other cancers [69,70]. In acute promyelocytic leukemia, the specific molecular event critical to the formation of malignant cells is known. A study by Puccetti et al. [71] found that forced overexpression of BCR-ABL susceptibility in human lymphoblasts cells resulted in greatly enhanced sensitivity to arsenic-induced apoptosis. They also concluded that arsenic trioxide is a tumor specific agent capable of inducing apoptosis selectively in acute promyelocytic leukemia cells. Several recent studies have shown that arsenic can induce apoptosis through alterations in other cell signaling pathways [72,73]. In addition to acute peomyelocytic leukemia, arsenic is thought to have therapeutic potential for myeloma [74]. In summary, numerous cancer chemotherapy studies in cell cultures and in patients with acute promyelocytic leukemia demonstrate that arsenic trioxide administration can lead to cell-cycle arrest and apoptosis in malignant cells.

Previous studies have also examined p53 gene expression and mutation in tumors obtained from subjects with a history of arsenic ingestion. p53 participates in many cellular functions, cell-cycle control, DNA repair, differentiation, genomic plasticity and programmed cell death. Additional support for the hypothesis that arsenic can modulate gene expression has been provided by several different studies [75,76]. Collectively, these studies provide further evidence that various forms of arsenic can alter gene expression and that such changes could contribute substantially to the toxic and carcinogenic actions of arsenic treatment in human populations [77].

Several *in vitro* studies in our laboratory have demonstrated that arsenic modulates DNA synthesis, gene and protein expression, genotoxicity, mitosis and/or apoptotic mechanisms in various cell lines including keratinocytes, melanocytes, dendritic cells, dermal fibroblasts, microvascular endothelial cells, monocytes, and T-cells [78], colon cancer cells [79], lung cancer cells [80], human leukemia cells [81], Jurkat-T lymphocytes [82], and human liver carcinoma cells [83]. We have also shown that oxidative stress plays a key role in arsenic induced cytotoxicity, a process that is modulated by pro- and/or anti-oxidants such as ascorbic acid and n-acetyl cysteine [84–86]. We have further demonstrated that the toxicity of arsenic depends on its chemical form, the inorganic form being more toxic than the organic one [42].

Various hypotheses have been proposed to explain the carcinogenicity of inorganic arsenic. Nevertheless, the molecular mechanisms by which this arsenical induces cancer are still poorly understood. Results of previous studies have indicated that inorganic arsenic does not act through classic genotoxic and mutagenic mechanisms, but rather may be a tumor promoter that modifies signal transduction pathways involved in cell growth and proliferation [68]. Although much progress has been recently made in the area of arsenic's possible mode(s) of carcinogenic action, a scientific consensus has not yet reached. A recent review discusses nine different possible modes of action of arsenic carcinogenesis: induced chromosomal abnormalities, oxidative stress, altered DNA repair, altered DNA methylation patterns, altered growth factors, enhanced cell proliferation, promotion/progression, suppression of p53, and gene amplification [87]. Presently, three modes (chromosomal abnormality, oxidative stress, and altered growth factors) of arsenic carcinogenesis have shown a degree of positive evidence, both in experimental systems (animal and human cells) and in human tissues. The remaining possible modes of carcinogenic action (progression of carcinogenesis, altered DNA repair, p53 suppression, altered DNA methylation patterns and gene amplification) do not have as much evidence, particularly from *in vivo* studies with laboratory animals, *in vitro* studies with cultured human cells, or human data from case or population studies. Thus, the mode-of-action studies suggest that arsenic might be acting as a cocarcinogen, a promoter, or a progressor of carcinogenesis.

Cadmium

Environmental Occurrence, Industrial Production and Use

Cadmium is a heavy metal of considerable environmental and occupational concern. It is widely distributed in the earth's crust at

an average concentration of about 0.1 mg/kg. The highest level of cadmium compounds in the environment is accumulated in sedimentary rocks, and marine phosphates contain about 15 mg cadmium/kg [88].

Cadmium is frequently used in various industrial activities. The major industrial applications of cadmium include the production of alloys, pigments, and batteries [89]. Although the use of cadmium in batteries has shown considerable growth in recent years, its commercial use has declined in developed countries in response to environmental concerns. In the United States for example, the daily cadmium intake is about $0.4\mu g/kg/day$, less than half of the U.S. EPA's oral reference dose [90]. This decline has been linked to the introduction of stringent effluent limits from plating works and, more recently, to the introduction of general restrictions on cadmium consumption in certain countries.

Potential for Human Exposure

The main routes of exposure to cadmium are via inhalation or cigarette smoke, and ingestion of food. Skin absorption is rare. Human exposure to cadmium is possible through a number of several sources including employment in primary metal industries, eating contaminated food, smoking cigarettes, and working in cadmium-contaminated work places, with smoking being a major contributor [91, 92]. Other sources of cadmium include emissions from industrial activities, including mining, smelting, and manufacturing of batteries, pigments, stabilizers, and alloys [93]. Cadmium is also present in trace amounts in certain foods such as leafy vegetables, potatoes, grains and seeds, liver and kidney, and crustaceans and mollusks [94]. In addition, foodstuffs that are rich in cadmium can greatly increase the cadmium concentration in human bodies. Examples are liver, mushrooms, shellfish, mussels, cocoa powder and dried seaweed. An important distribution route is the circulatory system whereas blood vessels are considered to be main stream organs of cadmium toxicity. Chronic inhalation exposure to cadmium particulates is generally associated with changes in pulmonary function and chest radiographs that are consistent with emphysema [95]. Workplace exposure to airborne cadmium particulates has been associated with decreases in olfactory function [96]. Several epidemiologic studies have documented an association of chronic low-level cadmium exposure with decreases in bone mineral density and osteoporosis [97–99].

Exposure to cadmium is commonly determined by measuring cadmium levels in blood or urine. Blood cadmium reflects recent cadmium exposure (from smoking, for example). Cadmium in urine (usually adjusted for dilution by calculating the cadmium/creatinine ratio) indicates accumulation, or kidney burden of cadmium [100, 101]. It is estimated that about 2.3% of the U.S. population has elevated levels of urine cadmium (>2µg/g creatinine), a marker of chronic exposure and body burden [102]. Blood and urine cadmium levels are typically higher in cigarette smokers, intermediate in former smokers and lower in nonsmokers [102, 103]. Because of continuing use of cadmium in industrial applications, the environmental contamination and human exposure to cadmium have dramatically increased during the past century [104].

Molecular Mechanisms of Toxicity and Carcinogenicity

Cadmium is a severe pulmonary and gastrointestinal irritant, which can be fatal if inhaled or ingested. After acute ingestion, symptoms such as abdominal pain, burning sensation, nausea, vomiting, salivation, muscle cramps, vertigo, shock, loss of consciousness and convulsions usually appear within 15 to 30 min [105]. Acute cadmium ingestion can also cause gastrointestinal tract erosion, pulmonary, hepatic or renal injury and coma, depending on the route of poisoning [105, 106]. Chronic exposure to cadmium has a depressive effect on levels of norepinephrine, serotonin, and acetylcholine [107]. Rodent studies have shown that chronic inhalation of cadmium causes pulmonary adenocarcinomas [108, 109]. It can also cause prostatic proliferative lesions including adenocarcinomas, after systemic or direct exposure [110].

Although the mechanisms of cadmium toxicity are poorly understood, it has been speculated that cadmium causes damage to cells primarily through the generation of ROS [111], which causes single-strand DNA damage and disrupts the synthesis of nucleic acids and proteins [112]. Studies using two-dimensional gel electrophoresis have shown that several stress response systems are

expressed in response to cadmium exposure, including those for heat shock, oxidative stress, stringent response, cold shock, and SOS [113–115]. *In vitro* studies indicate that cadmium induces cytotoxic effects at the concentrations 0.1 to 10 mM and free radical-dependent DNA damage [116, 117]. *In vivo* studies have shown that cadmium modulates male reproduction in mice model at a concentration of 1 mg/kg body weight [118]. However, cadmium is a weak mutagen when compared with other carcinogenic metals [119]. Previous reports have indicated that cadmium affects signal transduction pathways; inducing inositol polyphosphate formation, increasing cytosolic free calcium levels in various cell types [120], and blocking calcium channels [121, 122]. At lower concentrations (1–100 μ M), cadmium binds to proteins, decreases DNA repair [123], activates protein degradation, up-regulates cytokines and proto-oncogenes such as c-*fos*, c-*jun*, and c-*myc* [124], and induces expression of several genes including metallothioneins [125], heme oxygenases, glutathione transferases, heat-shock proteins, acute-phase reactants, and DNA polymerase β [126].

Cadmium compounds are classified as human carcinogens by several regulatory agencies. The International Agency for Research on Cancer [91] and the U.S. National Toxicology Program have concluded that there is adequate evidence that cadmium is a human carcinogen. This designation as a human carcinogen is based primarily on repeated findings of an association between occupational cadmium exposure and lung cancer, as well as on very strong rodent data showing the pulmonary system as a target site [91]. Thus, the lung is the most definitively established site of human carcinogenesis from cadmium exposure. Other target tissues of cadmium carcinogenesis in animals include injection sites, adrenals, testes, and the hemopoietic system [91, 108, 109]. In some studies, occupational or environmental cadmium exposure has also been associated with development of cancers of the prostate, kidney, liver, hematopoietic system and stomach [108, 109]. Carcinogenic metals including arsenic, cadmium, chromium, and nickel have all been associated with DNA damage through base pair mutation, deletion, or oxygen radical attack on DNA [126]. Animal studies have demonstrated reproductive and teratogenic effects. Small epidemiologic studies have noted an inverse relationship between cadmium in cord blood, maternal blood or maternal urine and birth weight and length at birth [127, 128].

Chromium

Environmental Occurrence, Industrial Production and Use

Chromium (Cr) is a naturally occurring element present in the earth's crust, with oxidation states (or valence states) ranging from chromium (II) to chromium (VI) [129]. Chromium compounds are stable in the trivalent [Cr(III)] form and occur in nature in this state in ores, such as ferrochromite. The hexavalent [Cr(VI)] form is the second-most stable state [28]. Elemental chromium [Cr(0)] does not occur naturally. Chromium enters into various environmental matrices (air, water, and soil) from a wide variety of natural and anthropogenic sources with the largest release coming from industrial establishments. Industries with the largest contribution to chromium release include metal processing, tannery facilities, chromate production, stainless steel welding, and ferrochrome and chrome pigment production. The increase in the environmental concentrations of chromium has been linked to air and wastewater release of chromium, mainly from metallurgical, refractory, and chemical industries. Chromium released into the environment from anthropogenic activity occurs mainly in the hexavalent form [Cr(VI)] [130]. Hexavalent chromium [Cr(VI)] is a toxic industrial pollutant that is classified as human carcinogen by several regulatory and non-regulatory agencies [130–132]. The health hazard associated with exposure to chromium depends on its oxidation state, ranging from the low toxicity of the metal form to the high toxicity of the hexavalent form. All Cr(VI)-containing compounds were once thought to be man-made, with only Cr(III) naturally ubiquitous in air, water, soil and biological materials. Recently, however, naturally occurring Cr(VI) has been found in ground and surface waters at values exceeding the World Health Organization limit for drinking water of 50 µg of Cr(VI) per liter [133]. Chromium is widely used in numerous industrial processes and as a result, is a contaminant of many environmental systems [134]. Commercially chromium compounds are used in industrial welding, chrome plating, dyes and pigments, leather tanning and wood preservation. Chromium is also used as anticorrosive in cooking systems and boilers [135, 136].

Potential for Human Exposure

It is estimated that more than 300,000 workers are exposed annually to chromium and chromium-containing compounds in the workplace. In humans and animals, [Cr(III)] is an essential nutrient that plays a role in glucose, fat and protein metabolism by potentiating the action of insulin [5]. However, occupational exposure has been a major concern because of the high risk of Cr-induced diseases in industrial workers occupationally exposed to Cr(VI) [137]. Also, the general human population and some wildlife may also be at risk. It is estimated that 33 tons of total Cr are released annually into the environment [130]. The U.S. Occupational Safety and Health Administration (OSHA) recently set a "safe" level of $5\mu g/m^3$, for an 8-hr time-weighted average, even though this revised level may still pose a carcinogenic risk [138]. For the general human population, atmospheric levels range from 1 to 100 ng/cm³ [139], but can exceed this range in areas that are close to Cr manufacturing.

Non-occupational exposure occurs via ingestion of chromium containing food and water whereas occupational exposure occurs via inhalation [140]. Chromium concentrations range between 1 and 3000 mg/kg in soil, 5 to 800 µg/L in sea water, and 26 µg/L to 5.2 mg/L in rivers and lakes [129]. Chromium content in foods varies greatly and depends on the processing and preparation. In general, most fresh foods typically contain chromium levels ranging from <10 to 1,300 µg/kg. Present day workers in chromium-related industries can be exposed to chromium concentrations two orders of magnitude higher than the general population [141]. Even though the principal route of human exposure to chromium is through inhalation, and the lung is the primary target organ, significant human exposure to chromium has also been reported to take place through the skin [142, 143]. For example, the widespread incidence of dermatitis noticed among construction workers is attributed to their exposure to chromium present in cement [143]. Occupational and environmental exposure to Cr(VI)-containing compounds is known to cause multiorgan toxicity such as renal damage, allergy and asthma, and cancer of the respiratory tract in humans [5, 144].

Breathing high levels of chromium (VI) can cause irritation to the lining of the nose, and nose ulcers. The main health problems seen in animals following ingestion of chromium (VI) compounds are irritation and ulcers in the stomach and small intestine, anemia, sperm damage and male reproductive system damage. Chromium (III) compounds are much less toxic and do not appear to cause these problems. Some individuals are extremely sensitive to chromium(VI) or chromium(III), allergic reactions consisting of severe redness and swelling of the skin have been noted. An increase in stomach tumors was observed in humans and animals exposed to chromium(VI) in drinking water. Accidental or intentional ingestion of extremely high doses of chromium (VI) compounds by humans has resulted in severe respiratory, cardiovascular, gastrointestinal, hematological, hepatic, renal, and neurological effects as part of the sequelae leading to death or in patients who survived because of medical treatment [141]. Although the evidence of carcinogenicity of chromium in humans and terrestrial mammals seems strong, the mechanism by which it causes cancer is not completely understood [145].

Mechanisms of Toxicity and Carcinogenicity

Major factors governing the toxicity of chromium compounds are oxidation state and solubility. Cr(VI) compounds, which are powerful oxidizing agents and thus tend to be irritating and corrosive, appear to be much more toxic systemically than Cr(III) compounds, given similar amount and solubility [146, 147]. Although the mechanisms of biological interaction are uncertain, the variation in toxicity may be related to the ease with which Cr(VI) can pass through cell membranes and its subsequent intracellular reduction to reactive intermediates. Since Cr(III) is poorly absorbed by any route, the toxicity of chromium is mainly attributable to the Cr(VI) form. It can be absorbed by the lung and gastrointestinal tract, and even to a certain extent by intact skin. The reduction of Cr(VI) is considered as being a detoxification process when it occurs at a distance from the target site for toxic or genotoxic effect while reduction of Cr(VI) may serve to activate chromium toxicity if it takes place in or near the cell nucleus of target organs [148]. If Cr(VI) is reduced to Cr(III) extracellularly, this form of the metal is not readily transported into cells and so toxicity is not observed. The balance that exists between extracellular Cr(VI) and intracellular Cr(III) is what ultimately dictates the amount and rate at which Cr(VI) can enter cells and impart its toxic effects [134].

Cr(VI) enters many types of cells and under physiological conditions can be reduced by hydrogen peroxide (H₂O₂), glutathione (GSH) reductase, ascorbic acid, and GSH to produce reactive intermediates, including Cr(V), Cr(IV), thiylradicals, hydroxyl radicals, and ultimately, Cr(III). Any of these species could attack DNA, proteins, and membrane lipids, thereby disrupting cellular integrity and functions [149, 150].

Studies with animal models have also reported many harmful effects of Cr (VI) on mammals. Subcutaneous administration of Cr (VI) to rats caused severe progressive proteinuria, urea nitrogen and creatinine, as well as elevation in serum alanine aminotransferase activity and hepatic lipid peroxide formation [151]. Similar studies reported by Gumbleton and Nicholls [152] found that Cr (VI) induced renal damage in rats when administered by single sub-cutaneous injections. Bagchi et al. demonstrated that rats received Cr (VI) orally in water induced hepatic mitochondrial and microsomal lipid peroxidation, as well as enhanced excretion of urinary lipid metabolites including malondialdehyde [153, 154].

Adverse health effects induced by Cr (VI) have also been reported in humans. Epidemiological investigations have reported respiratory cancers in workers occupationally exposed to Cr (VI)-containing compounds [142, 148]. DNA strand breaks in peripheral lymphocytes and lipid peroxidation products in urine observed in chromium-exposed workers also support the evidence of Cr (VI)-induced toxicity to humans [155, 156]. Oxidative damage is considered to be the underlying cause of these genotoxic effects including chromosomal abnormalities [157, 158], and DNA strand breaks [159]. Nevertheless, recent studies indicate a biological relevance of non-oxidative mechanisms in Cr(VI) carcinogenesis [160].

Carcinogenicity appears to be associated with the inhalation of the less soluble/insoluble Cr(VI) compounds. The toxicology of Cr(VI) does not reside with the elemental form. It varies greatly among a wide variety of very different Cr(VI) compounds [161]. Epidemiological evidence strongly points to Cr(VI) as the agent in carcinogenesis. Solubility and other characteristics of chromium, such as size, crystal modification, surface charge, and the ability to be phagocytized might be important in determining cancer risk [135].

Studies in our laboratory have indicated that chromium (VI) is cytotoxic and able to induce DNA damaging effects such as chromosomal abnormalities [162], DNA strand breaks, DNA fragmentation and oxidative stress in Sprague-Dawley rats and human liver carcinoma cells [27, 28]. Recently, our laboratory has also demonstrated that chromium (VI) induces biochemical, genotoxic and histopathologic effects in liver and kidney of goldfish, *carassius auratus* [163].

Various hypotheses have been proposed to explain the carcinogenicity of chromium and its salts, however some inherent difficulties exist when discussing metal carcinogenesis. A metal cannot be classified as carcinogenic per se since its different compounds may have different potencies. Because of the multiple chemical exposure in industrial establishments, it is difficult from an epidemiological standpoint to relate the carcinogenic effect to a single compound. Thus, the carcinogenic risk must often be related to a process or to a group of metal compounds rather than to a single substance. Differences in carcinogenic potential are related not only to different chemical forms of the same metal but also to the particle size of the inhaled aerosol and to physical characteristics of the particle such as surface charge and crystal modification [164].

Lead

Environmental Occurrence, Industrial Production and Use

Lead is a naturally occurring bluish-gray metal present in small amounts in the earth's crust. Although lead occurs naturally in the environment, anthropogenic activities such as fossil fuels burning, mining, and manufacturing contribute to the release of high concentrations. Lead has many different industrial, agricultural and domestic applications. It is currently used in the production of lead-acid batteries, ammunitions, metal products (solder and pipes), and devices to shield X-rays. An estimated 1.52 million metric tons of lead were used for various industrial applications in the United Stated in 2004. Of that amount, lead-acid batteries

production accounted for 83 percent, and the remaining usage covered a range of products such as ammunitions (3.5 percent), oxides for paint, glass, pigments and chemicals (2.6 percent), and sheet lead (1.7 percent) [165, 166].

In recent years, the industrial use of lead has been significantly reduced from paints and ceramic products, caulking, and pipe solder [167]. Despite this progress, it has been reported that among 16.4 million United States homes with more than one child younger than 6 years per household, 25% of homes still had significant amounts of lead-contaminated deteriorated paint, dust, or adjacent bare soil [168]. Lead in dust and soil often re-contaminates cleaned houses [169] and contributes to elevating blood lead concentrations in children who play on bare, contaminated soil [170]. Today, the largest source of lead poisoning in children comes from dust and chips from deteriorating lead paint on interior surfaces [171]. Children who live in homes with deteriorating lead paint can achieve blood lead concentrations of 20µg/dL or greater [172].

Potential for Human Exposure

Exposure to lead occurs mainly via inhalation of lead-contaminated dust particles or aerosols, and ingestion of lead-contaminated food, water, and paints [173, 174]. Adults absorb 35 to 50% of lead through drinking water and the absorption rate for children may be greater than 50%. Lead absorption is influenced by factors such as age and physiological status. In the human body, the greatest percentage of lead is taken into the kidney, followed by the liver and the other soft tissues such as heart and brain, however, the lead in the skeleton represents the major body fraction [175]. The nervous system is the most vulnerable target of lead poisoning. Headache, poor attention spam, irritability, loss of memory and dullness are the early symptoms of the effects of lead exposure on the central nervous system [170, 173].

Since the late 1970's, lead exposure has decreased significantly as a result of multiple efforts including the elimination of lead in gasoline, and the reduction of lead levels in residential paints, food and drink cans, and plumbing systems [173, 174]. Several federal programs implemented by state and local health governments have not only focused on banning lead in gasoline, paint and soldered cans, but have also supported screening programs for lead poisoning in children and lead abatement in housing [167]. Despite the progress in these programs, human exposure to lead remains a serious health problem [176, 177]. Lead is the most systemic toxicant that affects several organs in the body including the kidneys, liver, central nervous system, hematopoetic system, endocrine system, and reproductive system [173].

Lead exposure usually results from lead in deteriorating household paints, lead in the work place, lead in crystals and ceramic containers that leaches into water and food, lead use in hobbies, and lead use in some traditional medicines and cosmetics [167, 174]. Several studies conducted by the National Health and Nutrition Examination surveys (NHANES) have measured blood lead levels in the U.S. populations and have assessed the magnitude of lead exposure by age, gender, race, income and degree of urbanization [176]. Although the results of these surveys have demonstrated a general decline in blood lead levels since the 1970s, they have also shown that large populations of children continue to have elevated blood lead levels (> $10\mu g/dL$). Hence, lead poisoning remains one of the most common pediatric health problems in the United States today [167, 173, 174, 176–179]. Exposure to lead is of special concern among women particularly during pregnancy. Lead absorbed by the pregnant mother is readily transferred to the developing fetus [180]. Human evidence corroborates animal findings [181], linking prenatal exposure to lead with reduced birth weight and preterm delivery [182], and with neuro-developmental abnormalities in offspring [183].

Molecular Mechanisms of Toxicity and Carcinogenicity

There are many published studies that have documented the adverse effects of lead in children and the adult population. In children, these studies have shown an association between blood level poisoning and diminished intelligence, lower intelligence quotient-IQ, delayed or impaired neurobehavioral development, decreased hearing acuity, speech and language handicaps, growth retardation, poor attention span, and anti social and diligent behaviors [178, 179, 184, 185]. In the adult population, reproductive effects, such as decreased sperm count in men and spontaneous abortions in women have been associated with high lead exposure

[186, 187]. Acute exposure to lead induces brain damage, kidney damage, and gastrointestinal diseases, while chronic exposure may cause adverse effects on the blood, central nervous system, blood pressure, kidneys, and vitamin D metabolism [173, 174, 178, 179, 184–187].

One of the major mechanisms by which lead exerts its toxic effect is through biochemical processes that include lead's ability to inhibit or mimic the actions of calcium and to interact with proteins [173]. Within the skeleton, lead is incorporated into the mineral in place of calcium. Lead binds to biological molecules and thereby interfering with their function by a number of mechanisms. Lead binds to sulfhydryl and amide groups of enzymes, altering their configuration and diminishing their activities. Lead may also compete with essential metallic cations for binding sites, inhibiting enzyme activity, or altering the transport of essential cations such as calcium [188]. Many investigators have demonstrated that lead intoxication induces a cellular damage mediated by the formation of reactive oxygen species (ROS) [189]. In addition, Jiun and Hseien [190] demonstrated that the levels of malondialdehyde (MDA) in blood strongly correlate with lead concentration in the blood of exposed workers. Other studies showed that the activities of antioxidant enzymes, including superoxide dismutase (SOD), and glutathione peroxidase in erythrocytes of workers exposed to lead are remarkably higher than that in non-exposed workers [191]. A series of recent studies in our laboratory demonstrated that lead-induced toxicity and apoptosis in human cancer cells involved several cellular and molecular processes including induction of cell death and oxidative stress [29, 192], transcriptional activation of stress genes [30], DNA damage [29], externalization of phosphatidylserine and activation of caspase-3 [193].

A large body of research has indicated that lead acts by interfering with calcium-dependent processes related to neuronal signaling and intracellular signal transduction. Lead perturbs intracellular calcium cycling, altering releasability of organelle stores, such as endoplasmic reticulum and mitochondria [194, 195]. In some cases lead inhibits calcium-dependent events, including calcium-dependent release of several neurotransmitters and receptor-coupled ionophores in glutamatergic neurons [196]. In other cases lead appears to augment calcium-dependent events, such as protein kinase C and calmodulin [194, 197].

Experimental studies have indicated that lead is potentially carcinogenic, inducing renal tumors in rats and mice [198, 199], and is therefore considered by the IARC as a probable human carcinogen [200]. Lead exposure is also known to induce gene mutations and sister chromatid exchanges [201, 202], morphological transformations in cultured rodent cells [203], and to enhance anchorage independence in diploid human fibroblasts [204]. *In vitro* and *in vivo* studies indicated that lead compounds cause genetic damage through various indirect mechanisms that include inhibition of DNA synthesis and repair, oxidative damage, and interaction with DNA-binding proteins and tumor suppressor proteins. Studies by Roy and his group showed that lead acetate induced mutagenicity at a toxic dose at the *E. coli gpt* locus transfected to V79 cells [205]. They also reported that toxic doses of lead acetate and lead nitrate induced DNA breaks at the *E. coli gpt* locus transfected to V79 cells [205]. Another study by Wise and his collaborators found no evidence for direct genotoxic or DNA-damaging effects of lead except for lead chromate. They pointed out that the genotoxicity may be due to hexavalent chromate rather than lead [206].

Mercury

Environmental Occurrence, Industrial Production and Use

Mercury is a heavy metal belonging to the transition element series of the periodic table. It is unique in that it exists or is found in nature in three forms (elemental, inorganic, and organic), with each having its own profile of toxicity [207]. At room temperature elemental mercury exists as a liquid which has a high vapor pressure and is released into the environment as mercury vapor. Mercury also exists as a cation with oxidation states of +1 (mercurous) or +2 (mercuric) [208]. Methylmercury is the most frequently encountered compound of the organic form found in the environment, and is formed as a result of the methylation of inorganic (mercuric) forms of mercury by microorganisms found in soil and water [209].

Mercury is a widespread environmental toxicant and pollutant which induces severe alterations in the body tissues and causes a

wide range of adverse health effects [210]. Both humans and animals are exposed to various chemical forms of mercury in the environment. These include elemental mercury vapor (Hg^0) , inorganic mercurous (Hg^{+1}) , mercuric (Hg^{+2}) , and the organic mercury compounds [211]. Because mercury is ubiquitous in the environment, humans, plants and animals are all unable to avoid exposure to some form of mercury [212].

Mercury is utilized in the electrical industry (switches, thermostats, batteries), dentistry (dental amalgams), and numerous industrial processes including the production of caustic soda, in nuclear reactors, as antifungal agents for wood processing, as a solvent for reactive and precious metal, and as a preservative of pharmaceutical products [213]. The industrial demand for mercury peaked in 1964 and began to sharply decline between 1980 and 1994 as a result of federal bans on mercury additives in paints, pesticides, and the reduction of its use in batteries [214].

Potential for Human Exposure

Humans are exposed to all forms of mercury through accidents, environmental pollution, food contamination, dental care, preventive medical practices, industrial and agricultural operations, and occupational operations [215]. The major sources of chronic, low level mercury exposure are dental amalgams and fish consumption. Mercury enters water as a natural process of off-gassing from the earth's crust and also through industrial pollution [216]. Algae and bacteria methylate the mercury entering the waterways. Methyl mercury then makes its way through the food chain into fish, shellfish, and eventually into humans [217].

The two most highly absorbed species are elemental mercury (Hg⁰) and methyl mercury (MeHg). Dental amalgams contain over 50% elemental mercury [218]. The elemental vapor is highly lipophilic and is effectively absorbed through the lungs and tissues lining the mouth. After Hg⁰ enters the blood, it rapidly passes through cell membranes, which include both the blood-brain barrier and the placental barrier [219]. Once it gains entry into the cell, Hg⁰ is oxidized and becomes highly reactive Hg²⁺. Methyl mercury derived from eating fish is readily absorbed in the gastrointestinal tract and because of its lipid solubility, can easily cross both the placental and blood-brain barriers. Once mercury is absorbed it has a very low excretion rate. A major proportion of what is absorbed accumulates in the kidneys, neurological tissue and the liver. All forms of mercury are toxic and their effects include gastrointestinal toxicity, neurotoxicity, and nephrotoxicity [213].

Molecular Mechanisms of Mercury Toxicity and Carcingenicity

The molecular mechanisms of toxicity of mercury are based on its chemical activity and biological features which suggest that oxidative stress is involved in its toxicity [220]. Through oxidative stress mercury has shown mechanisms of sulfhydryl reactivity. Once in the cell both Hg^{2+} and MeHg form covalent bonds with cysteine residues of proteins and deplete cellular antioxidants. Antioxidant enzymes serve as a line of cellular defense against mercury compounds [221]. The interaction of mercury compounds suggests the production of oxidative damage through the accumulation of reactive oxygen species (ROS) which would normally be eliminated by cellular antioxidants.

In eukaryotic organisms the primary site for the production of reactive oxygen species (ROS) occurs in the mitochondria through normal metabolism [222]. Inorganic mercury has been reported to increase the production of these ROS by causing defects in oxidative phosphorylation and electron transport at the ubiquinone-cytochrome b5 step [223]. Through the acceleration of the rate of electron transfer in the electron transport chain in the mitochondria, mercury induces the premature shedding of electrons to molecular oxygen which causes an increase in the generation of reactive oxygen species [224].

Oxidative stress appears to also have an effect on calcium homeostasis. The role of calcium in the activation of proteases, endonucleases and phospholipases is well established. The activation of phospholipase A_2 has been shown to result in an increase in reactive oxygen species through the increase generation of arachidonic acid. Arachidonic acid has also been shown to be an important target of reactive oxygen species [225]. Both organic and inorganic mercury have been shown to alter calcium

homeostasis but through different mechanisms. Organic mercury compounds (MeHg) are believed to increase intracellular calcium by accelerating the influx of calcium from the extracellular medium and mobilizing intracellular stores, while inorganic mercury (Hg²⁺⁾ compounds increase intracellular calcium stores only through the influx of calcium from the extracellular medium [226]. Mercury compounds have also been shown to induce increased levels of MDA in both the livers, kidneys, lungs and testes of rats treated with HgCl₂ [227]. This increase in concentration was shown to correlate with the severity of hepatotoxicity and nephrotoxicity [228]. HgCl₂.induced lipid peroxidation was shown to be significantly reduced by antioxidant pretreatment with selenium. Selenium has been shown to achieve this protective effect through direct binding to mercury or serving as a cofactor for glutathione peroxidase and facilitating its ability to scavenge ROS [229]. Vitamin E has also been reported to protect against HgCl₂-induced lipid peroxidation in the liver [230].

Metal-induced carcinogenicity has been a research subject of great public health interest. Generally, carcinogenesis is considered to have three stages including initiation, promotion, and progression and metastasis. Although mutations of DNA, which can activate oncogenesis or inhibit tumor suppression, were traditionally thought to be crucial factors for the initiation of carcinogenesis, recent studies have demonstrated that other molecular events such as transcription activation, signal transduction, oncogene amplification, and recombination, also constitute significant contributing factors [231, 232]. Studies have shown that mercury and other toxic metals effect cellular organelles and adversely affect their biologic functions [231, 233]. Accumulating evidence also suggests that ROS play a major role in the mediation of metal-induced cellular responses and carcinogenesis [234–236].

The connection between mercury exposure and carcinogenesis is very controversial. While some studies have confirmed its genotoxic potential, others have not shown an association between mercury exposure and genotoxic damage [237]. In studies implicating mercury as a genotoxic agent, oxidative stress has been described has the molecular mechanism of toxicity. Hence, mercury has been shown to induce the formation of ROS known to cause DNA damage in cells, a process which can lead to the initiation of carcinogenic processes [238, 239]. The direct action of these free radicals on nucleic acids may generate genetic mutations. Although mercury-containing compounds are not mutagenic in bacterial assays, inorganic mercury has been shown to induce cell lines with doses as low as $0.5 \,\mu$ M [240]. These free radicals may also induce conformational changes in proteins that are responsible for DNA repair, mitotic spindle, and chromosomal segregation [241]. To combat these effects, cells have antioxidant mechanisms that work to correct and avoid the formation of ROS (free radicals) in excess. These antioxidant mechanisms involve low molecular weight compounds such as vitamins C and E, melatonin, glutathione, superoxide dismutase, catalase, glutathione peroxidase and glutathione reductase that protect the cells by chelating mercury and reducing its oxidative stress potential [242].

Glutathione levels in human populations exposed to methylmercury intoxication by eating contaminated fish have been shown to be higher than normal [243]. These studies were also able to confirm a direct and positive correlation between mercury and glutathione levels in blood. They also confirmed an increased mitotic index and polyploidal aberrations associated with mercury exposure [243]. Epidemiological studies have demonstrated that enzymatic activity was altered in populations exposed to mercury; producing genotoxic alterations, and suggesting that both chronic and relatively low level mercury exposures may inhibit enzyme activity and induce oxidative stress in the cells [244]. There is no doubt that the connection between mercury exposure and carcinogenesis is very controversial. However, *in-vitro* studies suggest that the susceptibility to DNA damage exists as a result of cellular exposure to mercury. These studies also indicate that mercury-induced toxicity and carcinogenicity may be cell-, organ-and/or species- specific.

Prospects

A comprehensive analysis of published data indicates that heavy metals such as arsenic cadmium, chromium, lead, and mercury, occur naturally. However, anthropogenic activities contribute significantly to environmental contamination. These metals are systemic toxicants known to induce adverse health effects in humans, including cardiovascular diseases, developmental

abnormalities, neurologic and neurobehavioral disorders, diabetes, hearing loss, hematologic and immunologic disorders, and various types of cancer. The main pathways of exposure include ingestion, inhalation, and dermal contact. The severity of adverse health effects is related to the type of heavy metal and its chemical form, and is also time- and dose-dependent. Among many other factors, speciation plays a key role in metal toxicokinetics and toxicodynamics, and is highly influenced by factors such as valence state, particle size, solubility, biotransformation, and chemical form. Several studies have shown that toxic metals exposure causes long term health problems in human populations. Although the acute and chronic effects are known for some metals, little is known about the health impact of mixtures of toxic elements. Recent reports have pointed out that these toxic elements may interfere metabolically with nutritionally essential metals such as iron, calcium, copper, and zinc [245, 246]. However, the literature is scarce regarding the combined toxicity of heavy metals. Simultaneous exposure to multiple heavy metals may produce a toxic effect that is either additive, antagonistic or synergistic.

A recent review of a number of individual studies that addressed metals interactions reported that co-exposure to metal/metalloid mixtures of arsenic, lead and cadmium produced more severe effects at both relatively high dose and low dose levels in a biomarker-specific manner [247]. These effects were found to be mediated by dose, duration of exposure and genetic factors. Also, human co-exposure to cadmium and inorganic arsenic resulted in a more pronounced renal damage than exposure to each of the elements alone [248]. In many areas of metal pollution, chronic low dose exposure to multiple elements is a major public health concern. Elucidating the mechanistic basis of heavy metal interactions is essential for health risk assessment and management of chemical mixtures. Hence, research is needed to further elucidate the molecular mechanisms and public health impact associated with human exposure to mixtures of toxic metals.

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