

Chapter 5



POND D CLOSURE ALTERNATIVES REPORT

HUTSONVILLE POWER STATION CRAWFORD COUNTY ILLINOIS

Project No: 1954

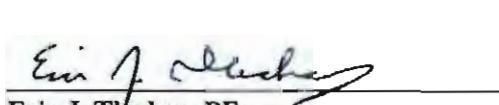
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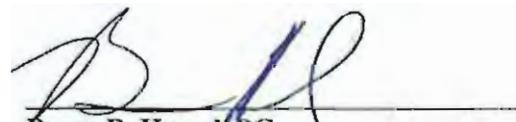

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TABLE OF CONTENTS

1	INTRODUCTION.....	1-1
1.1	Background.....	1-1
1.2	Closure Objectives and Approach	1-2
2	SITE CONDITIONS.....	2-1
2.1	Distribution of Coal Ash Fill	2-1
2.2	Hydrogeology and Groundwater Quality	2-1
2.2.1	Hydrogeology	2-1
2.2.2	Groundwater Quality.....	2-2
2.3	Potential Groundwater Receptors	2-3
3	IDENTIFICATION AND SCREENING OF CLOSURE ALTERNATIVES.....	3-1
3.1	Overview	3-1
3.2	Screening Criteria	3-1
3.3	Groundwater Management Alternatives	3-2
3.3.1	Overview	3-2
3.3.2	Site Monitoring with No Groundwater Collection	3-3
3.3.3	Groundwater Collection Trench	3-3
3.3.4	Containment Using a Low-Permeability Vertical Barrier.....	3-4
3.3.5	Ash Stabilization	3-4
3.3.6	Ash Removal and Disposal.....	3-5
3.3.7	Pond D Reconstruction.....	3-6
3.4	Final Cover Alternatives	3-6
3.5	Surface Water Management Alternatives	3-7
4	SELECTED CLOSURE ALTERNATIVES	4-1
4.1	Overview	4-1
4.2	Total Estimated Preliminary Costs for Selected Alternatives.....	4-1
5	REFERENCES.....	5-1

FIGURES

Figure 1-1	Site Location Map
Figure 1-2	Site Plan
Figure 2-1	Geologic Cross Sections
Figure 2-2	Third Quarter 2003 Upper Migration Zone Flow Contours
Figure 2-3	Fourth Quarter 2003 Upper Migration Zone Flow Contours
Figure 2-4	First Quarter 2004 Upper Migration Zone Flow Contours
Figure 2-5	Second Quarter 2004 Upper Migration Zone Flow Contours
Figure 2-6	February 12, 2007 Upper Migration Zone Flow Contours
Figure 2-7	May 13, 2007 Upper Migration Zone Flow Contours
Figure 2-8	July 2, 2007 Upper Migration Zone Flow Contours
Figure 2-9	October 2, 2007 Upper Migration Zone Flow Contours
Figure 2-10	Third Quarter 2003 Deep Alluvial Aquifer Flow
Figure 2-11	Fourth Quarter 2003 Deep Alluvial Aquifer Flow
Figure 2-12	First Quarter 2004 Deep Alluvial Aquifer Flow
Figure 2-13	Second Quarter 2004 Deep Alluvial Aquifer Flow
Figure 2-14	February 12, 2007 Deep Alluvial Aquifer Flow
Figure 2-15	May 13, 2007 Deep Alluvial Aquifer Flow
Figure 2-16	July 2, 2007 Deep Alluvial Aquifer Flow
Figure 2-17	October 2, 2007 Deep Alluvial Aquifer Flow
Figure 2-18a-d	Box-whisker plot showing parameter of concern concentrations in the upper migration zone from 2002 through 2008
Figure 2-19a-d	Box-whisker plot showing parameter of concern concentrations in the deep alluvial aquifer from 2002 through 2008
Figure 4-1	Selected Closure Alternatives

TABLES

Table 2-1	Soil Boring and Discrete Groundwater Sampling Data
Table 2-2	Monitoring Well Locations, Elevations, Depth to Bedrock, and Screened Formation
Table 2-3	Monitoring Well Completion Details
Table 2-4	Monitoring Well Slug Test Results
Table 2-5	Monitoring Well Programs, Monitored Aquifers, and Positions Relative to Pond D
Table 2-6	Groundwater Monitoring Results: Pond D Monitoring Wells
Table 3-1	Closure Alternatives Screening Summary
Table 3-2	Areal Extent and Volumes of Unsaturated and Saturated Ash in Pond D
Table 3-3	Final Cover Alternatives Material Balance Analysis

APPENDICES

- Appendix A:** Site Investigation Appendices
 A-1: Soil Boring Logs
 A-2: Monitoring Well Completion Reports and Abandonment Log
 A-3: Slug Test Data
 A-4: Groundwater Sampling SOP (AEG)
- Appendix B:** Alternative Cost Summary Sheets
- Appendix C:** Potable Well Survey

1 INTRODUCTION

1.1 Background

Ameren Energy Generating (AEG) operates the Hutsonville Power Station in Crawford County Illinois (Figure 1-1). The power station is located on the west bank of the Wabash River, one mile north of the City of Hutsonville (SW ¼, Section 17, Township 8N, Range 11W). The coal fired power plant has been in operation since the 1940's. There are currently two units operating at the plant, completed in 1953 (unit 3) and 1954 (unit 4), with a combined generating capacity of 164 MW. Fly ash from the operating units is collected by an electrostatic precipitator and sluiced to a 12-acre lined ash impoundment (Pond A, Figure 1-2), which was constructed in 1984. Bottom ash is sluiced to a separate pond and eventually recycled. Sluice water from Pond A is routed through a 4.2-acre lined interim pond (Pond B, constructed in 2000) before discharge to the Wabash River via NPDES-permitted outfall #002 (IL0000175). Sluice water from the bottom ash pond is routed through a 1.7-acre drainage collection pond (Pond C, constructed in 2000) and Pond B before discharge to the Wabash River via the same outfall.

The site also has a 22-acre unlined ash impoundment (Pond D), which was constructed in 1968. This impoundment was the primary ash management unit prior to construction of Pond A, and was used as a secondary settling pond until it was removed from service in 2000. On occasion, precipitation and flood backwater can accumulate in the impoundment and cause ponded conditions in low areas.

Groundwater quality has been monitored at this facility since 1984. Concentrations of boron and sulfate at several monitoring wells exceed the Illinois Class I groundwater quality standards (Title 35, Part 620, Illinois Administrative Code, or 35 IAC 620). Boron and sulfate are indicator parameters for coal ash leachate.

In 1999, Ameren retained Science & Technology Management, Inc. (STM) and Natural Resource Technology Inc. (NRT) to perform a hydrogeologic assessment. The hydrogeologic assessment identified a correlation between shallow groundwater quality (elevated boron and sulfate concentrations in groundwater) and potential leachate sources, namely the former ash laydown area (which was excavated prior to construction of Ponds B and C) and Pond D. Boron and sulfate are migrating east towards the Wabash River; however, there are no groundwater supply wells in the shallow sediments between Pond D and the Wabash River.

Groundwater quality data from monitoring wells in the deep alluvial aquifer, as well as periodic samples from the plant production wells show that boron and sulfate concentrations in this deeper aquifer are lower than Illinois Class I groundwater quality standards.

1.2 Closure Objectives and Approach

While Pond D has been dewatered, Ameren desires to close the impoundment so as to prevent off-site groundwater impacts and construct a final cover system to minimize infiltration. The goal of these actions is to close the impoundment in a manner protective of human health and the environment. Site-specific considerations for establishing appropriate closure objectives include a risk assessment confirming that groundwater discharge to the Wabash River from Pond D is not harming human health or the environment (AECOM, 2009).

A variety of groundwater management and final cover alternatives for closure of Pond D have been identified and screened based on factors such as technical feasibility and cost. Tables 3-1, 3-2, and 3-3 summarize the closure alternatives evaluated and screening process, which is described in Section 3.

2 SITE CONDITIONS

Hydrogeology and groundwater quality were characterized in the 1999 hydrogeologic assessment. Additional field investigation was performed in 2001 and 2004 to upgrade the monitoring well system surrounding Pond D, characterize the deep alluvial aquifer, and to collect detailed information specific to the alternatives assessment (Appendix A). Data from these sources were used to develop the description of current site conditions presented here.

Figure 1-2 shows the locations of soil borings and monitoring wells used in site investigations and monitoring. Tables 2-1 through 2-4 present information pertaining to soil borings and groundwater monitoring wells from which samples were collected.

2.1 Distribution of Coal Ash Fill

Ash at the Hutsonville Power Station has been managed in Ponds A and D. In addition, ash was placed in a laydown area between the southern portions of Ponds A and D. In 2000, all ash in the laydown area was excavated, and the interim pond (Pond B) and drainage collection pond (Pond C) were constructed in that location.

Four direct-push probe borings (GP20 through GP23) advanced through Pond D during the 1999 hydrogeologic assessment indicated ash thickness ranging from about 12 feet at the north end of the impoundment to 31 feet in the central portion of the impoundment (Figure 2-1, Section C-C'). Ash in the central and southern portions of Pond D extended as much as 16 feet below the normal water table elevation.

2.2 Hydrogeology and Groundwater Quality

2.2.1 Hydrogeology

The impoundments are underlain by two water-bearing units separated by materials that have low hydraulic conductivity (shale bedrock or silts and clays). The upland portion of the power plant property and the western portion of Pond D, are underlain by a thin (less than 20 feet thick) layer of sand-rich soil, which is underlain by Pennsylvanian-age sandstone and then shale (Figure 2-1, Cross-Section A-A'). The lowland portion of the site and eastern portion of Pond D are underlain by 90 feet of alluvium in the

Wabash River bedrock valley. The upper 20 feet of alluvium is fine-grained, primarily composed of silt and clay with thin sand lenses, while the lower 70 feet is coarse-grained, consisting of sand and gravel. Every boring drilled into the alluvium encountered the fine-grained deposits, and on-site borings that extended to the underlying sand and gravel (SB101, SB102, MW7D, MW14, MW115, and MW121) encountered 19 to 25 feet of these deposits (Figure 2-1, Cross-Section B-B'). Pennsylvanian-age shale underlies the alluvium.

The shallow upland sand and sandstone, and sand lenses in the fine-grained alluvium, are referred to as the upper migration zone, and constitute the uppermost aquifer at this site. There are 13 monitoring wells screened in this aquifer (Table 2-5); six of these wells are monitored for Pond D, and four of these are downgradient of Pond D. The coarse-grained alluvium is referred to as the deep alluvial aquifer. This aquifer is not present beneath most of the site, including the power plant, Ponds A, B, and C, and the northern and western portions of Pond D. There are five monitoring wells screened in the deep alluvial aquifer, all of which are monitored for Pond D (Table 2-5). The shale underlying the upland sandstone and the silts and clays of the fine grained alluvium separate the upper migration zone from the deep alluvial aquifer.

Groundwater flow was mapped for four consecutive quarters during which complete sample sets were available. Unfortunately, depth to water readings for all of the upper migration zone and one of the deep alluvial aquifer maps were not collected on the same day during this period. While this discrepancy did not appear to change map depictions of the overall direction of groundwater flow, it affected relative readings between wells. Therefore, a second set of drawings was produced using data collected after the plant initiated same-date measurements beginning in 2006. All maps (Figures 2-2 through 2-17) show that groundwater flow in the upper migration zone and the deep alluvial aquifer is eastward toward the Wabash River.

2.2.2 Groundwater Quality

The 1999 Hydrogeologic Assessment identified boron, sulfate, manganese, and TDS as parameters of concern (POCs) because their concentrations in groundwater near Pond D exceeded Illinois Class I groundwater quality standards. Boron and sulfate are indicator parameters of coal ash leachate, and are the primary POCs. Manganese is ubiquitous in soils, may have higher concentrations in soil than in coal ash, and is highly sensitive to redox conditions; therefore, it is not a reliable indicator of coal ash leachate. High TDS may be observed at sites where coal ash leachate migration occurs, because high TDS concentrations reflect elevated concentrations of soluble ash constituents such as calcium, potassium,

sodium, and sulfate; however, other natural and anthropogenic sources can cause high TDS concentrations, therefore it is not a reliable indicator of coal ash leachate impacts.

Pond D monitoring wells MW6, MW7, MW8, and MW11R have boron and sulfate concentrations higher than Class I standards; these wells are screened in the upper migration zone. Groundwater monitoring results are presented in Figures 2-18a and b, and Table 2-6a and b. Groundwater within the deep alluvial aquifer complies with Class 1 groundwater quality standards and reflects only nominal impacts from Pond D in only one of the five wells. The lack of significant groundwater impacts in the deep alluvial aquifer after more than 40 years of Pond D operation provides further evidence that the silts and shales separating the upper migration zone from the deep alluvial aquifer are an effective confining layer.

2.3 Potential Groundwater Receptors

There are no groundwater supply wells, other than the two plant wells, between Pond D and the Wabash River, which is the ultimate receptor of groundwater impacted by leachate from Pond D (Appendix C). The plant wells and four irrigation wells that are south of Pond D are completed in the deep alluvial aquifer.

As documented previously, groundwater in the upper migration zone downgradient of Pond D has elevated boron and sulfate concentrations and therefore represents an exposure pathway; however, this formation is not utilized for water supply in the vicinity of Pond D.

The deep alluvial aquifer is utilized as a drinking water supply by the city of Hutsonville, approximately 1 mile to the south. However, groundwater flow in this aquifer is toward the Wabash River (Figures 2-10 through 2-16). As a result, there are no potable water supply wells, other than the two plant wells, situated between Pond D and the discharge point for groundwater (the Wabash River). The plant wells have low boron and sulfate concentrations and do not show evidence of impacts from Pond D.

3 IDENTIFICATION AND SCREENING OF CLOSURE ALTERNATIVES

3.1 Overview

Several closure alternatives were identified for Pond D and evaluated to determine whether or not they would effectively and efficiently meet the closure objectives, specifically:

- Prevent off-site migration of impacted groundwater;
- Minimize infiltration of rain and snowmelt to the coal ash within Pond D; and
- Protect human health and the environment.

Alternatives that potentially meet the closure objectives are presented below and summarized in Table 3-1. These alternatives are divided into two distinct categories: Groundwater Management and Final Cover Alternatives.

Additionally, since surface water management is a necessary component of any final cover design, surface water management alternatives were developed and evaluated for incorporation into the final cover alternatives.

3.2 Screening Criteria

Screening criteria for assessing groundwater management, final cover, and surface water management alternatives consist of the following:

- Construction / Implementation Feasibility: Construction feasibility refers to the ability to build the system given site-specific conditions. Implementation feasibility refers to the ability of this alternative to meet technical factors, such as appropriateness or suitability, and availability of the technology given site-specific constraints, geographic location; and administrative factors, such as local and state permitting requirements and regulatory reviews for approval.
- Effectiveness: Effectiveness refers to the ability of the alternative to achieve the three closure objectives.

- **Cost:** Costs for the purpose of initial screening refer to relative cost ranges for each of the alternatives, and include utilization of available published cost data from similar projects, vendor data, and engineering judgment. As such, **costs are for general comparative purposes, and are not used singly as a screening tool unless substantial cost differentials would immediately preclude the technology from further consideration.**

Construction / implementation feasibility and effectiveness were significant criteria for screening. If an alternative failed these criteria, then it was not considered further. Therefore, the criteria of cost was secondary unless substantial concerns were identified that would clearly eliminate the alternative (e.g., same feasibility and effectiveness with significantly higher costs).

Comments on the screening criteria for each closure alternative are provided with the description of each alternative below and summarized on Table 3-1. Rough cost summaries for each of the alternatives are provided in Appendix B. Table 3-2 provides a summary of the areal extent and volumes of ash in Pond D used for quantity estimation in the rough cost summaries. Table 3-3 provides a material balance analysis for each of the final cover alternatives that explains how each source of fill available on site will be utilized within the final cover alternative.

3.3 Groundwater Management Alternatives

3.3.1 Overview

As noted in AECOM, 2009, groundwater migration from Pond D to the Wabash River does not pose a threat to human health and the environment. Further, impacted groundwater is localized and limited to the pond area itself and a narrow band of shallow groundwater immediately south of the property. Accordingly, the goal of the groundwater management alternatives is to prevent southward off-site migration of impacted groundwater in the upper migration zone.

The following groundwater management alternatives were evaluated:

- Site monitoring with no groundwater collection;
- Groundwater collection trench; and
- Containment using a low-permeability vertical barrier.

In addition, the following source control measures are grouped with the groundwater management alternatives because they have a similar objective of preventing off-site migration:

- Ash stabilization;
- Ash removal and disposal, recycling at an off-site facility, or beneficial reuse; and
- Ash impoundment reconstruction.

As noted in the discussion that follows, the source control measures were eliminated during the screening process because they are technologically infeasible and/or economically unviable.

3.3.2 Site Monitoring with No Groundwater Collection

This alternative represents a no-action alternative. Establishing a groundwater monitoring program will be required as a component of each Groundwater Management Alternative discussed below; therefore, costs for site monitoring have not been separately evaluated.

Groundwater modeling performed separately from this evaluation (NRT, 2009) suggests that groundwater quality at the south property boundary may achieve compliance with Class I groundwater quality within a period of about 17 years after closure of Pond D. This alternative does not achieve the objective of preventing off-site migration of impacted groundwater. Therefore the no-action component of this alternative was not carried forward, although, as presented above, the groundwater monitoring component is a necessary part of any groundwater management alternative.

3.3.3 Groundwater Collection Trench

This alternative consists of a collection trench south of Pond D. The collection trench would contain a perforated horizontal pipe surrounded by gravel bedding. A geotextile would be placed along the trench walls to filter out surrounding soils. The horizontal pipe would have a relatively shallow pitch to sumps placed along the alignment of the trench at a spacing determined by site-specific hydrogeologic conditions. Pumps would be placed in the sumps to extract groundwater from the trench. Extracted groundwater would be directly discharged to the interim pond (Pond B) for management and eventual discharge to the Wabash River via the existing NPDES permit.

This alternative was carried forward because it is capable of achieving the closure objective of preventing off-site, southward migration of impacted groundwater in the upper migration zone.

3.3.4 Containment Using a Low-Permeability Vertical Barrier

This Groundwater Management Alternative would prevent off-site migration of impacted groundwater by installing a low-permeability vertical barrier through the upper migration zone. Construction of a vertical barrier would require keying into a low-permeability geologic formation, such as shale bedrock or clay.

Two basic barrier configurations were considered:

- Partially Encapsulating Barrier: this type of barrier would be installed along the east and south (downgradient) sides of Pond D. The barrier would be completed with an interior hydraulic gradient control system utilizing groundwater collection trenches upgradient of the barrier or extraction wells within the impoundment. The hydraulic gradient control system would prevent hydraulic mounding by maintaining an inward gradient.
- Fully Encapsulating Wall: This type of barrier would surround the entire perimeter of Pond D to fully encapsulate the saturated ash zone and deflect upgradient groundwater flow around Pond D. Internal hydraulic controls would be required to manage groundwater fluctuations that could potentially compromise containment integrity. However, since this type of barrier would deflect upgradient groundwater flow, a significantly lower volume of groundwater compared to the partially encapsulating barrier would need to be extracted to maintain an inward gradient.

Several vertical barrier technologies are available, including sheet piling with sealed interlocks, cement-bentonite or soil-cement slurry, and jet grouting. Each of these technologies has the capability to create a barrier with hydraulic conductivity approaching 1×10^{-7} centimeters per second (cm/s) with proper design and construction quality control / assurance. However, without a competent low-permeability formation in which to key the barrier, proper containment cannot be achieved. Accordingly, this alternative was not considered.

3.3.5 Ash Stabilization

Ash stabilization is a technology designed to micro-encapsulate the ash in a cement-like matrix (monolith) to minimize the rate of groundwater infiltration and leaching of ash constituents to groundwater. Ash fill is stabilized and solidified using one of several reagents delivered either via soil mixing or jet grouting technology. Once the ash is stabilized, groundwater flows around, rather than through the ash, greatly reducing leachate volume and potentially eliminating the need for active groundwater management. A laboratory bench-scale test would be needed to fully quantify this alternative's feasibility and effectiveness, including whether such stabilization will effectively eliminate leaching from the coal ash as groundwater flows around the outer perimeter of the monolith.

Soil mixing utilizes large-diameter augers (5 to 12 feet in diameter) that mechanically mix soils with a stabilizing reagent carried by drilling fluid. Jet grouting utilizes a small drill rig to advance a drill bit into the soils, through which grout is pumped under high pressure. As the drill string is rotated and slowly raised, a cylindrical grout column is created. The grout injection produces grout columns ranging from approximately 2 to 5 feet in diameter. A key disadvantage of this technology is maintaining the continuity and integrity of the grout column. Discontinuities or irregularities in subsurface conditions can lead to irregularity in grout column diameter. Typically, conservative overlapping is performed to achieve uniform coverage.

This alternative was not considered due to technical uncertainties and relatively high cost compared to other groundwater management alternatives that have similar or better effectiveness and less technical uncertainty.

3.3.6 Ash Removal and Disposal

Removal of ash from Pond D eliminates the source of groundwater impacts at the site. Excavation of a significant volume of ash and extensive site dewatering throughout the course of the project would be required. For purposes of evaluating this alternative, partial removal (i.e., removal of saturated ash only) was compared to removal of all ash from Pond D. Key design and technical considerations for excavation include:

- Excavated ash would be disposed off site if not returned to its original location.
- For the partial removal alternative, a capillary break would be created following the removal of saturated ash by placing a relatively free-draining material, such as self-compacting gravel, at and above the groundwater interface. This material prevents saturation of the ash left above the groundwater interface due to capillary rise from the underlying water table, and provides a buffer to a future increase in groundwater elevation. Above the capillary break, excavated ash would be placed as backfill to grade. Above the ash backfill, an engineered cover would be constructed to minimize surface water infiltration through the unsaturated ash.
- Extensive engineering controls that could include water misting would be required for managing fugitive dust emissions.

This alternative's effectiveness would be controlled largely by the ability to remove saturated ash from below the water table. The technical and economic feasibility of this is questionable. In addition, there does not appear to be a regulatory requirement to remove ash from an IEPA-permitted impoundment facility such as Pond D. Consequently, this alternative was not considered due to its technical

uncertainties and relatively high cost compared to other groundwater management alternatives that have similar or better effectiveness and less technical uncertainty.

3.3.7 Pond D Reconstruction

Reconstruction of Pond D is identified as a Groundwater Management Alternative since the reconstructed facility would release significantly less leachate than Pond D. Reconstruction of Pond D would require extensive excavation and relocation or off-site disposal of all ash currently contained in Pond D. Pond D would then be reconstructed as a new unit designed to:

- Separate ash from the water table through the addition of clean fill to raise the base of Pond D above the water table; and
- Reduce or eliminate ash leachate migration by constructing a low-permeability liner.

Upon completion of reconstruction activities, ash removed from Pond D could either be replaced or the unit could be operated as a new ash impoundment. Alternatively, the reconstruction project could be designed to provide additional disposal capacity. If the ash removed from Pond D was replaced and no additional capacity was provided, reconstruction would not be complete until a final cover (as discussed in Section 3.4) was installed.

This alternative has similar feasibility uncertainties as the ash removal option described above with regard to the excavation of saturated ash. In addition, regulatory uncertainties associated with this alternative rendered it infeasible. Consequently, the costs for this alternative were not evaluated and it was not considered further.

3.4 Final Cover Alternatives

Four different final cover alternatives were selected for initial evaluation:

- Geomembrane (e.g., PVC);
- Compacted clay;
- Earthen (clean soil fill); and
- Pozzolanic.

The first two alternatives consist of (from the bottom up) a low-permeability layer, either a geomembrane or 3 feet of compacted clay, followed by a 3-foot thick soil layer designed to drain infiltrated surface

water from above the low-permeability layer, protect the low-permeability layer from weathering and maintenance activities on the surface of the final cover, and support vegetation.

The third alternative, a layered earthen final cover, reflects a simplified approach to conventional landfill cover design practices. Instead of relying on low-permeability clay or a geomembrane as a barrier, the design of a layered earthen cover incorporates the use of high-permeability sand and/or gravel layers to create a capillary break. The capillary break causes retention of water in the rooting zone, which increases transpiration to the atmosphere relative to covers without capillary breaks, and minimizes downward drainage. If the rooting zone becomes saturated, the high-permeability sand and/or gravel layer(s) promote rapid lateral drainage and continue to limit infiltration. However, migration of water to this drainage layer would only occur after the retention capacity of the rooting zone is reached.

Given the humid climate in this area, the layered earthen cover will not be as effective as a compacted clay or geomembrane cover in minimizing infiltration; however, a net reduction in annual infiltration can be achieved. Construction of a layered earthen cover is a lower cost approach than geomembrane or compacted clay because it relies on locally available materials and no geomembrane nor low-permeability clay is used, thus eliminating the cost of these materials themselves as well as the construction quality assurance / control efforts associated with them.

The fourth final cover alternative reflects an innovative approach to cover design. Fly ash from an on-site source (Pond A), would be collected and blended with a stabilizing reagent (e.g., quick lime, Portland cement, class C fly ash) to create a cement-like monolithic cover to minimize the rate of infiltration and leaching of ash constituents to groundwater. A 3-foot thick, low-permeability layer would be constructed from the pozzolanic fly ash mixture followed by a 3-foot thick earthen protective layer. However, mix design testing for this alternative was unable to identify a mix that achieves a permeability lower than 1×10^{-6} cm/s with adequate strength.

Of the final cover alternatives evaluated, only the geomembrane cover was carried forward. The layered earthen and pozzolanic alternatives were screened out because the geomembrane alternative is more effective at minimizing infiltration. The compacted clay alternative was screened out because it has a higher estimated cost for similar effectiveness as the geomembrane alternative.

3.5 Surface Water Management Alternatives

Three surface water management alternatives were selected for initial evaluation:

- Route surface water east towards the Wabash River;
- Route surface water west towards Pond C; and
- A combination of these two approaches.

Diverting all surface water to the Wabash River would require the most fill, while combining surface water drainage to either the Wabash River or Pond C would require the least fill. Detailed design of surface water management features will consider the stability of the dikes surrounding Pond D. A box culvert has already been constructed to route surface water from Pond D to Pond C. For purposes of estimating fill volumes to construct the surface water management alternatives, a minimum 5% slope has been assumed to provide adequate drainage and prevent standing water from accumulating in depressions on the final cover surface.

Of the Surface Water Management Alternatives evaluated, only the combination alternative was carried forward since the others are anticipated to be significantly more expensive and provide only similar effectiveness.

4 SELECTED CLOSURE ALTERNATIVES

4.1 Overview

The results of closure alternative screening are presented with the descriptions for each alternative in Section 3 and summarized in the last column of Table 3-1. To summarize briefly, the selected alternatives consist of the following:

Groundwater Management Alternative

- Groundwater collection trench

Final Cover Alternative

- Geomembrane

Surface Water Management Alternative

- Route surface water east and west towards the Wabash River and Pond C

Figure 4-1 depicts the site plan for the selected closure alternatives.

4.2 Total Estimated Preliminary Costs for Selected Alternatives

The total estimated costs for the selected closure alternatives are as follows:

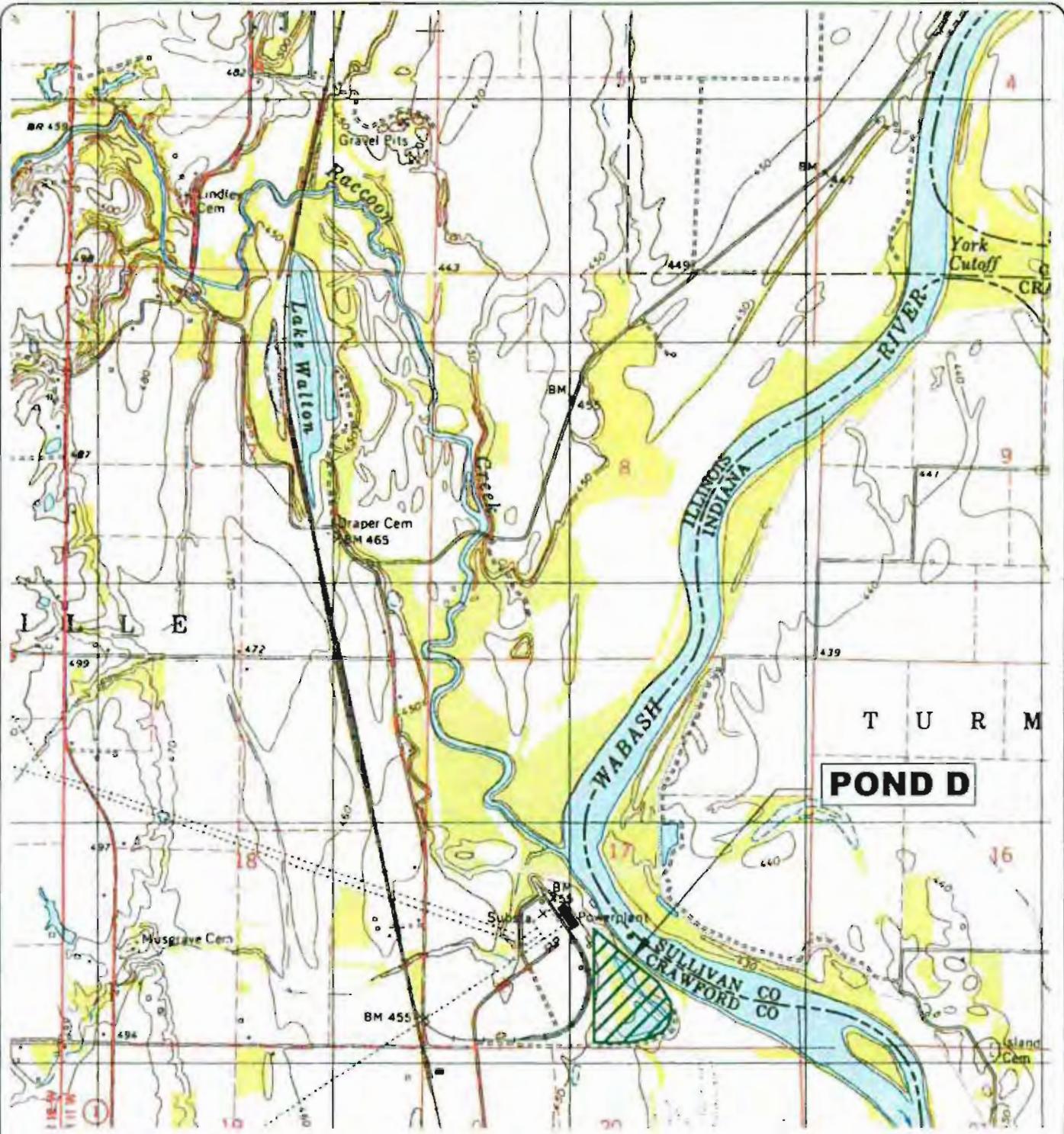
- Total Capital Cost: \$4,700,000
- Total Annual Operation & Maintenance Costs: \$52,000
- Projected 5-year Cost in 2005 Dollars: \$4,960,000
- Projected 30-year Cost in 2005 Dollars: \$6,260,000

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FIGURES

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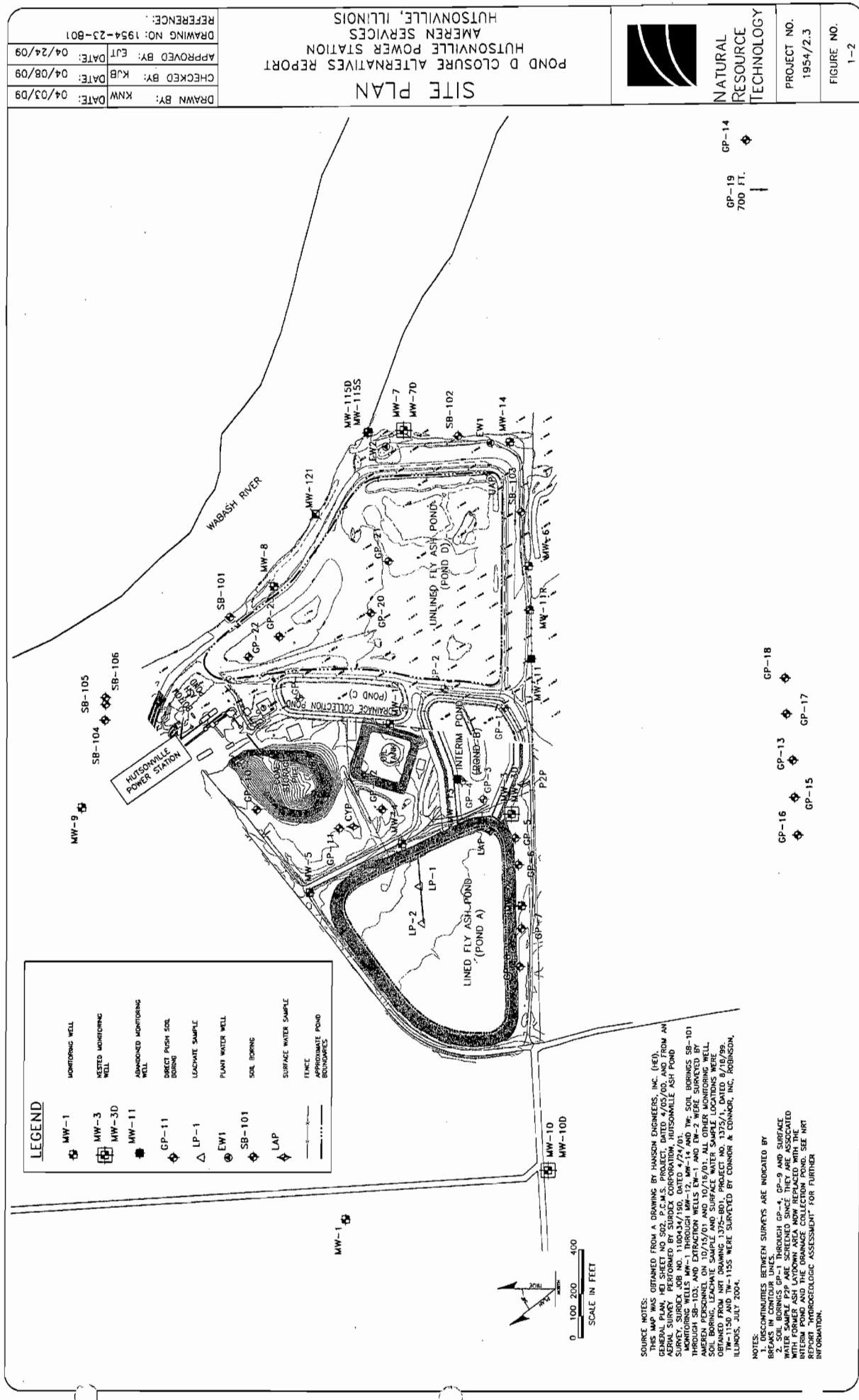
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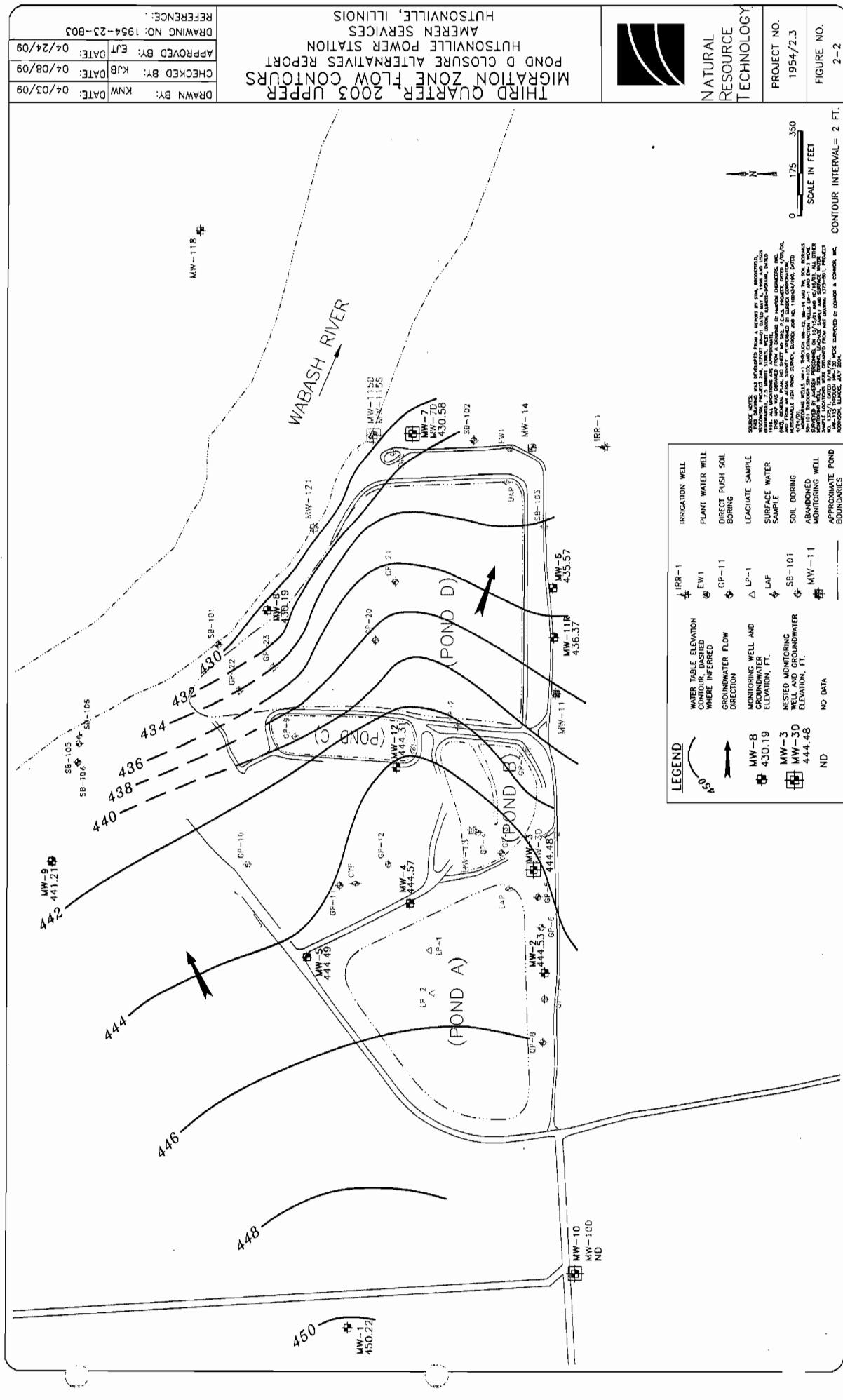
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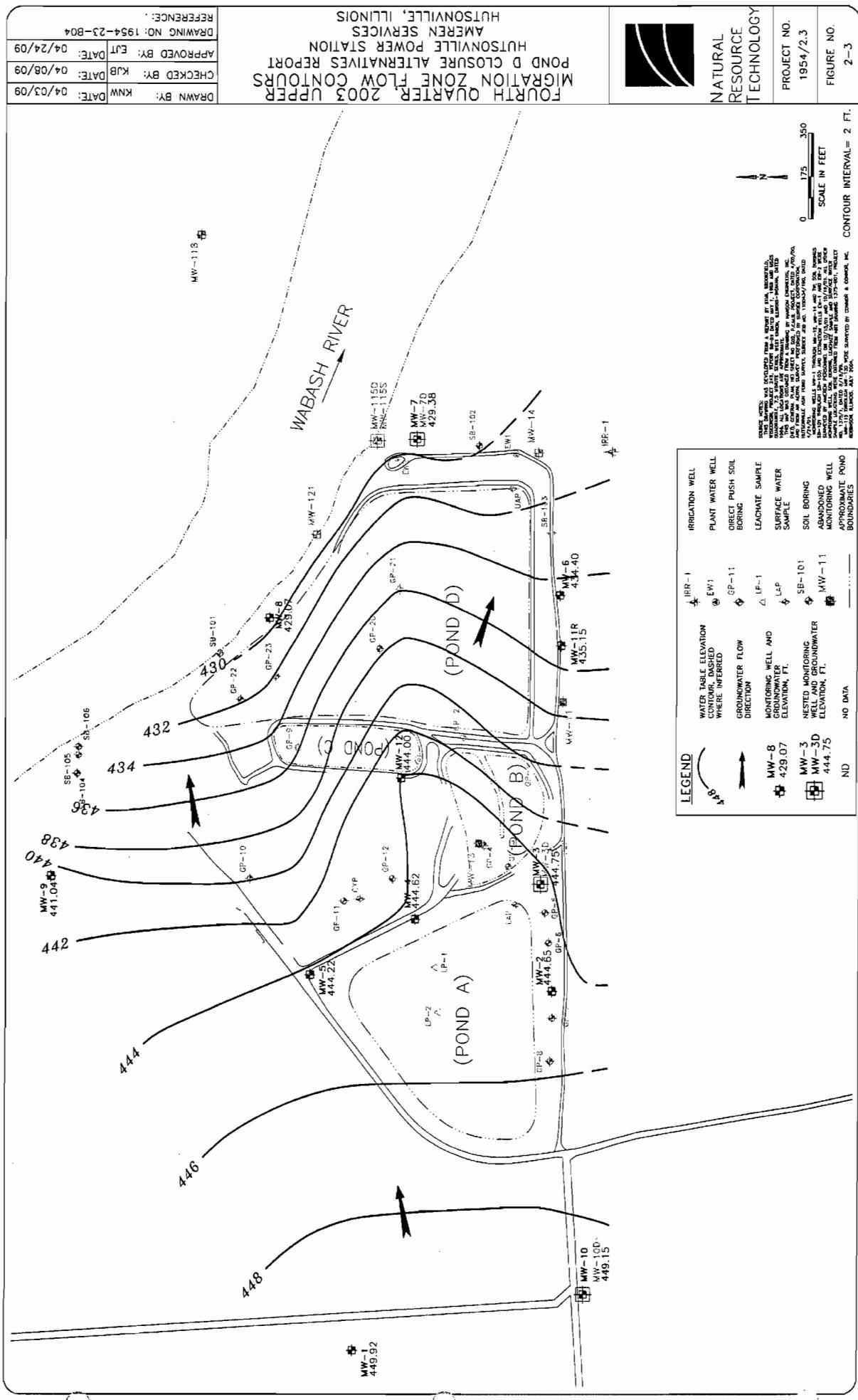
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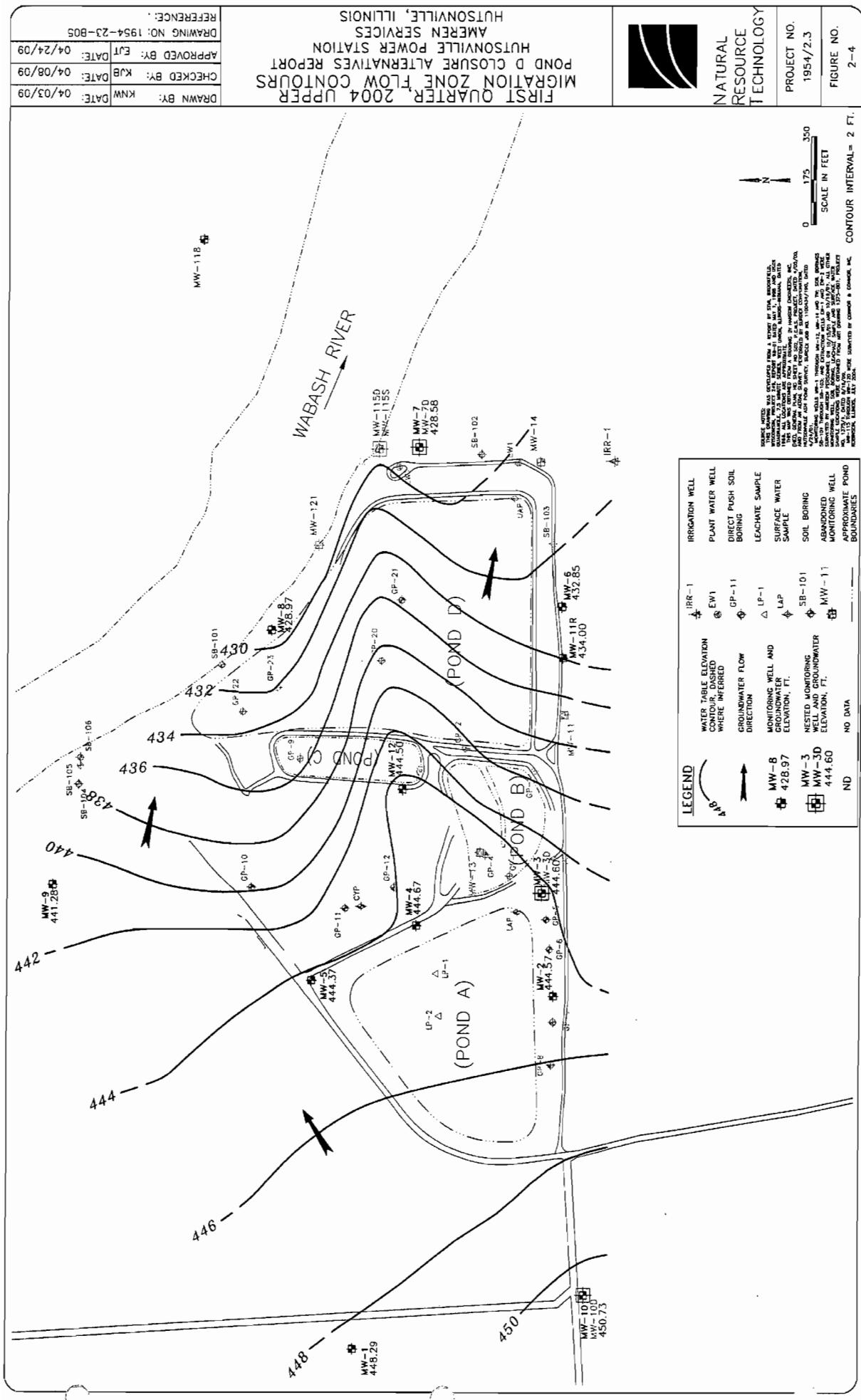
SITE LOCATION MAP
POND D CLOSURE ALTERNATIVES REPORT
AMEREN SERVICES
HUTSONVILLE, ILLINOIS

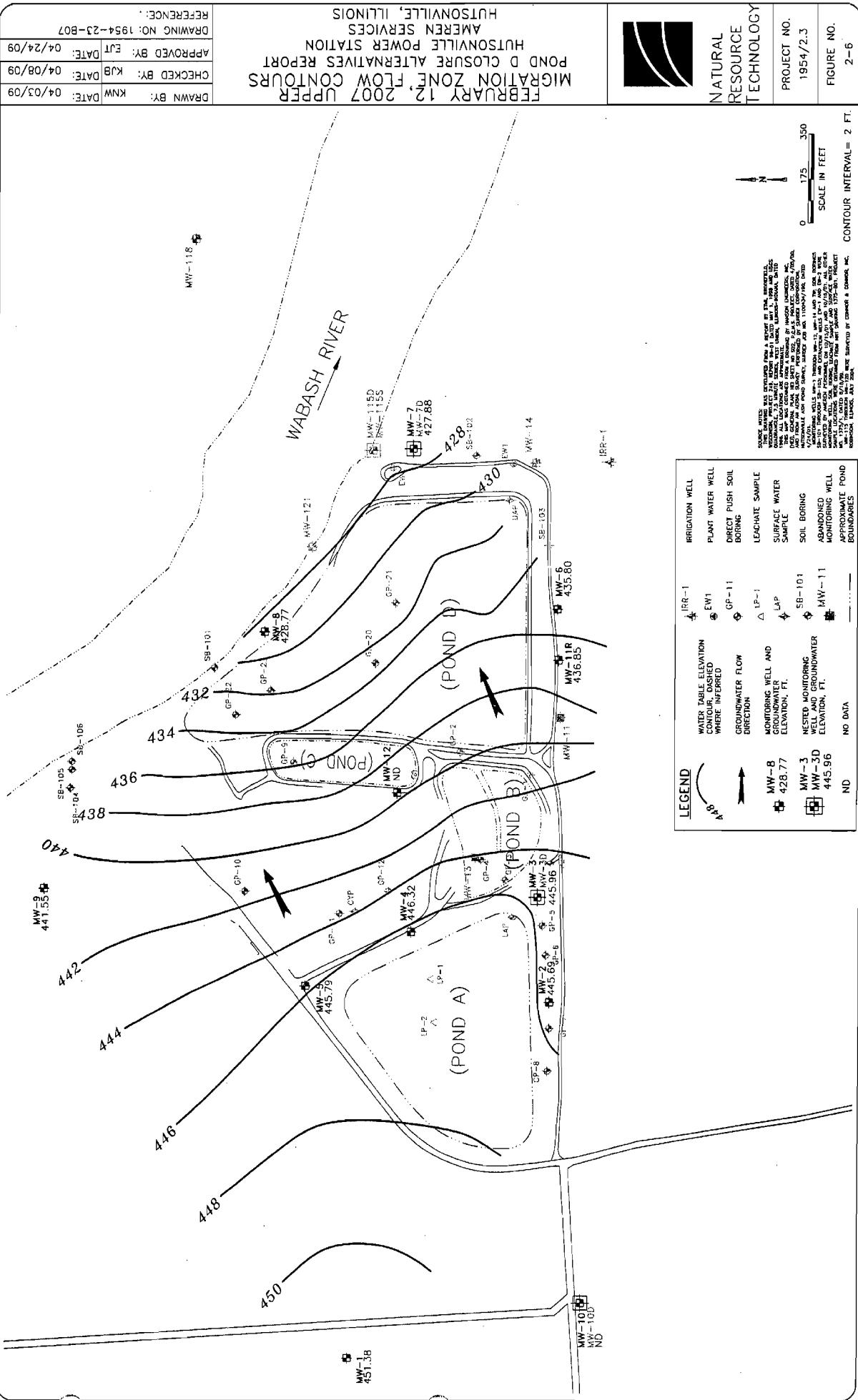
PROJECT NO.
1954
DRAWING NO.
1954-A05
FIGURE NO.
1-1

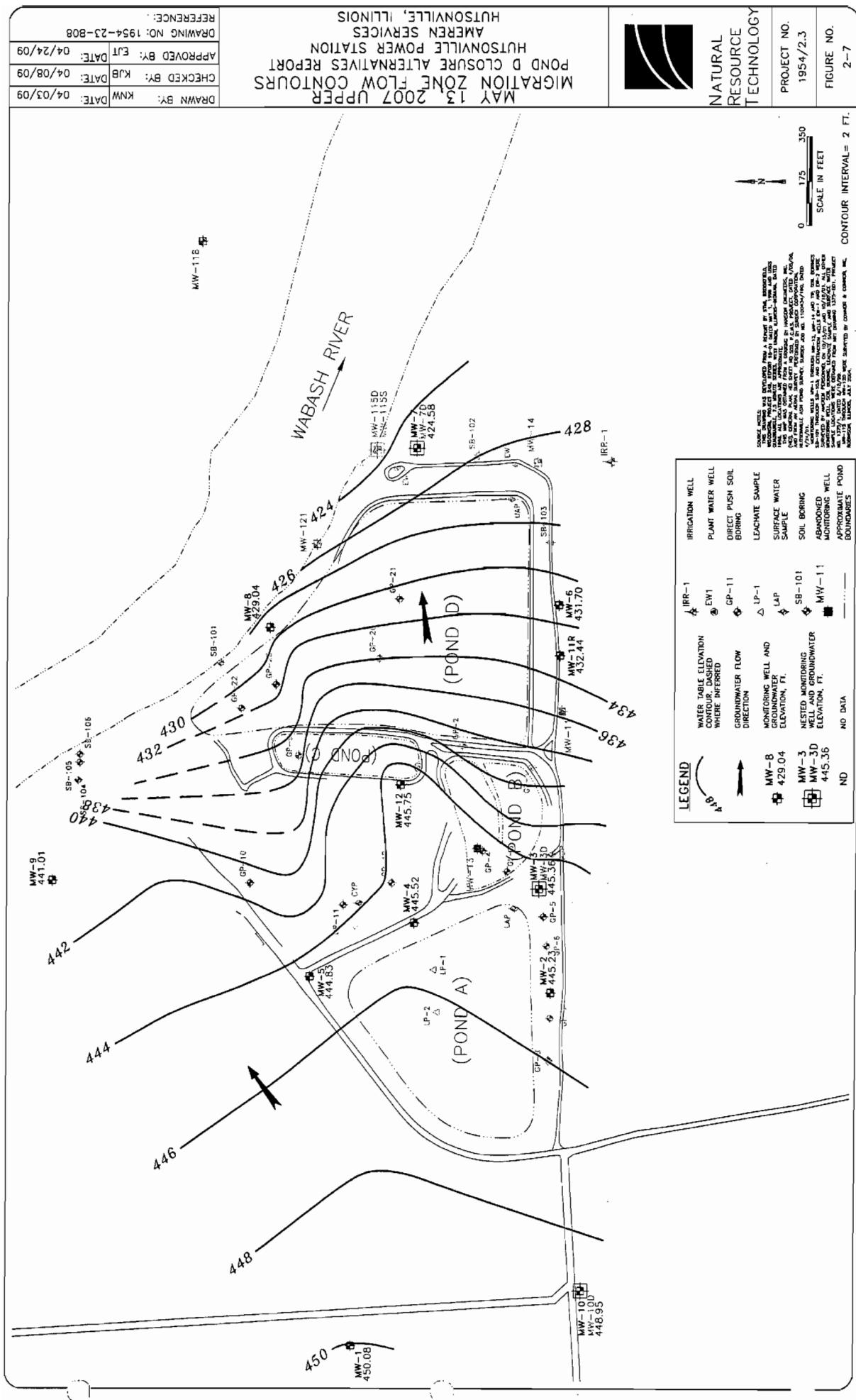


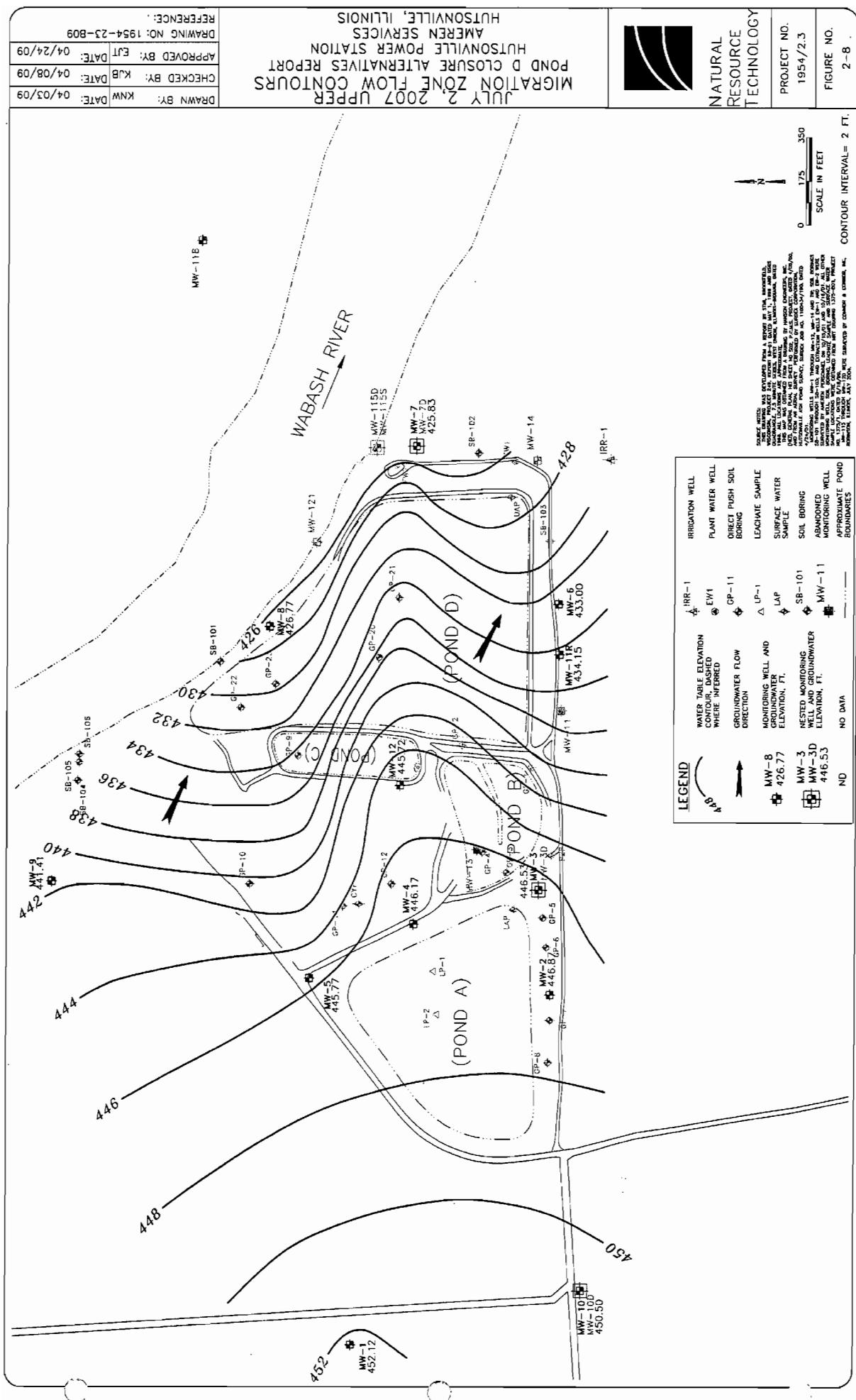


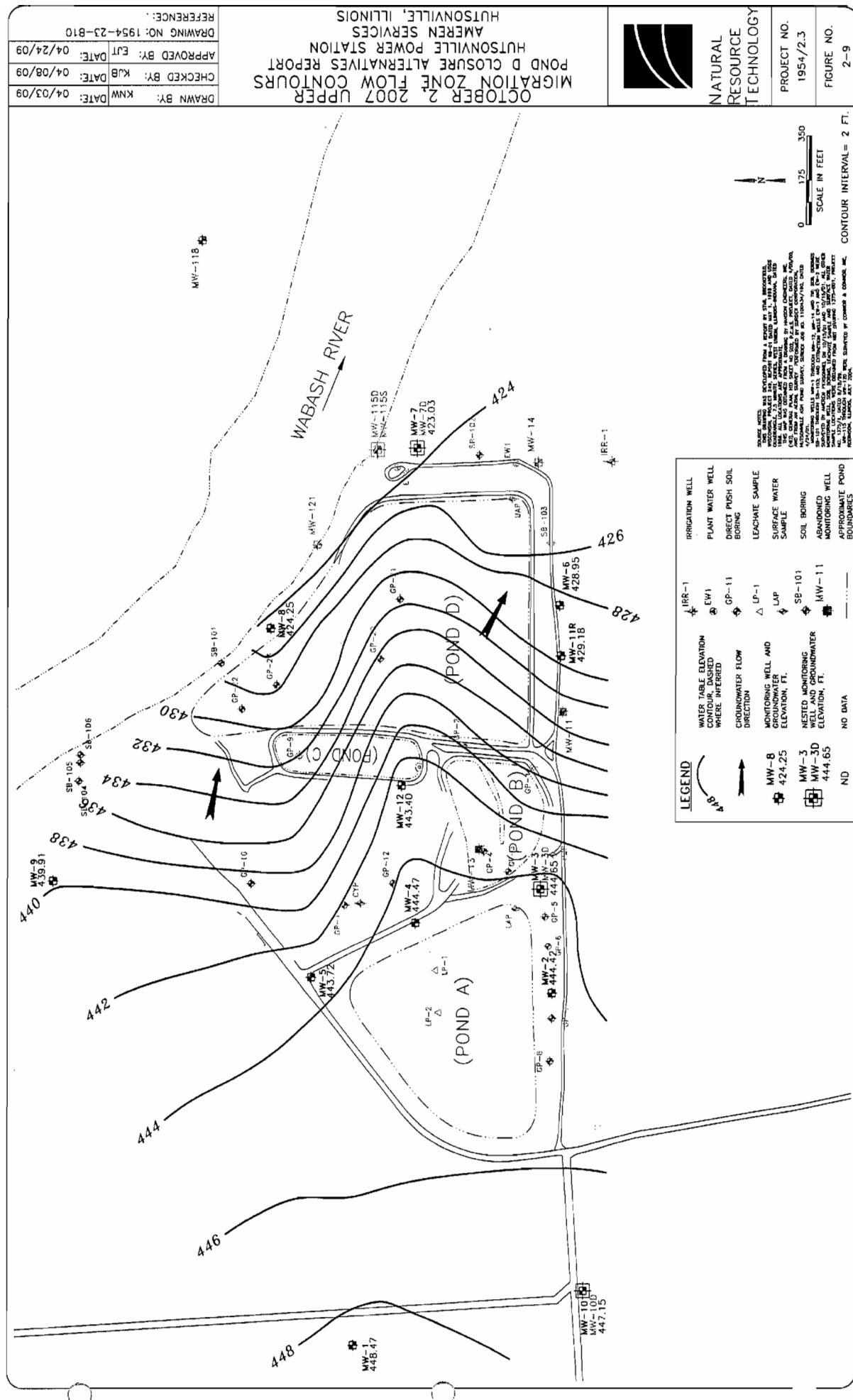


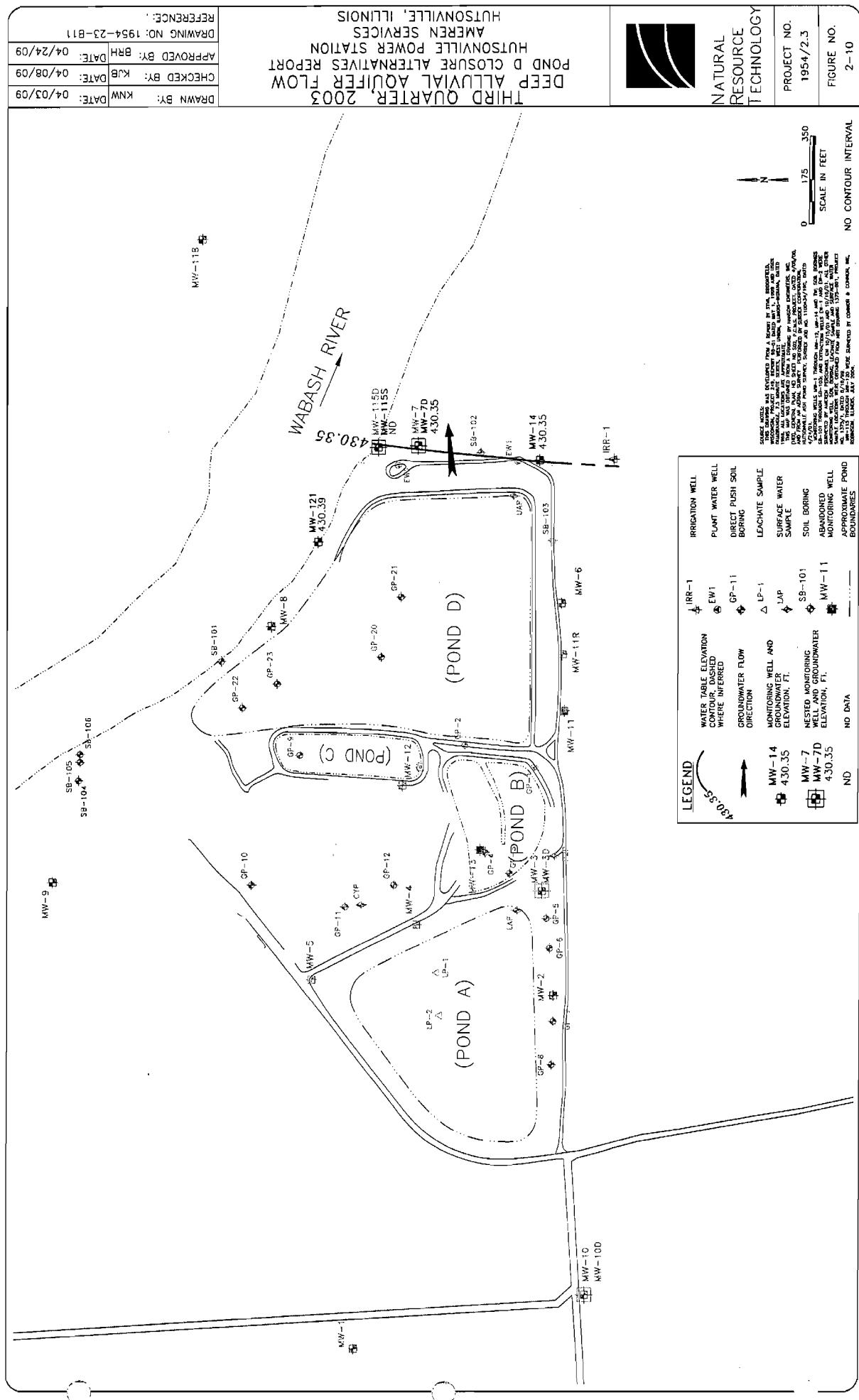


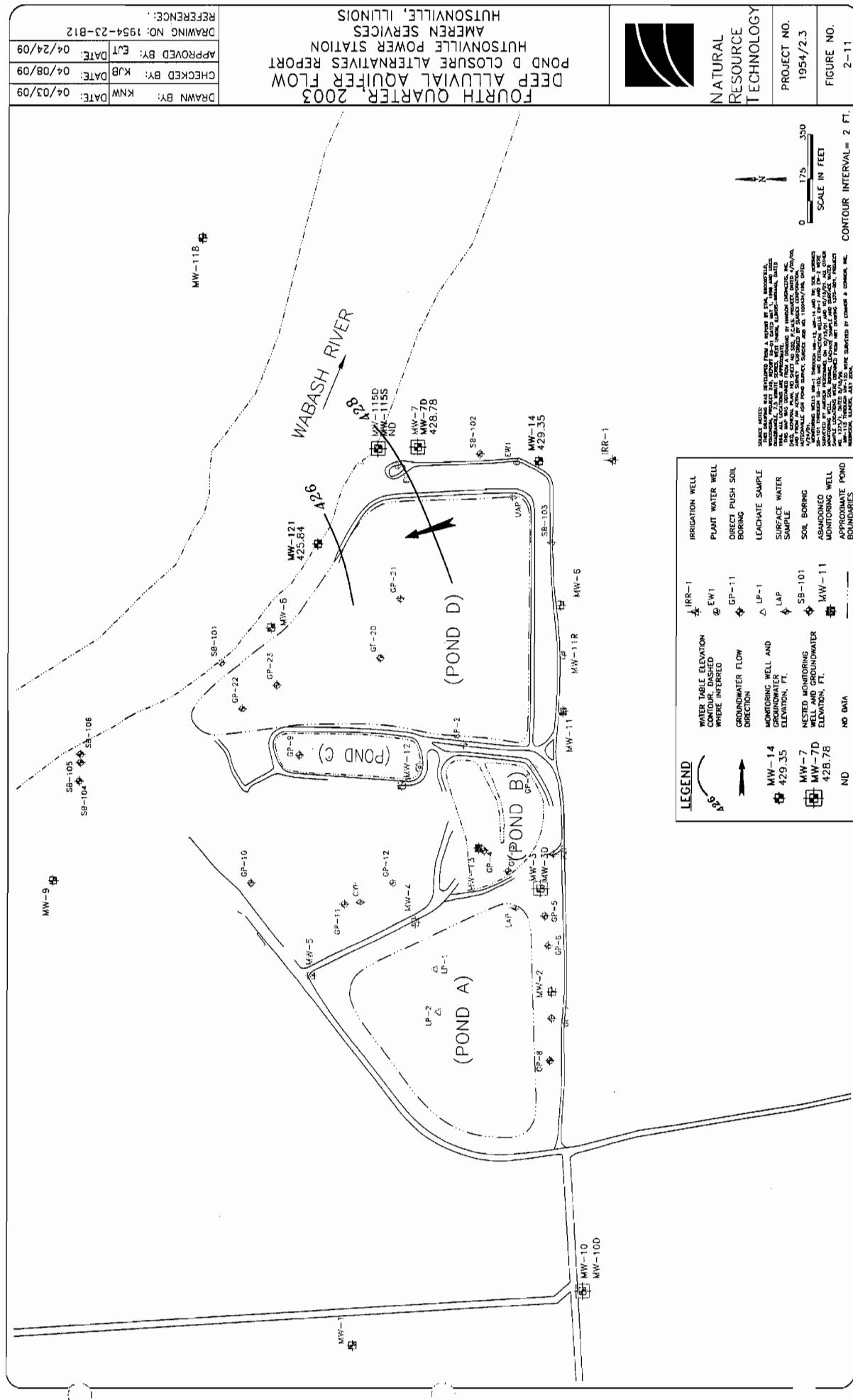


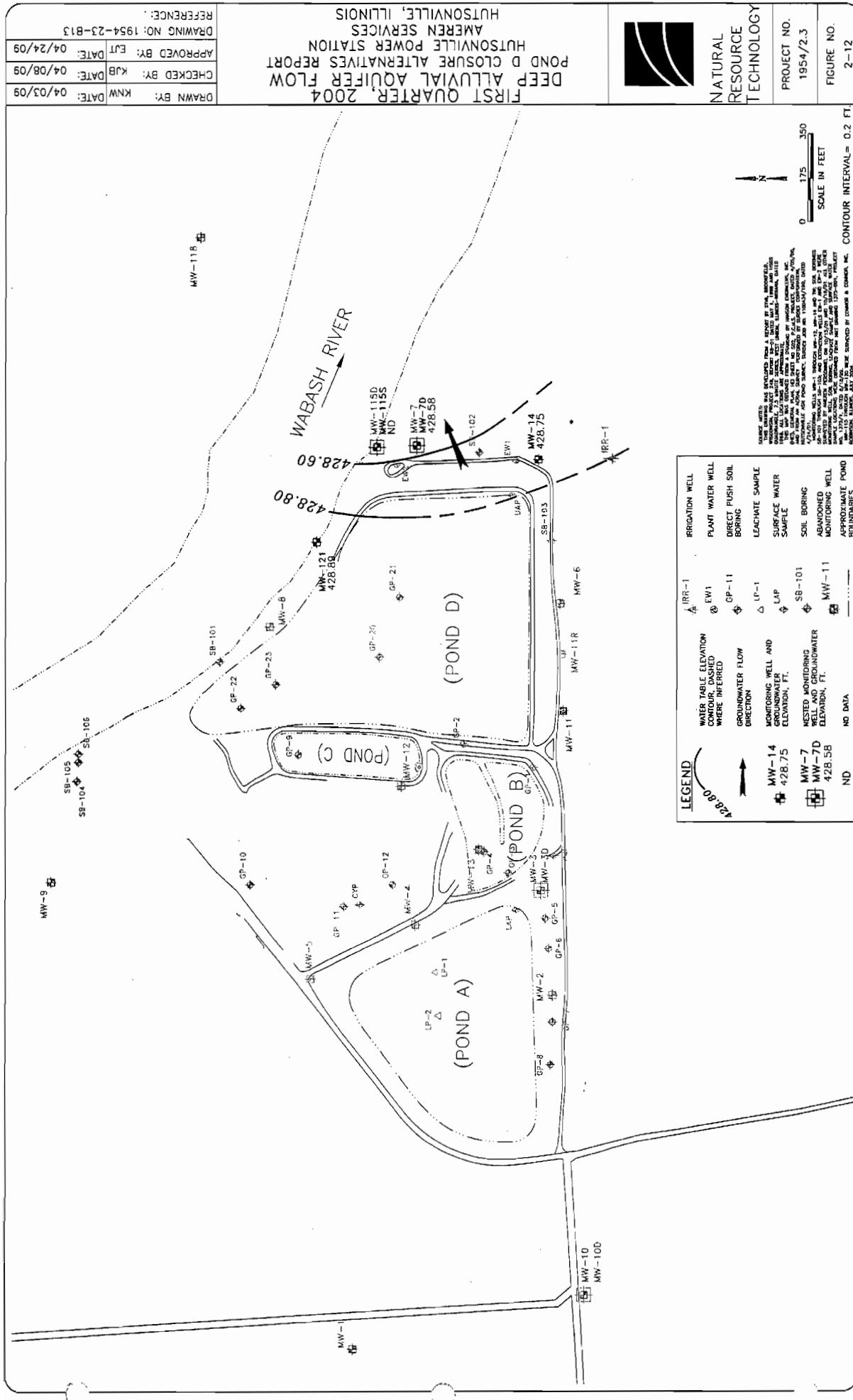


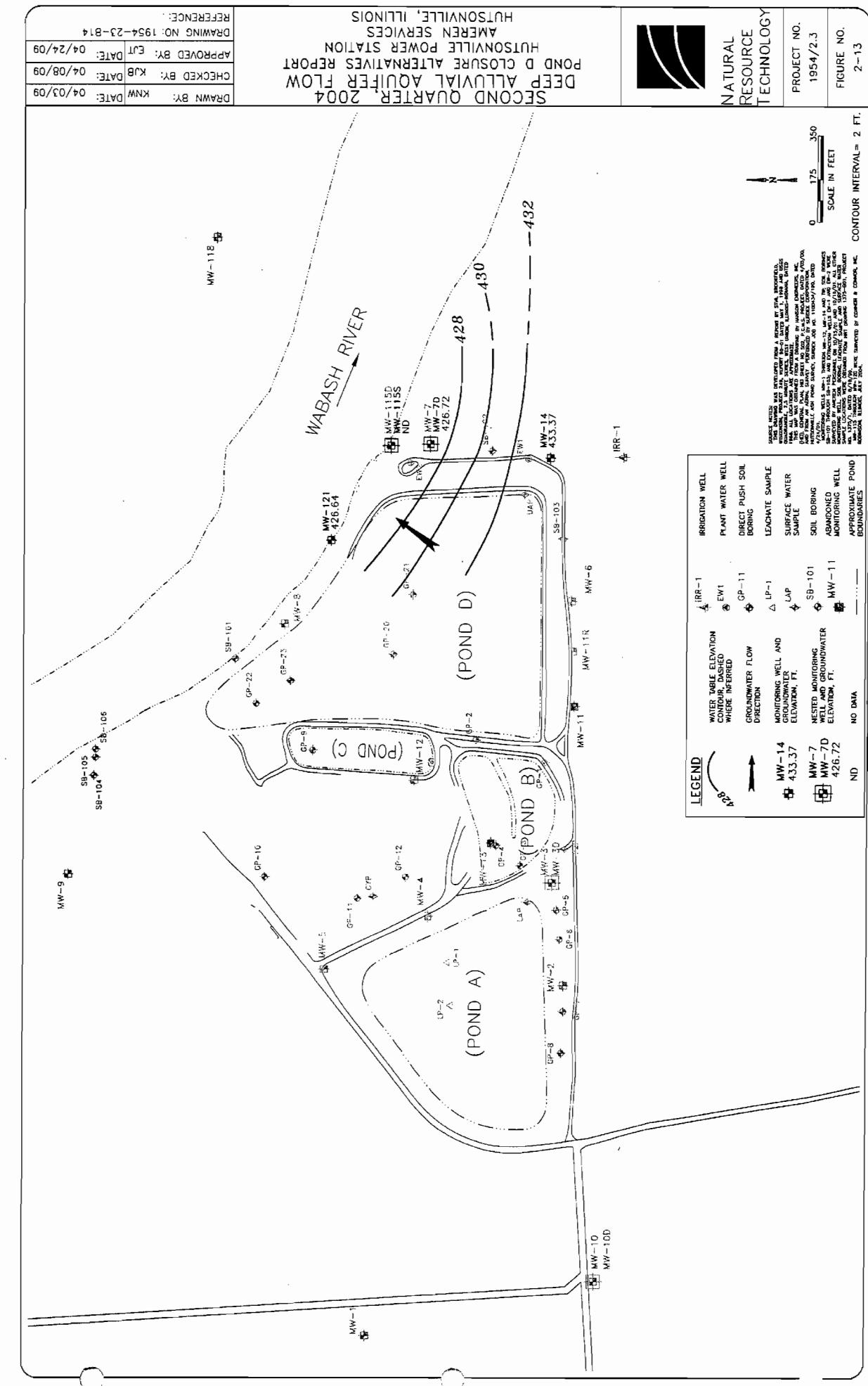


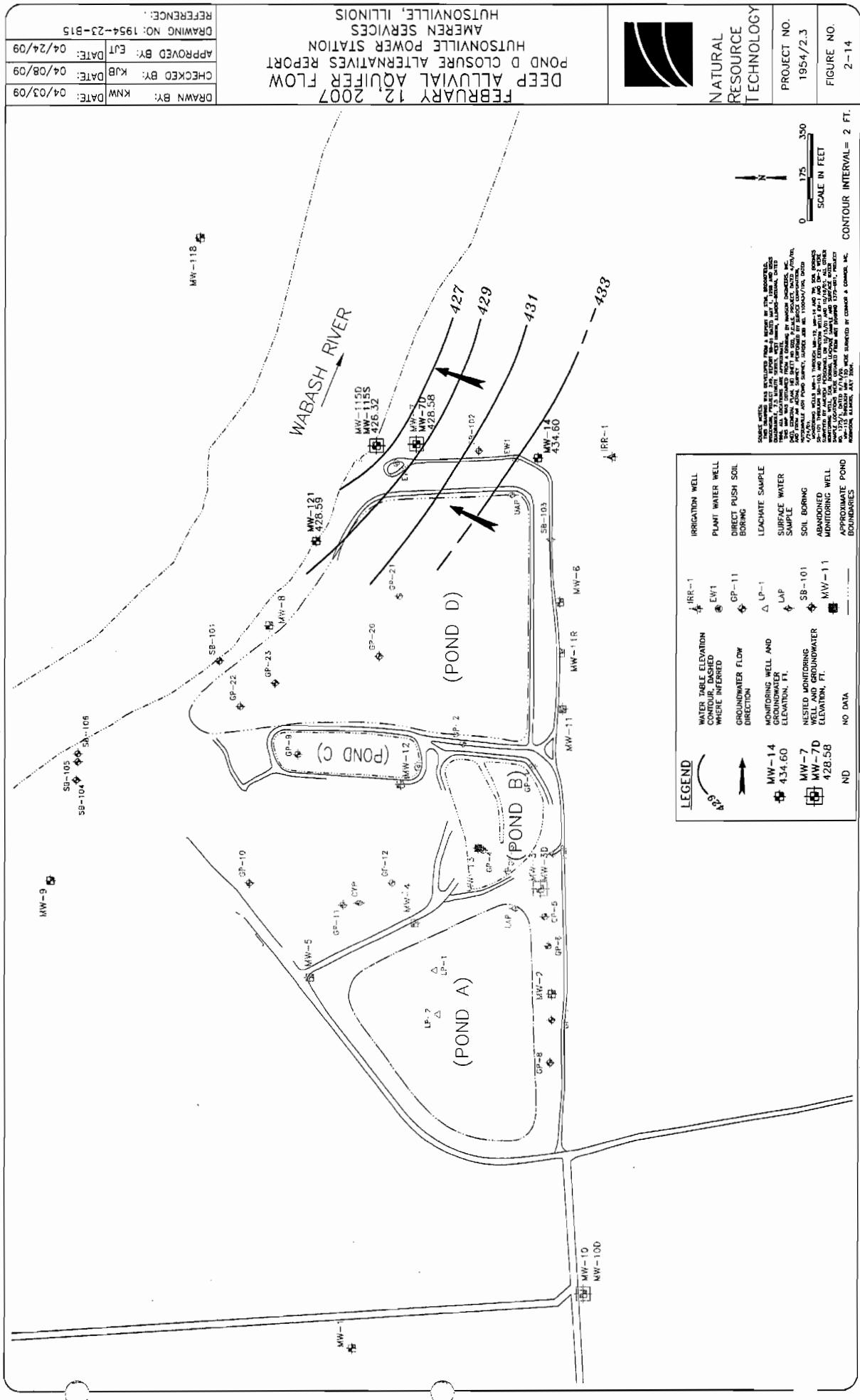


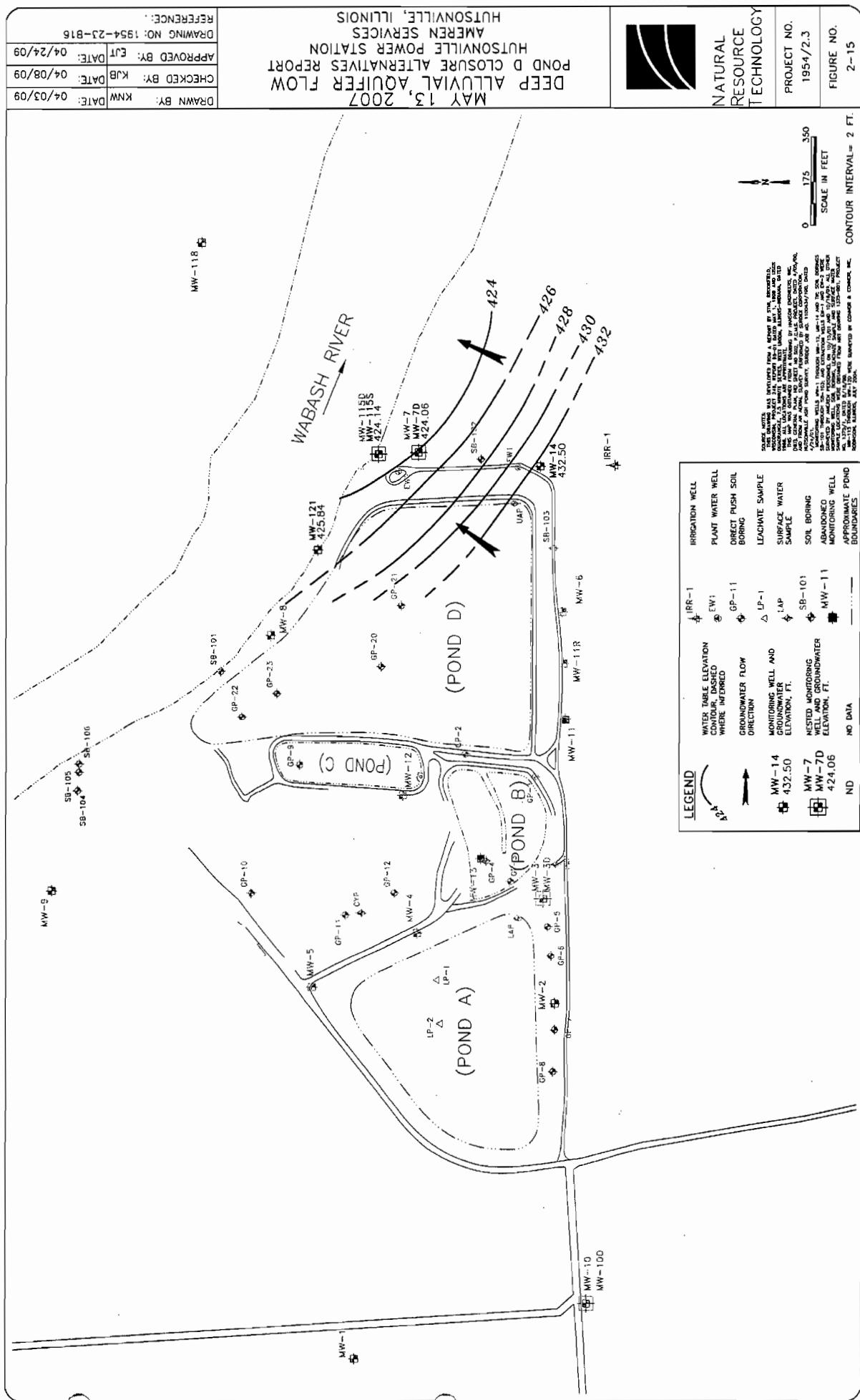












NATURAL
RESOURCE
TECHNOLOGY

TSD 000047

DEEP ALLUVIAL AQUIFER FLOW POND D CLOSURE ALTERNATIVES REPORT

JULY 2, 2007

HUTSONVILLE POWER STATION

AMEREN SERVICES

HUTSONVILLE, ILLINOIS

REFERENCE:
DRAWING NO.: 1954-23-B17
APPROVED BY: EJT DATE: 04/08/09
CHECKED BY: KJB DATE: 04/08/09
DRAWN BY: KNW DATE: 04/03/09

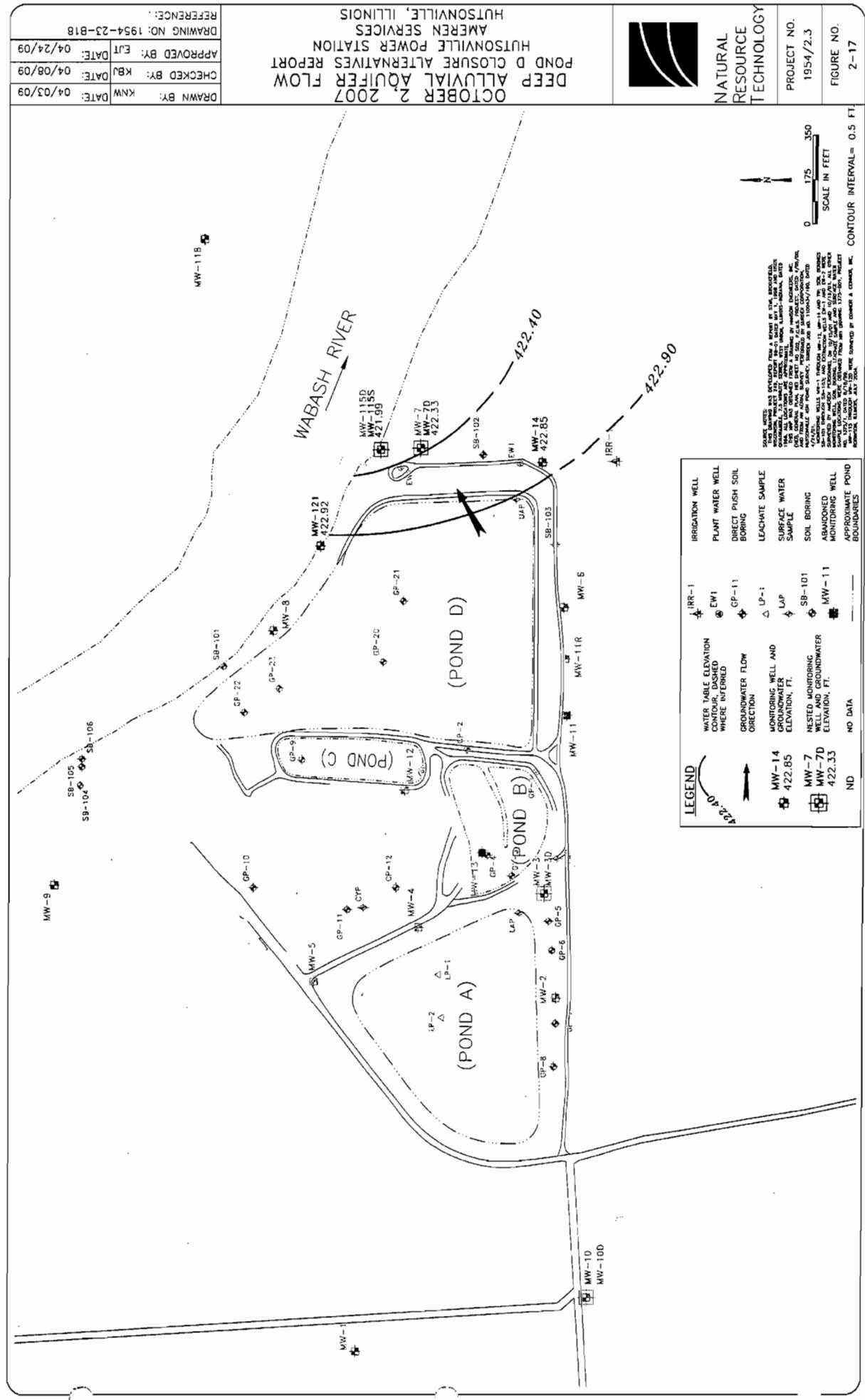
NATIONAL RESOURCE TECHNOLOGY
PROJECT NO.: 1954/2.3
FIGURE NO.: 2-16

LEGEND

- WATER TABLE ELEVATION CONTOUR, DASHED WHERE INFERRED
- IRRIGATION WELL
- PLANT WATER WELL
- DIRECT PUSH SOIL BORING
- GROUNDWATER FLOW DIRECTION
- LEACHATE SAMPLE
- SURFACE WATER SAMPLE
- SOIL BORING
- MONITORING WELL AND GROUNDWATER ELEVATION, FT.
- NESTED MONITORING WELL AND GROUNDWATER ELEVATION, FT.
- IRRIGATION WELL
- ABANDONED MONITORING WELL
- APPROXIMATE POND BOUNDARIES
- NO DATA

SCALE IN FEET
CONTOUR INTERVAL = 0.5 FT.

SCALE IN FEET
0 175 350



Box Whisker Plot - 1 Parameter, Multi Location

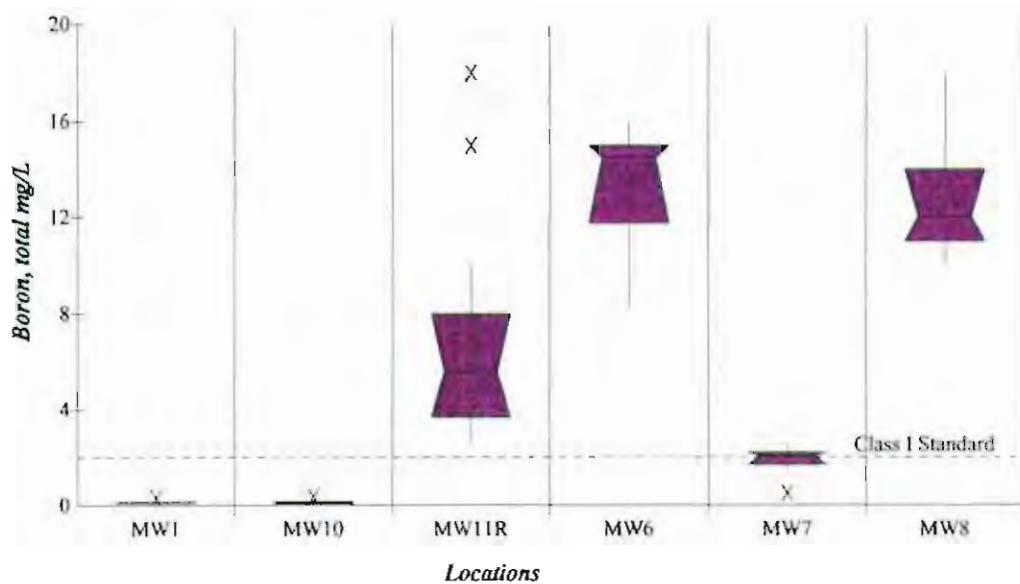


Figure 2-18a. Box-whisker plot showing boron concentrations in the upper migration zone from 2002 through 2008. MW1 and MW10 are upgradient wells.

Box Whisker Plot - 1 Parameter, Multi Location

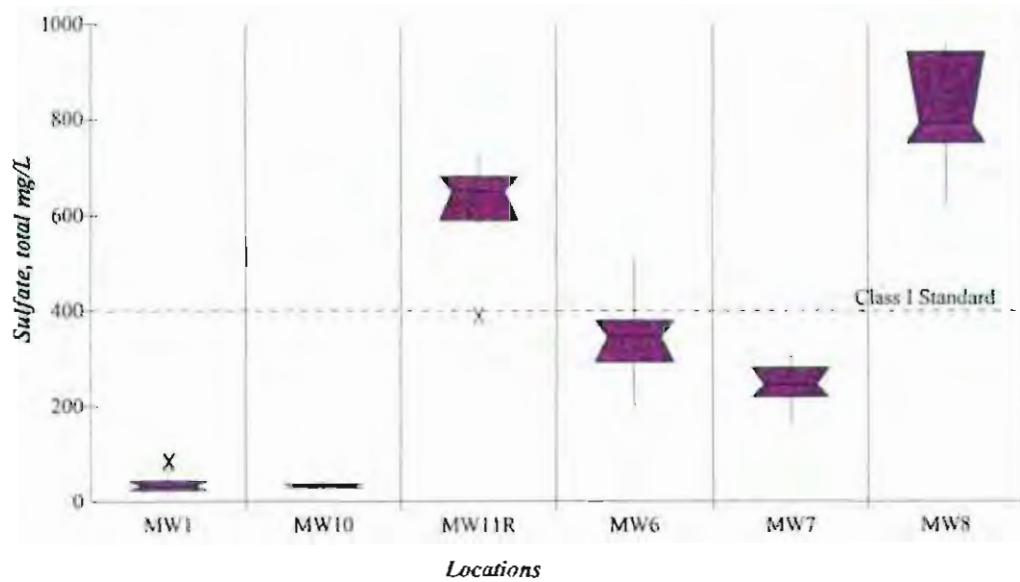


Figure 2-18b. Box-whisker plot showing sulfate concentrations in the upper migration zone from 2002 through 2008. MW1 and MW10 are upgradient wells.

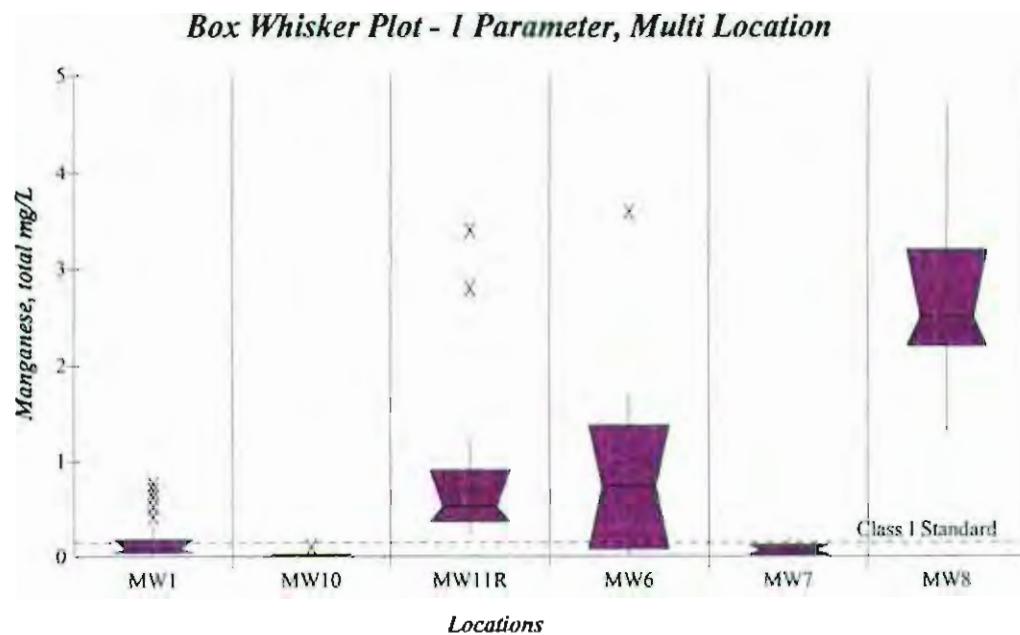


Figure 2-18c. Box-whisker plot showing manganese concentrations in the upper migration zone from 2002 through 2008. MW1 and MW10 are upgradient wells.

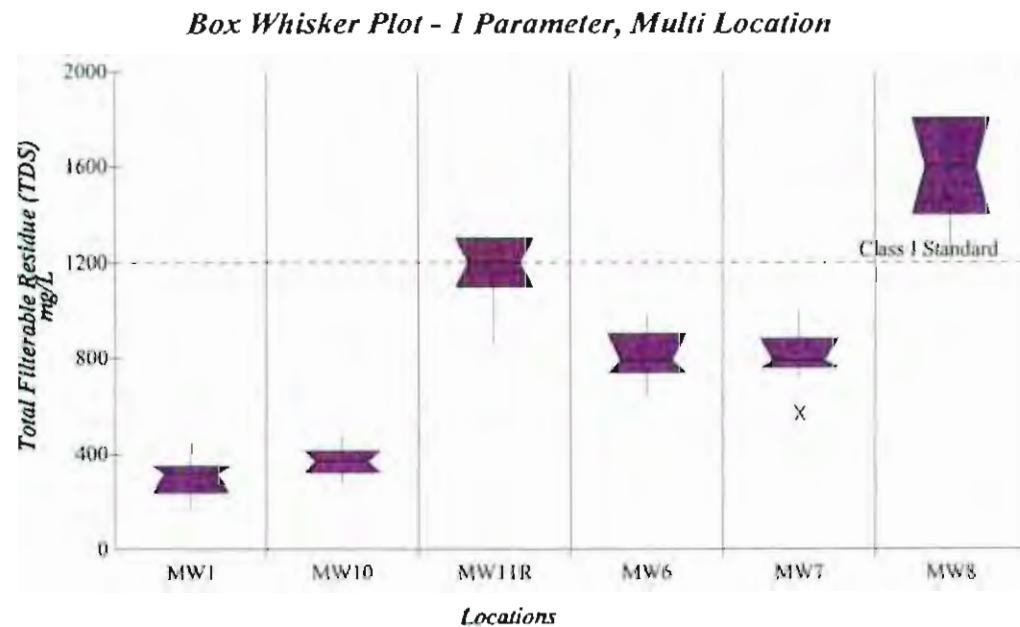


Figure 2-18d. Box-whisker plot showing TDS concentrations in the upper migration zone from 2002 through 2008. MW1 and MW10 are upgradient wells.

Box Whisker Plot - 1 Parameter, Multi Location

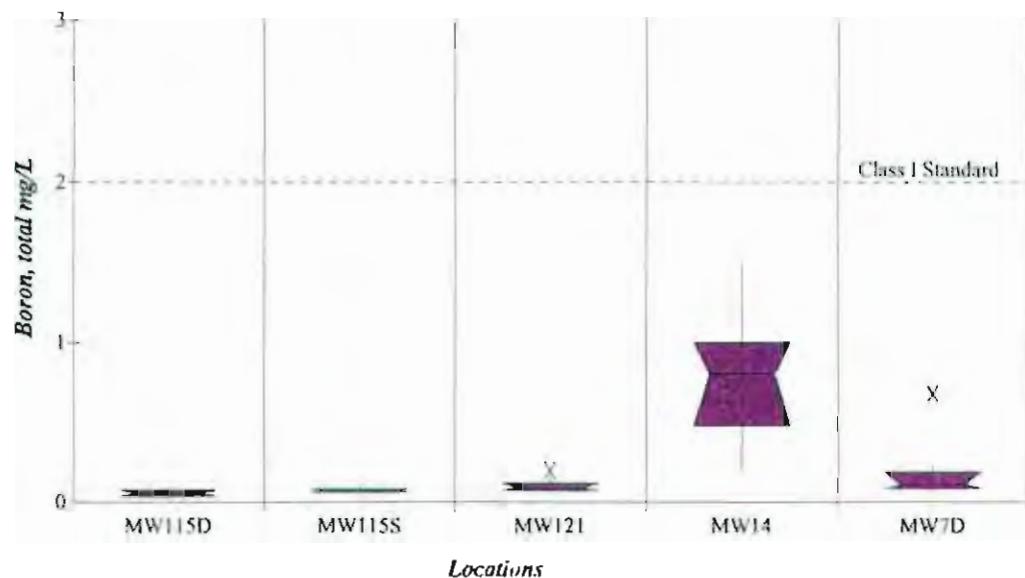


Figure 2-19a. Box-whisker plot showing boron concentrations in the deep alluvial aquifer from 2002 through 2008.

Box Whisker Plot - 1 Parameter, Multi Location

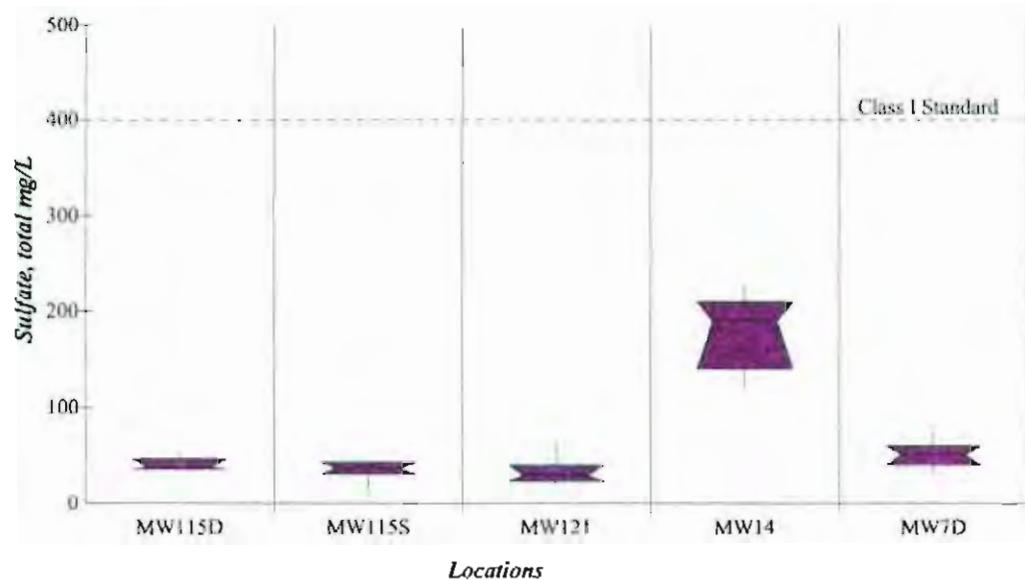


Figure 2-19b. Box-whisker plot showing sulfate concentrations in the deep alluvial aquifer from 2002 through 2008.

Box Whisker Plot - 1 Parameter, Multi Location

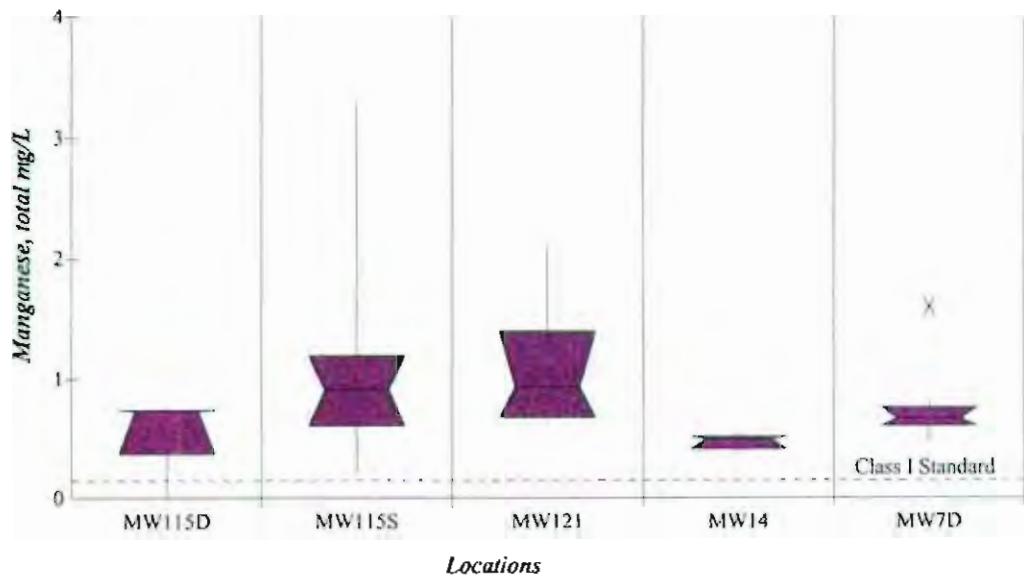


Figure 2-19c. Box-whisker plot showing manganese concentrations in the deep alluvial aquifer from 2002 through 2008.

Box Whisker Plot - 1 Parameter, Multi Location

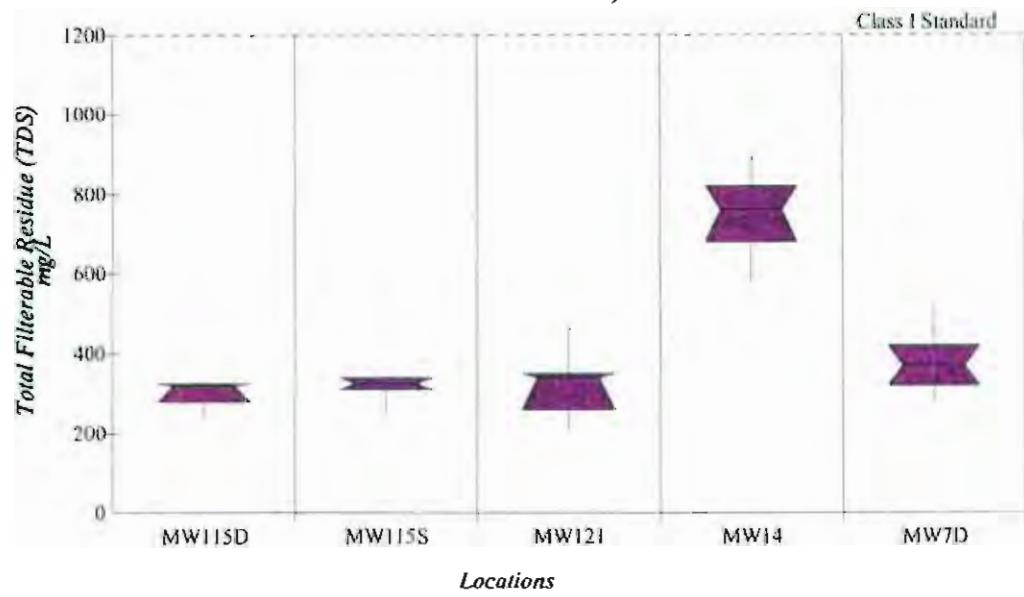
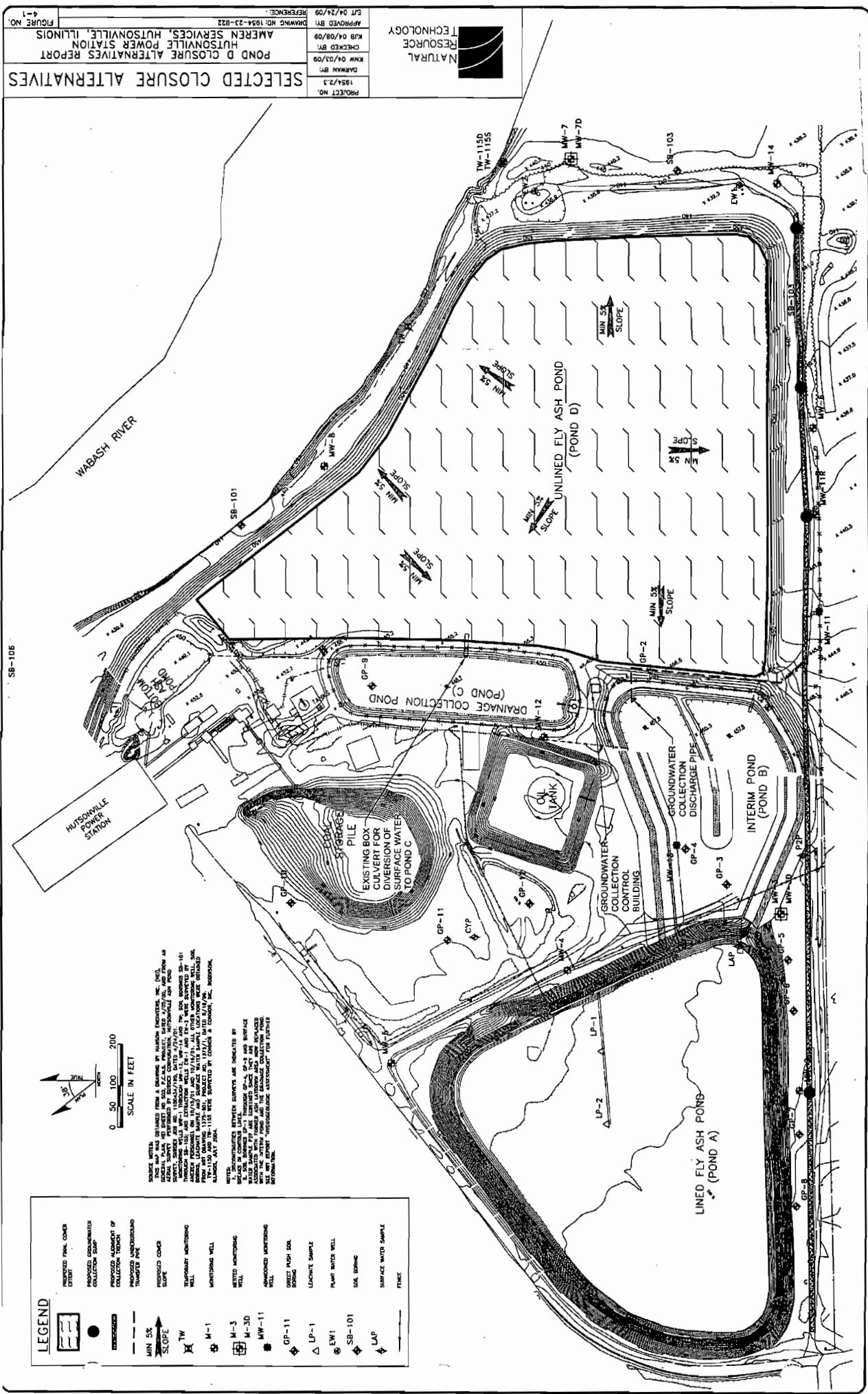


Figure 2-19d. Box-whisker plot showing TDS concentrations in the deep alluvial aquifer from 2002 through 2008.



TABLES

Table 2-1 - Soil Boring and Discrete Groundwater Sampling Data

Pond D Closure Alternatives Report

Hutsonville Power Station

Ameren Services

NRT PROJECT NO.: 1954/2.3

BY: AAS/KJB CHKD BY: RJC/CAR/EJT

DATE: 0-11/01; U-4/09

Location	Northing (ft)	Easting (ft)	Ground Elevation	Target Sample Depth	Depth to Water	Bedrock Surface Depth & Elevation	
			(ft, MSL ²)	(ft, BGS ³)	(ft, BGS)	(ft, BGS)	(ft, MSL)
SB-101	4325	5483	440	no water sample	unknown	>34.5	<405.5
SB-102	2982	5497	440	(17.5-19.5)(26-29)	unknown	>29.0	<410.8
SB-103	2969	5038	442	no water sample	unknown	29.0	412.6
SB-104	— ⁹	— ⁹	— ⁹	no water sample	unknown	11.0	— ⁹
SB-105	— ⁹	— ⁹	— ⁹	no water sample	unknown	9.0	— ⁹
SB-106	— ⁹	— ⁹	— ⁹	no water sample	unknown	>24.5	— ⁹
GP-1	3586	4366	460	17 ³	14	17.3	442.5
GP-2	3753	4610	457	19	9	20.0	437.3
GP-3	3924	4093	459	16	11	16.0	443.3
GP-4	3951	4221	459	16	10	17.0	442.4
GP-5	3918	3859	453	11	6	11.3	441.9
GP-6	3981	3754	453	10	6	10.5	442.5
GP-7	4151	3512	452	10	4	18.0	434.0
GP-8	4263	3380	451	no water sample	4	16.0	435.3
GP-9	4307	4990	453	12	7	21.0	432.4
GP-10	4779	4701	454	12	6	14.3	439.5
GP-11	4534	4399	453	10	5	13.0	439.5
GP-12	4325	4346	451	9	4	9.5	441.3
GP-13	2693	3354	447	9	4	10.0	437.0
GP-14	1105	5752	440	32	10	>40	<400
GP-15	2790	3213	450	12	4	18.0	431.8
GP-16	2887	3065	454	12	4	28.0	425.7
GP-17	2583	3541	446	8	4	12.0	433.6
GP-18	2488	3677	446	12	4	23.8	422.2
GP-19	(6)	(6)	~440	no water sample	10	>32	<410
GP-20	3805	5099	451	21	3	21.0	429.7
GP-21	3594	5239	451	22	3	36.5	414.2
GP-22	4373	5285	459	11 ³	>11.5	11.5	447.2
GP-23	4203	5273	461	22	7	34.0	426.7
LP-1 ⁴	4405	3961	466	7.3	1	--	--
LP-2 ⁴	4502	3815	466	8	1	--	--
MW-11R	3217	4655	441	5.5-15.5	14	16.0	424.9
MW-14	2812	5326	441	(22-24)(36-39) 28-33	19	>39	<401.93
MW-121	3717	5605	438	(25-27)(34-39)	16	>39.5	<398.314

Notes:

1. Four-foot stainless steel screen (for GPs) or polyvinyl chloride (PVC) screen (for LPs).
2. MSL = mean sea level; BGS = below ground surface.
3. Insufficient water sample recovery for laboratory analysis.
4. Temporary 1-inch outside diameter, PVC well point installed in lined ash impoundment.
5. Chips at 3 feet in GP-8 and at 0.5 feet in GP-9.
6. Surveyors could not locate GP-19. It was about 700 feet south of GP-14.
7. Depth to water in wells MW-11R, MW-14 and TW were taken from top of casing.
8. Target sample depths in parentheses for B-103, MW-14 and TW were taken using a hydropunch for deep depths and bailers inside of augers for shallower depths.
9. Location and elevation data not available; these soil boring locations were flooded during the most recent survey on October 15 and 16, 2001.

Pond D Closure Alternatives Report
 Hutzonville Power Station
 Ameren Services

Table 2-2 - Monitoring Well Locations, Elevations, Depth to Bedrock, and Screened Formation

NRT PROJECT NO.: 1954/2.3
 BY: AAS/PAR/KJB CHKD BY: RJC/CARE/JT
 DATE: 01/17/01, U.S./05, U4/09

Well	Date Drilled	Northling (ft) ⁴	Easting (ft) ⁴	Surface Elevation (ft, MSL ²)	TOC ¹ Elevation (ft, MSL)	Total Well Depth (ft, BGS)	Bedrock Elevation (ft, MSL)	Penetration (ft)	Bedrock Formation ³	Screened Formation ³
MW-1	2/14/1984	5606	2964	455.8	459.22	8.9	6.3	449.5	2.7	sand, ss
MW-2	2/10/1984	4087	3594	452.9	455.85	18.1	>21	...	0	s&g
MW-3	2/9/1984	3865	3957	453.6	455.15	10.8	10.3	443.3	0.5	s&g
MW-3D	10/6/1998	3860	3952	453.6	455.28	25.1	10.5	443.1	15.0	ss
MW-4	2/13/1984	4351	4164	453.9	457.02	12.3	10.7	443.2	2.5	s&g, ss
MW-5	2/13/1984	4822	4249	452.2	455.02	17.9	17.7	434.5	1.4	s&g, ss
MW-6	2/9/1984	3095	4818	438.9	443.70	11.5	8.5	430.4	3.0	s&g, ss
MW-7	2/8/1984	3166	5675	438.1	442.78	25.1	>25	...	0	si s&g
MW-7D	10/5/1998	3176	5676	437.5	438.68	44.3	>44	...	0	si s&g
MW-8	2/7/1984	4081	5469	440.0	443.97	22.5	>21.5	...	0	si sand
MW-9	2/14/1984	5408	5205	451.8	454.78	18.4	16.3	435.5	2.4	si s&g, ss
MW-10	10/7/1998	4730	2560	452.8	454.40	10.7	7.5	445.3	3.5	si s&g, ss
MW-10D	10/7/1998	4729	2565	452.7	454.66	21.3	7.5	445.2	14.0	ss
MW-11R	10/3/2001	3217	4655	440.9	443.55	15.5	16.0	424.9	0	s&g
MW-14	10/3/2001	2812	5326	440.9	443.35	33.0	>39	...	0	s&g
MW-115D	5/1/2004	898053	1176882	438.4	440.80	87.0	90	348.4	15	grave
MW-115S	5/1/2004	898047	1176886	438.4	440.89	35.0	90	348.4	0	s&g
MW-121	10/2/2001	3717	5605	437.8	440.59	39.0	>39.5	...	0	s&g

Notes:

- TOC = top of casing
- B GS = below ground surface; MSL = mean sea level.
- s&g = sand and gravel, si = silty, ss = sandstone, cl=clayey.
- Location coordinates for wells installed through 2001 based on plant coordinate system. Coordinates for wells installed in 2004
- Does not include temporary and abandoned wells.
 are state plane.
 -: not determined

TSD 000056

Table 2-3 - Monitoring Well Completion Details
 Pond D Closure Alternatives Report
 Husonville Power Station
 Ameren Services

NRT PROJECT NO.: 194/D.3
 BY: AAS/PAR/KJB CHKD BY: RJC/CAR/EJT
 DATE: 0-11/01, U-205, U-409

Well	Screen Top Depth (ft, BGS ¹)	Screen Bottom Elevation (ft)	Screen Length (ft)	Casing/Screen Type	Filter Pack Elevation ² (ft)	Fine Sand Thickness ³ (ft)	Bentonite Chip Thickness ⁴ (ft)	Annular Seal Thickness ⁵ (ft)	Concrete Collar Thickness ⁶ (ft)	PVC Casing (ft, AGS ¹)	Gallons Water Purged ^{3,6} (ft, TOC ¹)	Depth to Water ⁷ (ft, TOC ¹)	Water Level Elevation ⁷ (ft)
MW-1	4.0	455.3	450.32	5.0	2" I.D. PVC	447.4-453.5	-	-	1.5	1.5	3.4	7.43	451.79
MW-2	5.0	450.8	437.75	13.0	2" I.D. PVC	431.8-449.3	-	-	2	2	3.0	-	8.67
MW-3	4.4	449.4	444.35	5.0	2" I.D. PVC	442.7-448.1	-	-	2	2	1.5	-	7.64
MW-3D	18.4	435.2	430.18	5.0	2" I.D. PVC	428.2-436.7	1	1	14	3	1.7	20	7.91
MW-4	5.0	452.2	444.72	7.5	2" I.D. PVC	441.0-450.4	-	-	2	2	3.1	-	9.72
MW-5	5.0	450.1	437.12	13.0	2" I.D. PVC	433.1-448.3	-	-	2	2	2.8	-	8.46
MW-6	5.0	438.6	432.20	6.4	2" I.D. PVC	427.5-434.9	-	-	2	2	4.8	-	10.83
MW-7	15.0	427.7	417.68	10.0	2" I.D. PVC	412.9-423.9	-	-	2	2	4.7	-	10.71
MW-7D	38.2	399.4	394.38	5.0	2" I.D. PVC	382.5-402.5	3	-	32	3	1.1	27	10.81
MW-8	16.5	426.5	421.47	5.0	2" I.D. PVC	417.9-423.9	-	-	2	2	4.0	-	16.05
MW-9	8.5	446.4	436.38	10.0	2" I.D. PVC	433.2-444.0	-	-	2	2	3.0	-	7.59
MW-10	4.1	448.7	443.70	5.0	2" I.D. PVC	441.9-448.9	-	1	4	--	1.6	20	3.10
MW-10D	14.3	438.4	433.36	5.0	2" I.D. PVC	431.4-438.9	1	1	14	--	2.0	12	3.68
MW-11R	2.8	438.1	428.05	10.0	2" I.D. PVC	424.9-436.4	1	--	4	--	2.7	120	13.55
MW-14	25.5	415.4	410.35	5.0	2" I.D. PVC	401.9-414.9	2	--	24	--	2.4	150	18.23
MW-115D	82	356.4	351.40	5.0	2" I.D. PVC	350.4-357.4	1	3.0	28	--	2.4	135	15.48
MW-115S	30	408.4	403.40	5.0	2" I.D. PVC	402.4-409.4	1	--	80	--	2.5	40	15.55
MW-121	31.2	406.6	401.59	5.0	2" I.D. PVC	387.8-405.8	2	--	30	--	2.8	120	16.30

Notes:

- TOC = top of well casing; BGS = below ground surface; AGS = above ground surface.
- All elevations have been adjusted to match information collected during October 2001 survey of the monitoring wells.
- Data on fine sand thickness, bentonite chip thickness, and gallons of water purged were only available for wells installed since 1998.
- Annular seal thickness includes bentonite/cement grout and bentonite pellets/chips.
- Concrete collar was not installed at shallow 1998 wells and all wells installed in 2001 in order to maximize annular seal. Concrete collars were also not installed around 2004 wells due to their anticipated abandonment within approximately 18 months.
- Volume removed during well development.
- Depth to groundwater measured on 11/12/98 except as follows: 10/3/01 for wells MW-11R, MW-14 and TW; 9/14/04 for the TW-100 series wells.
- Does not include temporary and abandoned wells.
- : Not present or unknown.

TSD 000057

Table 2-4 - Monitoring Well Slug Test Results

Pond D Closure Alternatives Report
Hutsonville Power Station
Ameren Services

NRT PROJECT NO.: 1954/2.3
BY: AAS/ PAR/ KJB **CHKD BY:** RJC/ CAR/ EJT
DATE: 0-11/01, U-5/05, U-4/09

Well	Hydraulic Conductivity (ft/min)	Hydraulic Conductivity (cm/s)	Geologic Unit
MW-1 ¹	8.0E-05	4.1E-05	Sand & Sandstone
MW-3 ¹	5.2E-02	2.7E-02	Silty Sand & Gravel
MW-3D ¹	1.1E-03	5.4E-04	Sandstone
MW-5 ¹	1.6E-02	8.0E-03	Silty Sand & Gravel
MW-6 ¹	6.3E-02	3.2E-02	Clayey Gravel, Silty Sand, Sandstone
MW-7 ¹	5.1E-04	2.6E-04	Sandy Silt, Sand & Gravel
MW-7D ¹	9.5E-02	4.8E-02	Silty Sand & Gravel
MW-9 ¹	1.6E-03	8.3E-04	Silt, Silty Sand, Sandstone
MW-10 ¹	1.2E-03	6.2E-04	Silty Sand, Sandstone
MW-10D ¹	7.9E-04	4.0E-04	Sandstone
MW-12 ¹	1.2E-01	6.2E-02	Sand
MW-13 ^{1,2}	3.5E-02	1.8E-02	Clayey Sand & Gravel
MW-121 ¹	4.7E-02	2.4E-02	Sand
MW-115D ¹	2.3E-02	1.2E-02	Gravel with Sand
MW-115S ³	1.8E-01	9.3E-02	Gravel to Sand
TW-116 ¹	9.0E-04	4.6E-04	Clayey Sand & Gravel
TW-117 ¹	1.3E-02	6.7E-03	Sand
TW-118 ³	3.2E-01	1.6E-01	Sand
TW-119 ¹	4.4E-03	2.2E-03	Sand

Notes:

1. Bouwer and Rice (1976) analysis method.
2. Slug test data for monitoring well MW-13 provided for reference. MW-13 has been abandoned.
3. Butler (1998) analysis method.

TSD 000058

Table 2-5 - Monitoring Well Programs, Monitored Aquifers, and Positions Relative to Pond D

Pond D Closure Alternatives Report
 Hutsonville Power Station
 Ameren Services

NRT PROJECT NO.: 1954/7.3
 BY: BRH CHKD BY: EJT
 DATE: 0-4/09

Well	Monitoring Program	Aquifer	Position Relative to Pond D
MW-1	Ponds A and D	Upper Migration Zone	Upgradient
MW-2	Pond A	Upper Migration Zone	Upgradient
MW-3	Pond A	Upper Migration Zone	Upgradient
MW-3D	none	Upper Migration Zone	Upgradient
MW-4	Pond A	Upper Migration Zone	Upgradient
MW-5	Pond A	Upper Migration Zone	Upgradient
MW-6	Pond D	Upper Migration Zone	Downgradient
MW-7	Pond D	Upper Migration Zone	Downgradient
MW-7D	Pond D	Deep Alluvial Aquifer	Downgradient
MW-8	Pond D	Upper Migration Zone	Downgradient
MW-9	none	Upper Migration Zone	Sidegradient
MW-10	Pond D	Upper Migration Zone	Upgradient
MW-10D	none	Upper Migration Zone	Upgradient
MW-11R	Pond D	Upper Migration Zone	Downgradient
MW-14	Pond D	Deep Alluvial Aquifer	Downgradient
MW-115D	Pond D	Deep Alluvial Aquifer	Downgradient
MW-115S	Pond D	Deep Alluvial Aquifer	Downgradient
MW-121	Pond D	Deep Alluvial Aquifer	Downgradient

TSD 000059

Hutsonville Ash Impoundment
Table 2-6a. Groundwater Monitoring Results: Pond D Upper Migration Zone, 2002-2008

Date Range: 01/01/2002 to 12/31/2008

Well Id	Date Sampled	Lab Id	Limit		B, tot, mg/L	C _a , tot, mg/L	Mn, tot, mg/L	pH (field), std	SO4, tot, mg/L	TDS, mg/L
			State Std	2.000	0.150	6.500 - 9.000	400.000	1,200,000		
MW1	01/14/2002		0.170	58.000	[0.180]	7.300	57.000	290.000	290.000	
	02/25/2002		0.150	44.000	0.069	7.770	43.000	270.000	270.000	
	03/25/2002		0.150	35.000	0.098		40.000	190.000	190.000	
	04/23/2002		0.150	33.000	0.130	7.430	37.000	220.000	220.000	
	05/23/2002		0.170	42.000	[0.420]	7.380	25.000	240.000	240.000	
	06/27/2002		0.098	74.000	[0.690]	7.450	24.000	290.000	290.000	
	07/30/2002		0.110	96.000	0.091	7.410	30.000	390.000	390.000	
	08/31/2002		0.160	96.000	0.014	7.510	63.000	450.000	450.000	
	09/17/2002	02092695-1	0.150	99.000	0.042	7.530	68.000	440.000	440.000	
	10/17/2002		0.310	160.000	0.019		80.000	450.000	450.000	
	11/21/2002		0.140	90.000	0.150	7.120				
	11/25/2002					7.200	49.000	360.000	360.000	
	12/11/2002	02122282-1	0.180	96.000	[0.270]	7.090	39.000	370.000	370.000	
	01/08/2003	03011887-1	0.140	67.000	0.003	7.190	84.000	300.000	300.000	
	02/05/2003	03021653-1	0.140	76.000	0.053	7.210	87.000	340.000	340.000	
	03/17/2003	03032351-1	0.120	41.000	0.003	7.460	48.000	180.000	180.000	
	04/07/2003	03041847-1	0.140	37.000	0.001	7.850	38.000	210.000	210.000	
	05/05/2003	03051599-1	0.140	40.000	0.014	7.470	37.000	200.000	200.000	
	06/02/2003	03061314-1	0.110	56.000	0.072	7.600	25.000	270.000	270.000	
	07/07/2003	03071766-1	0.092	85.000	[0.240]	7.318	20.000	330.000	330.000	
	08/04/2003	03081508-1	0.110	85.000	0.047	7.500	19.000	320.000	320.000	
	10/06/2003	03101729-1	0.093	80.000	0.070	7.200	17.000	320.000	320.000	
	11/03/2003	03111368-1	0.093	78.000	0.120	7.000	16.000	340.000	340.000	
	12/01/2003	03121269-1	0.160	75.000	0.013	7.100	50.000	370.000	370.000	
	01/05/2004	04011364-1	0.100	60.000	0.041	7.090	40.000	260.000	260.000	
	02/09/2004	04021831-1	0.150	42.000	0.025	7.500	40.000	190.000	190.000	
	03/02/2004	04031476-1	0.110	46.000	0.032	7.400	32.000	240.000	240.000	
	04/04/2004	04041354-1	0.120	40.000	0.044	7.500	35.000	210.000	210.000	
	05/04/2004	04051491-1	0.100	55.000	[0.280]	7.300	15.000	260.000	260.000	
	06/01/2004	04061297-1	0.067	77.000	[0.220]	7.300	15.000	290.000	290.000	

MANAGES

TSD 000060

Hutsonville Ash Impoundment
Table 2-6a. Groundwater Monitoring Results: Pond D Upper Migration Zone, 2002-2008

Date Range: 01/01/2002 to 12/31/2008

MW1	07/12/2004	04072337-1	0.082	85,000	[0.210]	7,200	18,000	3,50,000
	08/02/2004	04081328-1	0.099	86,000	[0.170]	7,200	15,000	33,000
	09/13/2004	04092601-1	0.098	80,000	0.100	7,600	20,000	37,000
	10/04/2004	04101561-1	0.140	85,000	0.047	7,300	18,000	34,000
	11/08/2004	041112264-1	0.110	85,000	0.130	7,200	35,000	36,000
	12/06/2004	04121931-1	0.140	84,000	[0.260]	7,200	51,000	30,000
	01/03/2005	05011545-1	0.170	48,000	[0.180]	7,300	42,000	26,000
	02/23/2005	05022558-1	0.200	38,000	[0.180]	7,220	34,000	200,000
	03/14/2005	05032818-1	0.130	40,000	[0.300]	7,260	26,000	180,000
	04/19/2005	05043119-1	0.140	54,000	[0.200]	7,260	32,000	230,000
	05/04/2005		0.140	56,000	[0.760]	7,080	17,000	210,000
	06/19/2005		0.120	90,000	[0.520]	7,260	26,000	290,000
	07/18/2005		0.130	97,000	[0.210]	6,900	23,000	280,000
	08/08/2005		0.093	86,000	0.046	6,990	25,000	340,000
	09/12/2005		0.140	95,000	[0.230]	6,900	39,000	420,000
	10/04/2005		0.110	[20,000]	0.130	7,010	48,000	300,000
	11/01/2005		0.140	86,000	0.140	6,740	53,000	380,000
	12/05/2005		0.110	84,000	0.016	6,670	32,000	340,000
	01/09/2006		0.100	91,000	0.048	6,570	27,000	340,000
	02/07/2006		0.110	61,000	0.005	6,700	71,000	300,000
	03/06/2006		0.110	66,000	0.008	6,900	80,000	300,000
	04/11/2006		0.160	44,000	0.007	7,500	39,000	190,000
	05/23/2006		0.120	69,000	0.049	7,500	31,000	300,000
	06/12/2006		0.100	88,000	[0.320]	7,150	26,000	350,000
	07/10/2006		0.120	85,000	0.055	7,200	29,000	350,000
	08/07/2006		0.120	88,000	0.052	7,000	31,000	380,000
	09/11/2006		0.100	94,000	0.003	7,000	38,000	380,000
	10/04/2006		0.110	84,000	0.082	6,900	26,000	330,000
	11/06/2006		0.110	91,000	[0.200]	[6,400]	49,000	410,000
	12/05/2006		0.130	65,000	0.120	7,000	44,000	280,000
	01/08/2007						7,000	
	02/12/2007						7,000	
	03/21/2007	07033395-1	0.140	43,000	0.100		29,000	200,000
	04/09/2007		0.140	41,000	[0.170]		26,000	200,000
	05/06/2007		0.130	42,000	[0.420]		21,000	220,000
	06/11/2007		0.098	89,000	[0.620]	6,800	9,900	350,000
	07/09/2007		0.100	77,000	[0.280]	7,000	18,000	290,000

MANAGES

TSD 000061

Hutsonville Ash Impoundment
Table 2-6a. Groundwater Monitoring Results: Pond D Upper Migration Zone, 2002-2008

Date Range: 01/01/2002 to 12/31/2008

MW1	08/08/2007 09/10/2007 10/15/2007	0.096 0.100 0.150 0.120	88.000 95.000 94.000 96.000	0.140 0.002 0.084 0.032	7.100 6.900 7.000 6.700	14,000 17,000 33,000 38,000	340,000 370,000 360,000 350,000
	11/05/2007 12/10/2007	07103111-1 07122239-1	96.000 73.000	0.042 0.050	6.800 7.100	29,000 54,000	380,000 330,000
01/07/2008	08011897-1	0.092	53,000	0.048	[6,100]	39,000	230,000
02/18/2008	08022938-1	0.098	47,000	0.046	6,800	33,000	240,000
03/10/2008	08032268-1	0.093	33,000	0.007	7,000	22,000	170,000
04/07/2008	08042166-1	0.120	43,000	0.130	6,800	25,000	200,000
05/12/2008	08052529-1	0.160	37,000	0.025	6,900	16,000	160,000
06/10/2008	08062618-1	0.180	73,000	[0.180]	6,700	26,000	320,000
07/08/2008	08072242-1	0.150	92,000	[0.220]	6,800	21,000	340,000
08/11/2008	08082425-1	0.130	82,000	0.025	7,100	25,000	330,000
10/06/2008	08101954-1	0.110	93,000	0.110	7,000	33,000	340,000
11/04/2008	08111694-1	0.110	91,000	0.044	[6,100]	45,000	380,000
12/02/2008	08121591-1	0.130	86,000	0.150	43,000	360,000	

Hutsonville Ash Impoundment
Table 2-6a. Groundwater Monitoring Results: Pond D Upper Migration Zone, 2002-2008

Date Range: 01/01/2002 to 12/31/2008

Well Id	Date Sampled	Lab Id	Limit	B, tot, mg/L	Ca, tot, mg/L	Mn, tot, mg/L	pH (field), std	SO4, tot, mg/L	TDS, mg/L
				State Std	2.000	0.150	6.500 - 9.000	400.000	1,200.000
M/W10	01/14/2002			0.160	94.000	0.017		32.000	370.000
	06/30/2002			0.098	90.000	0.100	7.110	31.000	370.000
	09/17/2002	02092695-7		0.200	86.000	0.004	7.060	38.000	380.000
	12/19/2002	02123013-5		0.079	76.000	0.001	7.210	38.000	330.000
	02/05/2003	03021653-8		0.076	80.000	0.002	7.200	38.000	310.000
	05/05/2003	03051599-6		0.092	89.000	0.022	7.200	44.000	270.000
	07/07/2003	03071766-7		0.120	100.000	0.019	7.000	36.000	340.000
	10/13/2003	03102279-5		0.064	100.000	0.008	7.100	31.000	450.000
	03/02/2004	04031476-6		0.086	100.000	0.029	7.100	29.000	410.000
	04/04/2004	04041382-3		0.130	120.000	0.045	7.000	29.000	390.000
	08/03/2004	04081328-10		0.160	110.000	0.040	7.100	31.000	450.000
	10/04/2004	04101561-10		0.150	93.000	0.008	7.100	33.000	470.000
	03/14/2005	05032818-9		0.068	130.000	0.024	6.950	32.000	400.000
	04/19/2005	05043119-7							430.000
	03/06/2006								6.800
	06/20/2006								7.070
	07/10/2006								7.000
	11/06/2006						[6.400]		
	03/21/2007	07033395-6		0.085	86.000	0.002		32.000	330.000
	06/11/2007								6.900
	08/08/2007								7.000
	11/12/2007								7.100
	03/11/2008	08032485-1		0.059	80.000	0.002	[5.900]		300.000
	06/23/2008	08064092-2		0.140	85.000	0.014		23.000	
	09/15/2008							26.000	310.000
	10/21/2008	08103771-1		0.350	95.000	0.007			24.000
									350.000

Hutsonville Ash Impoundment
Table 2-6a. Groundwater Monitoring Results: Pond D Upper Migration Zone, 2002-2008

Date Range: 01/01/2002 to 12/31/2008

Well Id	Date Sampled	Lab Id	Limit	B, tot, mg/L	C _a , tot, mg/L	Mn, tot, mg/L	pH (field), std	SO4, tot, mg/L	TDS, mg/L
				State Std	2.000	0.150	6.500 - 9.000	400.000	1,200.000
MW11R	01/14/2002		[3.700]	240.000	[2.800]		[730.000]	[1,300.000]	
	06/30/2002		[6.600]	150.000	[3.400]		7.150	390.000	1,200.000
	09/19/2002	02092792-4	[7.000]	250.000	[0.880]		7.090	[690.000]	850.000
	12/13/2002	02122525-3	[5.600]	220.000	[0.380]		7.000	[590.000]	[1,300.000]
	03/18/2003	03032481-4	[5.800]	220.000	[0.590]		7.200	[590.000]	1,100.000
	05/12/2003	03052186-4	[2.600]	220.000	[0.520]		7.200	[650.000]	1,100.000
	08/04/2003	03081508-8	[2.800]	220.000	[0.700]		6.700	[650.000]	1,200.000
	10/13/2003	03102279-6	[2.800]	240.000	[1.200]		[6.000]	[720.000]	1,200.000
	02/23/2004	04022960-4	[4.900]	240.000	[0.270]		6.800	[650.000]	[1,300.000]
	04/04/2004	04041354-8	[5.800]	260.000	[0.320]		[670.000]	[1,300.000]	
	07/12/2004	04072337-9	[8.000]	230.000	[0.240]		6.800	[650.000]	[1,300.000]
	11/08/2004	04112264-8	[4.300]	290.000	[0.850]		6.700	[680.000]	[1,300.000]
	01/04/2005	05011545-9					[6.300]		
	03/13/2006						6.830		
	06/20/2006						6.800		
	08/07/2006						6.800		
	10/25/2006						6.800		
	02/27/2007						[6.100]		
	06/20/2007						6.700		
	07/11/2007						6.600		
	11/12/2007						6.900		
	03/11/2008	08032485-4	[18.000]	240.000	[0.370]		[580.000]		1,100.000
	03/12/2008						6.900		
	06/23/2008	08064092-4	[15.000]	260.000	[0.910]		6.700		
	09/08/2008	08092188-6	[10.000]	140.000	[0.450]		[590.000]	[640.000]	1,200.000
	09/15/2008						6.600		[1,300.000]
	10/14/2008						7.000		

Hutsonville Ash Impoundment
Table 2-6a. Groundwater Monitoring Results: Pond D Upper Migration Zone, 2002-2008

Date Range: 01/01/2002 to 12/31/2008

Well Id	Date Sampled	Lab Id	Limit		B, tot, mg/L	C _a , tot, mg/L	Mn, tot, mg/L	pH (field), std	SO4, tot, mg/L	TDS, mg/L
			State Std	2.000	0.150	6,500 - 9,000	400,000	1,200,000		
MW6	01/14/2002		[15.000]	130,000	[1.400]			270,000	740,000	
	06/30/2002		[15.000]	130,000	[3,600]			200,000	690,000	
	09/19/2002	02092792-1	[16.000]	130,000	[1,300]			6,910	240,000	
	12/13/2002	02122525-1	[11.000]	170,000	0,007			6,700	[450,000]	
	03/18/2003	03032481-3	[8,200]	150,000	0,004			7,000	360,000	
	05/12/2003	030521186-3	[13,000]	150,000	0,080			7,000	330,000	
	08/04/2003	03081508-6	[15,000]	140,000	[0,290]			6,900	300,000	
	10/13/2003	03102279-1	[14,000]	150,000	[0,880]			7,400	310,000	
	02/23/2004	04022960-7	[11,000]	140,000	[0,890]			6,900	310,000	
	04/04/2004	04041354-6	[12,000]	160,000	[1,700]			360,000	900,000	
	07/12/2004	04072337-7	[14,000]	140,000	[0,590]			6,700	380,000	
	11/08/2004	04112264-6	[15,000]	140,000	[0,970]			7,200	380,000	
	01/04/2005	05011545-7						6,800		
	03/13/2006							6,840		
	06/20/2006							6,700		
	08/07/2006							6,500		
	10/25/2006							6,500		
	02/27/2007							6,600		
	06/20/2007							6,900		
	07/11/2007							6,800		
	11/12/2007							[6,200]		
	03/11/2008	08032485-3	[15.000]	190,000	0,083			[460,000]	930,000	
	06/23/2008	08064092-1	[16,000]	200,000	[0,420]			6,800	[510,000]	
	09/15/2008							6,700	980,000	
	10/14/2008									

Hutsonville Ash Impoundment
Table 2-6a. Groundwater Monitoring Results: Pond D Upper Migration Zone, 2002-2008

Date Range: 01/01/2002 to 12/31/2008

Well Id	Date Sampled	Lab Id	Limit		B, tot, mg/L	C _R , tot, mg/L	Mn, tot, mg/L	pH (field), std	SO ₄ , tot, mg/L	TDS, mg/L
			State Std	2.000	0.150	6.500 - 9.000	400.000	1,200.000		
MW7	01/15/2002		[2.300]	150.000	0.100			220.000	770.000	770.000
	07/01/2002		[2.200]	180.000	0.052			240.000	760.000	720.000
	09/18/2002	02092792-7	[2.500]	180.000	[0.220]			250.000	790.000	790.000
	12/19/2002	02123013-2	0.500	130.000	0.020			160.000	570.000	570.000
	03/19/2003	03032570-1	1.800	150.000	0.024			220.000	790.000	790.000
	06/02/2003	03061314-6	[2.100]	170.000	0.018			220.000	790.000	790.000
	08/11/2003	03082176-1	[2.200]	180.000	0.120			240.000	820.000	820.000
	10/13/2003	03102279-2	[2.100]	190.000	0.022			280.000	880.000	880.000
	02/23/2004	04022960-5	2.000	180.000	0.051			310.000	970.000	970.000
	04/19/2004	04042676-1	2.000	200.000	[0.160]			310.000	950.000	950.000
	08/02/2004	04081328-6	[2.600]	210.000	0.120			300.000	1,000.000	1,000.000
	10/04/2004	04101561-7	1.400	150.000	0.012			220.000	730.000	730.000
	03/15/2005	05032818-6			[6.400]					
	03/27/2006				6.680					
	06/26/2006				6.700					
	10/09/2006				6.700					
	02/19/2007				6.700					
	06/20/2007				6.600					
	09/10/2007				7.000					
	10/22/2007				7.100					
	06/29/2008	08071070-1	1.700	190.000	0.095			6.900	250.000	800.000
	09/15/2008				6.800					
	10/08/2008	08102352-1	1.700	200.000	0.078			6.700	280.000	860.000

Hutsonville Ash Impoundment
Table 2-6a. Groundwater Monitoring Results: Pond D Upper Migration Zone, 2002-2008

Date Range: 01/01/2002 to 12/31/2008

Well Id	Date Sampled	Lab Id	Limit	B, tot, mg/L	Ca, tot, mg/L	Mn, tot, mg/L	pH (field), std	SO4, tot, mg/L	TDS, mg/L
				State Std	2.000	0.150	6.500 - 9.000	400.000	1,200.000
MW8	01/15/2002	[14.000]		330.000	[3.200]			[790.000]	[1,800.000]
	07/01/2002								[1,400.000]
	09/19/2002	02092792-2	[10.000]	320.000	[3.800]		6.920	[790.000]	[1,300.000]
	12/19/2002	02123013-4	[11.000]	320.000	[3.600]		6.970	[740.000]	[1,600.000]
	03/17/2003	03032351-2	[12.000]	390.000	[2.900]		7.000	[960.000]	[1,700.000]
	06/18/2003	03062696-1	[12.000]	360.000	[2.500]		7.400	[940.000]	[1,800.000]
	08/11/2003	03082176-3	[14.000]	360.000	[2.500]		7.093	[960.000]	[1,800.000]
	10/13/2003	03102279-4	[13.000]	370.000	[2.200]		7.100	[920.000]	[1,800.000]
	02/23/2004	04022960-8	[13.000]	340.000	[4.700]		7.000	[820.000]	[1,800.000]
	04/19/2004	04042676-3	[12.000]	310.000	[2.300]		7.000	[870.000]	[1,800.000]
	08/02/2004	04081328-8	[11.000]	300.000	[2.100]		6.900	[800.000]	[1,500.000]
	10/04/2004	04101561-8	[11.000]	200.000	[1.300]		6.900	[620.000]	1,200.000
	03/16/2005	05032818-8	[13.000]	310.000	[2.200]		7.440	[940.000]	[1,600.000]
	03/27/2006							6.900	
	06/19/2006							6.850	
	07/10/2006							6.900	
	10/04/2006							6.900	
	02/12/2007							6.900	
	05/13/2007							6.800	
	07/09/2007							7.000	
	10/22/2007							7.000	
	06/29/2008	08071070-3	[18.000]	320.000	[3.000]			[770.000]	[1,500.000]
	07/21/2008	08073732-2	[16.000]	330.000	[2.500]		6.800	[750.000]	[1,600.000]
	10/08/2008	08102352-3	[14.000]	310.000	[2.400]		[6.300]	[740.000]	[1,400.000]

April 9, 2009
9 :5 AM

Hutsonville Ash Impoundment
Table 2-6b. Groundwater Monitoring Results: Pond D Deep Alluvial Aquifer, 2002-2008

Date Range: 01/01/2002 to 12/31/2008

Well Id	Date Sampled	Lab Id	B, tot, mg/L	Ca, tot, mg/L	Mn, tot, mg/L	pH (field), std	SO4, tot, mg/L	TDS, mg/L
MW115D	04/11/2005	05042061-3	0.022	59,000	[0.730]	7.410	55,000	320,000
	06/26/2006					7.400		
	10/09/2006					7.400		
	02/19/2007					7.200		
	06/20/2007					7.400		
	09/12/2007					7.100		
	10/22/2007					7.200		
	06/29/2008	08071070-5	0.100	57,000	0.008	7.200	34,000	240,000
	09/16/2008	08093137-2	0.054	68,000	[0.760]	7,000	38,000	330,000
	10/14/2008							

MANAGES

TSD 000068

April 9, 2009
9:15 AM

Table 2-6b. Groundwater Monitoring Results: Pond D Deep Alluvial Aquifer, 2002-2008 Hursonville Ash Impoundment

Date Range: 01/01/2002 to 12/31/2008

Limit		B, tot, mg/L	Ca, tot, mg/L	Mn, tot, mg/L	pH (field), std	SO4, tot, mg/L	TDS, mg/L
Well Id	Date Sampled	State SId	Lab Id				
MW115S	04/11/2005	05042061-4		0.020	75.000 [0.200]	7.500 46.000	7.160 340.000
	06/26/2006						
	10/09/2006						
	02/19/2007						
	06/20/2007						
	09/12/2007						
	10/22/2007						
	06/29/2008						
	08071070-6			0.083	57.000 [0.610]	7.300 7.200	31.000 250.000
	09/16/2008						
	08093137-3			0.065	75.000 [3.300]		14.000 350.000
	10/08/2008						
	08102352-6			0.110	67.000 [1.200]	7.100 43.000	310.000 310.000

MANAGES

April 9, 2009
5 AM

Hutsonville Ash Impoundment
Table 2-6b. Groundwater Monitoring Results: Pond D Deep Alluvial Aquifer, 2002-2008

Date Range: 01/01/2002 to 12/31/2008

Well Id	Date Sampled	Lab Id	Limit	B, tot, mg/L	Ca, tot, mg/L	Mn, tot, mg/L	pH (field), std	SO4, tot, mg/L	TDS, mg/L
				State Std	2.000	0.150	6.500 - 9.000	400.000	1,200.000
MW121	01/15/2002	02092792-6	0.110	70.000	[2.000]	34.000	34.000		
	09/19/2002		0.082	77.000	[1.400]	40.000	40.000		
	12/19/2002	02123013-8	0.067	78.000	[1.200]	7.310	38.000		
	03/17/2003	03032351-3	0.200	83.000	[0.920]	7.300	65.000		
	06/17/2003	03062509-1	0.052	74.000	[0.820]	7.600	62.000		
	08/11/2003	03082176-5	0.110	71.000	[1.100]	7.484	52.000		
	10/13/2003	03102279-9	0.075	56.000	[0.760]	7.500	30.000		
	02/23/2004	04022960-1	0.085	86.000	[2.100]	7.300	27.000		
	04/19/2004	04042676-5	0.099	72.000	[1.200]	7.300	19.000		
	08/02/2004	04081328-9	0.180	72.000	[1.400]	7.400	24.000		
	10/04/2004	04101561-12	0.084	77.000	[1.400]	7.400	23.000		
	03/16/2005	05032818-13	0.060	57.000	[0.640]	7.440	34.000		
	03/27/2006					7.000			
	06/19/2006					7.350			
	07/10/2006					7.580			
	10/04/2006					7.200			
	02/12/2007					7.280			
	05/13/2007					7.200			
	07/09/2007					7.400			
	10/22/2007					7.000			
	06/29/2008	08071070-4	0.180	51.000	[0.640]	7.000			
	07/21/2008	08073732-5	0.086	50.000	[0.680]	6.800	23.000		
	10/08/2008	08102352-5	0.120	58.000	[0.680]	6.800	18.000		
							33.000	210.000	
								230.000	
								260.000	

April 9, 2009
9 15 AM

Hutsonville Ash Impoundment
Table 2-6b. Groundwater Monitoring Results: Pond D Deep Alluvial Aquifer, 2002-2008

Date Range: 01/01/2002 to 12/31/2008

Well Id	Date Sampled	Lab Id	Limit		B, tot, mg/L	Ca, tot, mg/L	Mn, tot, mg/L	pH (field), std	SO4, tot, mg/L	TDS, mg/L
			State Std	2.000	0.150	6,500 - 9,000	400,000	1,200,000		
MW14	01/14/2002			1.400	170,000	[0.380]		230,000	78,000	
	06/30/2002			0.190	180,000	[0.530]	7,000	230,000	900,000	790,000
	09/18/2002	02092792-9		0.570	180,000	[0.500]	6,920	210,000	740,000	
	12/13/2002	02122525-5		0.730	160,000	[0.510]	7,000	120,000	570,000	
	03/18/2003	03032481-5		1,000	180,000	[0.480]	7,000	230,000	830,000	
	05/12/2003	03032186-5		0.400	160,000	[0.410]	7,345	180,000	740,000	
	08/11/2003	03082176-4		0.630	170,000	[0.510]	7,300	200,000	810,000	
	10/13/2003	03102279-8		1,400	180,000	[0.430]	6,800	190,000	810,000	
	02/23/2004	04022960-3		1,500	170,000	[0.400]	6,900	190,000	780,000	
	04/04/2004	04041354-7		1,000	180,000	[0.450]	6,900	200,000	810,000	
	08/03/2004	04081328-12		1,100	170,000	[0.510]	6,900	180,000	760,000	
	11/08/2004	04112264-10		0.880	160,000	[0.350]	6,920	220,000	780,000	
	03/15/2005	05032818-12					6,800	7,500		
	03/13/2006							6,600	6,600	
	06/20/2006							6,800	6,800	
	10/25/2006							6,700	6,700	
	02/27/2007							7,200	7,200	
	05/13/2007							6,600	6,600	
	09/10/2007							140,000	140,000	650,000
	11/11/2007							7,100	7,100	
	03/17/2008	08032889-1		0.480	160,000	[0.500]		170,000	170,000	690,000
	06/23/2008	08064092-5		0.910	180,000	[0.560]	6,700	120,000	650,000	
	09/16/2008	08093137-1		0.370	150,000	[0.480]	6,700	140,000	670,000	
	10/21/2008	08103771-3		0.540	170,000	[0.570]				

MANAGES

TSD 000071

April 9, 2009
C 5 AM

Hutsonville Ash Impoundment
Table 2-6b. Groundwater Monitoring Results: Pond D Deep Alluvial Aquifer, 2002-2008

Date Range: 01/01/2002 to 12/31/2008

Well Id	Date Sampled	Lab Id	Limit		B, tot, mg/L	Ca, tot, mg/L	Mn, tot, mg/L	pH (field), std	SO4, tot, mg/L	TDS, mg/L
			State Std	2.000	0.150	6.500 - 9.000	400,000	1,200,000		
MW7D	01/15/2002		0.240	88,000	[0.620]			58,000	420,000	420,000
	07/01/2002				[0.750]		7.410	51,000	370,000	370,000
	09/18/2002	02092792-8	0.083	71,000						
	12/19/2002	02123013-3	0.140	67,000	[0.750]		7.380	31,000	320,000	320,000
	03/19/2003	03032570-2	0.089	66,000	[0.760]		7.300	51,000	350,000	350,000
	06/02/2003	03061314-7	0.088	68,000	[0.680]		7.700	60,000	390,000	390,000
	08/11/2003	03082176-2	0.140	69,000	[0.660]		7.530	59,000	370,000	370,000
	10/13/2003	03102279-3	0.110	66,000	[0.640]		7.500	44,000	320,000	320,000
	02/23/2004	04022960-6	0.110	89,000	[0.770]		7.400	68,000	430,000	430,000
	04/19/2004	04042676-2	0.067	85,000	[0.830]		7.300	61,000	440,000	440,000
	08/02/2004	04081328-7	0.091	81,000	[0.570]		7,000	47,000	360,000	360,000
	10/04/2004	04101561-9	0.210	85,000	[0.660]		7,500	36,000	420,000	420,000
	03/15/2005	05032818-7	0.062	61,000	[0.450]		7.530	42,000	280,000	280,000
	03/27/2006						6,800			
	06/26/2006						7,300			
	10/09/2006						6,900			
	02/19/2007						7,200			
	06/20/2007						7,100			
	09/10/2007						7,300			
	10/22/2007						7,300			
	06/29/2008						7,000			
	(08071070-2)		0.680	130,000	[1.600]			75,000	530,000	530,000
	09/15/2008						7,000			
	10/08/2008	(08102352-2)	0.180	75,000	[0.540]		7,000		35,000	320,000

MANAGES

TSD 000072

Table 3-1 - Closure Alternatives Screening Summary
Pond D Closure Alternatives Report
Huntington Power Station
Ameren Services

NRT PROJECT NO.: 19542.3
 BY: EIT CIRCD BY: BRH
 DATE: 4/22/09 DATE: 4/23/09

Category	Alternative	Description	Construction / Implementation Feasibility	Effectiveness	Relative Cost		Capital	Annual O & M	Carry Forward (Y/N/no)
					Capital	Annual O & M			
Groundwater Management	Site Monitoring w/ No Groundwater Collection	The groundwater monitoring network is already in place - additional wells can be added as necessary to enhance the monitoring network.	This option will not prevent off-site migration of impacted groundwater.	Quarterly monitoring currently performed. No additional cost.	At a minimum, site monitoring will be performed. Additional groundwater management alternatives may be incorporated with site monitoring.	NO			
Collection Trench	A groundwater collection trench would be installed south of Pond D to collect impacted groundwater. A perforated pipe in the trench would drain by gravity to sumps containing pumps designed to transfer collected groundwater to the Intern Ponds (Pond B).	A hydraulic analysis would need to be performed to model additional loading to the sluice water system and evaluate compliance with the existing NPDES permit for outfall #002.	Collection of groundwater and management through Pond B for eventual discharge to the Wabash River via outfall #002 will prevent off-site migration of impacted groundwater.	\$800,000	\$47,000	Cost could increase substantially (2 to 5 times) if treatment of extracted groundwater is required.	YES	For an undetermined period	This alternative could effectively prevent off-site migration of impacted groundwater. Capital costs are lower than other groundwater management alternatives considered.
Ash Stabilization	Ash fill is stabilized and solidified using one of several methods to form a cementitious matrix (monolith) that immobilizes ash constituents, increases strength, and decreases permeability.	Stabilization process would result in a substantial increase in volume (typically 20 - 40 %). Stabilized/solidified ash monolith would minimize leaching, but concentrations of certain trace constituents, such as selenium, may increase with pH, making performance difficult to predict. Long term monitoring would be required to evaluate effectiveness.	Removal of ash is an effective means of source control (i.e., source elimination) provided that saturated ash is removed, and removal of saturated ash may be very difficult due to its depth below the water table.	\$20,000,000	\$5,000	Very high cost groundwater management option.	NO	O & M costs would be similar to those associated with a final cover.	Capital costs are too high compared to other groundwater management alternatives with less technical uncertainty and same or better effectiveness.
Ash Removal and Disposal, Recycling	Ash is excavated and transported to an appropriate landfill, moved to appropriate sites for recycling, or re-used on site. Recycling may include incorporation into cement, for use in agricultural settings as a source of minerals, or as flowable fill in slurry form.	Excavation involves standard construction equipment. Excavation of saturated ash may require shoring, dewatering, and use of drainage bucket or mud, and is likely not technically or economically feasible. This alternative would likely require profit of the ash waste for disposal in an appropriate landfill or identification of large-volume users of mixed ash. Recycling may require grading or sorting of ash. Based on prior testing, excavated ash from Pond D may not meet criteria for beneficial reuse.	Removal of ash is an effective means of source control (i.e., source elimination) provided that saturated ash is removed, and removal of saturated ash may be very difficult due to its depth below the water table.	\$23,000,000 to \$34,000,000	None to \$5,000	Very high capital cost groundwater management alternative. Range of costs represents partial removal (saturated ash) only and overburden replacement to total removal of ash. Incremental increases in general fill or ash disposal/recycling costs would cause significant increases in capital costs for this alternative.	NO	O & M costs would be similar to those associated with a final cover if partial excavation was performed.	Capital costs are too high compared to other groundwater management alternatives with less technical uncertainty and same or better effectiveness.
Pond D Reconstruction (Ash Excavation; Install Liner and Leachate Collection System; Ash Replacement)	Ash is excavated and moved to facilitate reconstruction of impoundment to minimize infiltration, leachate generation, and groundwater impact; separate ash from water table, and control erosion.	Reconstruction would require excavation and off-site disposal or relocation of all ash in pond D. As discussed above, excavation of saturated ash is likely not technically or economically feasible. Clean fill would have to be placed to re-establish the base of the impoundment at least 1' feet above the historical high water table. Potential for significant regulatory issues for permitting since reconstruction project could be considered establishing a new disposal unit.	Reconstruction could be an effective means of source control; however a viable method for removing ash up to 15 feet below the water table would be needed for this option to be seriously considered - effectiveness would be greatly reduced, particularly in terms of preventing off-site migration of impacted groundwater, if saturated ash could not be removed.	NOT EVALUATED	Due to construction feasibility, very high anticipated capital costs.	NOT EVALUATED	Due to lack of effectiveness.	NOT EVALUATED	Due to construction feasibility, very high anticipated capital costs.
Containment Using a Low-Permeability Vertical Barrier	A vertical barrier constructed of low-permeability materials would be constructed downgradient or surrounding Pond D.	A slurry wall may not be feasible between Pond D and the Wabash River due to spatial constraints and buried utilities. Installation of a sheet pile wall may be feasible depending on depth. A low-permeability vertical barrier requires a low-permeability key-in-formation to create an effective barrier to groundwater flow. Based on the Sherry Hall Study, prepared by Hanson Engineers, Inc. (1984), and slug tests performed at the site, the sandstone bedrock present in the upland portion of the site would not provide a competent key-in formation for a low-permeability vertical barrier.	A low-permeability vertical barrier would not be effective at this site since a competent key-in formation is not present in all areas.	NOT EVALUATED	NOT EVALUATED	NOT EVALUATED	NOT EVALUATED	NOT EVALUATED	Not effective for groundwater management at this site.
Final Cover	Geomembrane	Pond D is covered with a geomembrane to prevent direct contact, control infiltration of surface water, reduce leachate generation, and provide erosion control. A 3-foot thick soil layer would be needed over the geomembrane to drain infiltrated surface water from above the geomembrane, protect the geomembrane from weathering and maintenance activities on the surface of the final cover, and support vegetation.	A geomembrane cover would effectively minimize infiltration and resulting leachate generation from Pond D. Additionally, the cover would provide protection from erosion and prevent direct contact with ash.	\$3,900,000	\$5,000	Lowest cost cover alternative meeting closure objective of minimizing infiltration. Capital costs sensitive to surface water management options and related cover grading plans / fill costs.	YES	O & M costs associated with maintaining vegetation and 3-foot protective soil layer, and repairing erosion damage.	Capital costs are lower than compacted clay, and geomembrane has greater effectiveness than either the porouslattice or earthen cover alternatives.

TSD 000073

Table 3-1 - Closure Alternatives Screening Summary
Pond D Closure Alternatives Report
Huntsville Power Station
Ameren Services

NRT PROJECT NO.: 19340.3
 BY: EIT CHECK BY: BRH
 DATE: 4/22/09

Category	Alternative	Description	Construction / Implementation Feasibility	Effectiveness	Capital	Relative Cost	Annual O&M	Curv. Forward (Tca/yr)
Final Cover (continued)	Compacted Clay	Pond D is covered with compacted clay to prevent direct contact, control infiltration of surface water, reduce leachate generation, and provide erosion control.	Compacted clay has been installed in other by ash management facilities to reduce surface water infiltration and leachate generation. A local source for clay would have to be identified and may not be available. There would be site grading and drainage limitations to geomembrane cover, the clay cover would provide protection from erosion and prevent direct contact with ash.	A compacted clay cover would effectively reduce surface water infiltration or resulting in reduced leachate generation from Pond D. Additionally similar to a geomembrane cover, the clay cover would provide protection from erosion and infiltration. When compared to geomembrane, a compacted clay is not a cost-competitive cover option.	\$4,200,000	\$5,000	\$5,000	NO Higher cost final cover option. Additional capital cost not warranted since geomembrane has similar feasibility / effectiveness.
	Layered Earth	A layered earth cover is constructed from on-site earth materials to prevent site grading and drainage limitations to overcome similar to geomembrane.	A layered earth cover could be readily constructed from on-site materials. There would identify a mix that achieves a permeability lower than 1×10^{-6} cm/s with adequate strength.	A layered earth cover will allow more surface water infiltration and resulting leachate generation from Pond D than a geomembrane or compacted clay cover. The layered earth cover would provide erosion control if vegetated property and would prevent direct contact with ash.	\$2,900,000	\$5,000	\$5,000	NO This alternative is less effective than the geomembrane and compacted clay alternatives.
	Pozzolan Fly Ash	Pond D is covered with a pozzolan fly ash cover could potentially use fly ash already on site in pond A and result in a significant cost savings for materials. Mit design testing was unable to identify a mix that achieves a permeability lower than 1×10^{-6} cm/s with adequate strength.	Construction of a pozzolan fly ash cover would reduce surface water infiltration and leachate generation from Pond D, provide erosion control, and prevent direct contact with ash, although not to the same degree as a geomembrane or compacted clay cover.	A pozzolan fly ash cover would reduce surface water infiltration and leachate generation from Pond D than a geomembrane or compacted clay cover.	\$4,000,000	\$5,000	\$5,000	NO This alternative is less effective than the geomembrane and compacted clay alternatives.
	Rout. Surface Water East Toward Wabash River	The grade of Pond D would be adjusted to promote gravity drainage of surface water toward the Wabash River.	Technically and administratively feasible - the grade of Pond D could be readily adjusted to route surface water toward the Wabash River. Can be constructed if adequate source(s) of fill are identified in close proximity to the site.	This would be an effective surface water management option that could be readily integrated with a final cover.	NOT EVALUATED	Only slightly more expensive than the geomembrane cover. However, capital cost for the cover could be evaluated versus the benefit of creating an additional 110,000 yd ³ capacity in Pond A.	Routing all surface water to the Wabash River would require excess fill compared to other alternatives.	NO Routing all surface water to the Wabash River would require excess fill compared to other alternatives.
	Rout. Surface Water West Toward Pond C	The grade of Pond D would be adjusted to promote gravity drainage of surface water toward Pond C.	Technically and administratively feasible - the grade of Pond D could be readily adjusted to route surface water towards Pond C. Can be constructed if adequate source(s) of fill are identified in close proximity to the site. This surface water management option would require its fill to route surface water towards the Wabash River. A box culvert has already been constructed to allow surface water drainage from Pond D to Pond C.	This would be an effective surface water management option that could be readily integrated with a final cover.	NOT EVALUATED	Anticipated to be significantly more expensive than routing surface water to both the east (Wabash River) and west (Pond C).	Routing all surface water to Pond C would require excess fill compared to the other alternatives.	NO Routing all surface water to both the east (Wabash River) and west (Pond C).
	Rout. Surface Management	The grade of Pond D would be adjusted to promote gravity drainage of surface water on the west side of Pond D toward source(s) of general fill.	Technically and administratively feasible - the grade of Pond D could be readily adjusted to route surface water towards Pond C and the Wabash River. Can be constructed if adequate source(s) of fill are identified in close proximity to the site. This surface water management option would require the least amount of fill to construct. A box culvert has already been constructed to allow surface water draining from Pond D to Pond C.	This would be an effective surface water management option that could be readily integrated with a final cover. It combined with an earthen cover, swales designed to route surface water may have to be lined with a geomembrane.	SEE FINAL COVER OPTIONS	Fills required for grade adjustment to route surface water drainage towards Pond C and the Wabash River is already included as part of the final cover estimates. Actual costs would likely be less than routing surface water exclusively towards the Wabash River or Pond C.	YES	YES This surface water management alternative requires the least amount of fill needed to route surface water off of Pond D; it has been incorporated within the final cover alternative estimates.

Pond D Closure Alternatives Report
 Hutsonville Power Station
 Ameren Services

Table 3-2 - Areal Extent and Volumes of Unsaturated and Saturated Ash In Pond D

NRT PROJECT NO.: 1954/2.3

BY: GRL/EJT/KJB CHKD BY: CAR/EJT

DATE: 0-7/05, U-4/09

Site Specific Parameters	Unit	Unlined Ash Impoundment (Pond D)
Total Volume of Ash	CY	950,000
Volume of Unsaturated Ash	CY	670,000
Volume of Saturated Ash	CY	280,000
Areal Extent of Ash	SF	966,000
	ACRES	22
Areal Extent of Saturated Ash	SF	790,000
	ACRES	18
Thickness of Unsaturated Ash	FT	11-31
Thickness of Saturated Ash	FT	5-14
Depth to Bottom of Saturated Ash	FT	11-31

Source Notes:

1. Total estimated area for saturated ash: areal extent ~ 790,000 ft², average thickness ~ 9.5 ft, average depth to bottom of saturated ash ~ 25 ft.
2. Based on above estimates: 280,000 yd³ saturated ash (790,000 ft² x 9.5 ft).
3. Total estimated area for ash: areal extent ~ (22 acres) 966,000 ft², average thickness estimated from Geoprobe boring logs (20.9 feet).
4. Based on above estimates: 750,000 yd³ ash (966,000 ft² x average thickness) + 80,000 yd³ transferred in 2004 + 120,000 yd³ transferred in 2006-2007 = 950,000 yd³.
5. Total ash volume includes unsaturated ash (550,000 yd³) and saturated ash (280,000 yd³).

CY = Cubic yards

SF = Square Feet

TSD 000075

Table 3-3 - Final Cover Alternatives Material Balance Analysis
 Pond D Closure Alternatives Report
 Husonville Power Station
 Ameren Services - Husonville, Illinois

NRT PROJECT NO.: 132516.1
 BY: CAR CRKD BY: ENT S19/05
 DATE: 0-7/05 U-4/09

Fill Utilization	Fill Origin	Calculation	Final Cover Alternative				
			Unit	Clay	Pozzolanic	Geosynthetic	Earthen
Establish Grade	Fly Ash Stockpile ³ (V_{as})	[A] - Assumption 8 [B = L * (A + C + D + E + F + G + H + I)]	CY	50,500	50,500	50,500	50,500
Additional Imported Fill ⁴			CY	700	700	86,100	86,100
Beneficial Reuse Ash		[C] - Assumption 9	CY	--	--	20,000	20,000
Low Permeability Layer ⁵ (V_{fc})	Clay	[D] - Assumption 5	CY	105,400	--	--	--
	Cement	[E] - 5% of Pozzolanic Cover (dry weight basis)	CY	--	2,500	--	--
	Fly Ash-Pozzolanic Mix	[F = D - E]	CY	--	102,900	--	--
Final Protective Layer ⁶ (V_{al})	Beneficial Reuse Ash	[G] - Assumption 9	CY	20,000	--	--	--
	Imported Rooting Zone Soil	[H = Assumption 6 - G - I]	CY	85,400	105,400	87,800	87,800
	Sand Drainage Layer ⁷	[I] - Assumption 7	CY	--	--	--	17,600
Total Imported Rooting Zone		[J = H + I]	CY	85,400	85,400	105,400	105,400
Total Fill Volume for Pond D ¹		[K] - Assumption 1	CY	262,000	262,000	262,000	262,000

Assumptions and References:

- The Total Fill Volume for Pond D was calculated from design grades with minimum 5% final cover slope for drainage, existing grades established by aerial survey performed by Connor & Connor on April 14, 2005 including an estimate of capacity below standing water of 5,000 yd³ and estimate of current ash volume provided by Ameren Energy Generating; the calculated Total Fill Volume for Pond D was approximately 262,000 yd³.
- Final cover material estimates are included as part of estimated volume of fill to make Pond D grades.
- All material balance estimates assume the ash stockpile will be used as fill beneath the final cover.
- Additional imported fill is required if $V_{as} + V_{re} + V_{pl} < 357,000$ yd³.
- Low permeability layer volume (105,400 CY) estimated assuming an approximate 22 acre cover area with 3' thick cover, clay and pozzolanic final covers only.
- Final protective layer volume (105,400 CY) estimated using an approximate 22 acre cover area with 3' thick cover, required for ALL final cover alternatives.
- For the earthen cover, the final protective layer consists of: 1) a 6" sand drainage layer, and 2) a 2.5' rooting zone layer.
- Fly ash stockpile volume (50,500 CY) estimate calculated from elevation 453 feet and above.
- Beneficial ash volume estimated by Husonville Power Station personnel at approximately 20,000 yd³.

CY = Cubic yards

TSD 000076

APPENDIX A

SITE INVESTIGATION APPENDICES

APPENDIX A-1

SOIL BORING LOGS

CENTRAL ILLINOIS DRILLING COMPANY
1909 OAKWOOD AVE.
BLOOMINGTON, ILLINOIS 61701
(309) 662-5968

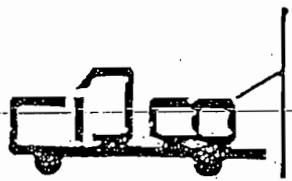


LOG OF BORING

CONTRACTED WITH HANSON ENGINEERS
PROJECT NAME MURGOVILLE POWER STATION
LOCATION PEC PLAN
DATUM HAMMER WT. 140# HAMMER DROP 30" HOLE DIA. 8"
SURFACE ELEV. CORE DIA.
DATE STARTED 2-14-84 COMPLETED 2-14-84 CASING
DRILLING METHOD HSA

ELEV.	DESCRIPTION	STRATA	DEPTH	SAMPLES						NOTES
		DEPTH	SCALE	BLOWS FT.	NO.	TYPE	RECOV.	Q.P.		
456.5		0.0	30							
455.6	See #A	0.0								
453.4	Lt. brn. sandy silt, wf. clay, occas. f-c sand, occas. f. gravel roots moist-v. moist	3.1		1-2-3	1	ss	18"	1.0 2.4		
	Lt. br. m-c sand, wf. occas. f-m gravel tr. silt	5		6-5-7	2	ss	17	--		
450.1	wet	6.4								
448.4	Lt. brn. sandstone moist	8.1		6-54- 40/2"	3	ss	14	2.2		
447.4	Lt.-gray sandstone	9.1		65-35/	4	ss	7	--	WATER 2-14-84	
	END OF BORING 9.1'	10		1"					DD 6.0 8:30am	
		11							BAR 7.0 8:55am	
		12							AAR--	
		13							WL 6.5 9:05am	
		14							F-c gravel 5.0'	
		15							Screen 9.0'-4.0' 2" PVC Pipe 4.0' Gravel 9.1'-3.0' Bentonite 3.0'-2	
		16							Plug 1.5'-surface	
		17							Water level 4.0 air 21	
		18							#A Blk. clayey s wf. tr. f. sand occas. organic fibers topsoil moist	

TSD 000079



LOG OF BORING

CENTRAL ILLINOIS DRILLING COMPANY
1909 OAKWOOD AVE.
BLOOMINGTON, ILLINOIS 61701
G (309) 662-5968

CONTRACTED WITH HANSON ENGINEERS

CONTRACTED WITH HUTSONVILLE POWER STATION

BORING NO. A-2

PROJECT NAME _____

CONTRACT NO. .

DATUM _____ HAMMER WT 140^{LB} HAMMER DROP 30."

HAMMER WT. 17.0 HAMMER DROP 11" HOLE DIA. 1/2"

DATE STARTED 2-10-84 CORE DIA. 2 3/8" CASING

DATE STARTED 2-10-84 COMPLETED 2-10-84 DRILLING METHOD HSA

ELEV.	DESCRIPTION	STRATA DEPTH		SAMPLES					NOTES
		DEPTH	SCALE	BLOWS FT.	NO.	TYPE	RECOV.	CD	
953.3		0.0	30						
952.9	See SA	0.4							
951.2	Brn. silty sand fill v. moist	2.1							
	Brn. m-c sand, wf. m-c gravel tr. silt			8-8-6	1	ss	18"	2.4	
	v. moist	5		7-5-3	2	ss	17	--	
				3-3-3	3	ss	16	--	WATER 2-10-84
444.9		8.4							
	Brn.-gray m-c sand, wf. m. gravel			10	3-4-7	4	ss	14	--
	wet								WL 7.0 2:10pm
				8-7-0	5	ss	17	--	Screen 18.0-5. 2" PVC pipe 5.0 3.0' surface Gravel 21.5'-1' Bentonite 4.0' Plum 2.0'-surf.
439.2		14.1							
	Brn.-gray m-c sand, wf. f-m gravel			15	6-8-10	6	ss	17	--
	wet								#A 51/2' coal refuse 4" wf. occas. silt fi wet
436.0		17.3							
	Gray silty clay, wf. tr. f. sand, occas. f. gravel			10-13-	7	ss	17	--	
	till moist			13					
				5-10-	8	ss	18	4.2	
				20					

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LOG OF BORING

CONTRACTED WITH HANSON ENGINEERS BORING NO. M-2
PROJECT NAME HUTSONVILLE POWER STATION CONTRACT NO. _____
LOCATION Per Plan
DATUM _____ HAMMER WT. 140# HAMMER DROP 30" HOLE DIA. 8"
SURFACE ELEV. CORE DIA. CASING.
DATE STARTED 2-10-84 COMPLETED 2-10-84 DRILLING METHOD E&A

ELEV.	DESCRIPTION	STRATA		DEPTH DEPTH	SAMPLES					NOTES
		SCALE	BLOWS FT.		NO.	TYPE	RECOV.	QP		
453.3		n/a	30							
431.8		21.5			5-7-11	0'	ss	18"	4.0	
	END OF BORING 21.5'									

TSD 000081



LOG OF BORING

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CONTRACTED WITH HANSON ENGINEERS BORING NO. 1-?
 PROJECT NAME POTTSVILLE POWER STATION CONTRACT NO.
 LOCATION P-5 PLAN
 DATUM 140' HAMMER WT. 140# HAMMER DROP 30" HOLE DIA. 8"
 SURFACE ELEV. CORE DIA. CASING
 DATE STARTED 2-0-84 COMPLETED 2-9-84 DRILLING METHOD RSA

ELEV.	DESCRIPTION	SAMPLES						NOTES		
		STRATA	DEPTH	DEPTH	SCALE	BLOWS FT.	NO.	TYPE	RECOV.	
452.1			0.0	30						
451.7	See #A		0.4							
	Rust brn. silty sand.					4-6-8	1	ss	14"	--
	fill v. moist			5		4-3-4	2	ss	16	--
445.8	BTM. f-c gravel, wf. m-c sand, occas. sandstone wet		6.3							
444.5	F-m sand		7.6		6-10-	3	ss	18	--	WATER 1-9-84
443.2	v. moist		8.0		11					DD 5.5' 2:30pm
442.7	See #B		0.4		15-85/	4	ss	17	--	BAR 6.0' 2:45pm
	END OF BORING 9.4'			10	5"					AAR
										WL 5.0' 4:45pm
										#A Blk. coal refuse, 4" cir wf. silt fill v. moist
										#B Brn. sandst wf. f-m sand w
										Screen 0.4'-4 2" PVC Pipe 4"
										Gravel 0.4'-4 Bentonite 4.0' 2.5'
										Plum 1.5'-surf Grout 2.5'-1.1' 4" standpipes 3.



LOG OF BORING

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CONTRACTED WITH HANSON ENGINEERS

PROJECT NAME HUTSONVILLE POWER STATION

LOCATION PER PLAN

DATUM HAMMER WT. 140#

HAMMER DROP 30"

HOLE DIA. 8"

SURFACE ELEV.

CORE DIA.

CASING

DATE STARTED 2-13-84

COMPLETED 2-13-84

DRILLING METHOD HSA

ELEV.	DESCRIPTION	STRATA		DEPTH	SAMPLES					NOTES
		DEPTH	SCALE		BLOWS	FT.	NO.	TYPE	RECOV.	
454.4		0.0	30							
453.1	Blk. asphalt 1.0" F-m gravel 1.0", brn, clayey silt wf. f-c gravel pavement mater- ials moist	1.3			5-5-7		1	ss	16"	--
451.3	Blk. silt, wf. f-c gravel silt moist	3.1								
)	Brn. silty sand, wf. occas. f-m gravel moist	5	4-3-3	2			ss	18	0.9	
448.5		5.9								
446.2	Br. f-m sand wf. silt v. moist	8.2	3-3-4	2			ss	18	--	WATER 2-13-84
443.5	Br. f-m gravel, wf. c-m sand, silt wet	10	3-3-3	4			ss	17	0.6	DD 8.0 9:45am BAR 8.0 10:30am AAR --- JL 7.5 11:45am
441.0	Lt.-br. sandstone	13.4	23-77	5			ss	11	--	Screen 12.5' -5 2" PVC Pipe 5.0' 3.0'
	END OF BORING 13.4'	15	100/4"	6			ss	4	4.5t	Gravel 13.4' -4 Bentonite 4' 0'. 2' 0'. Flux 2.0' -surf.

TSD 000083

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LOG OF BORING

CONTRACTED WITH HANSON ENGINEERS
PROJECT NAME HUTSONVILLE POWER STATION

BORING NO. 3-5
CONTRACT NO.

LOCATION PER PLAN

DATUM HAMMER WT. 140# HAMMER DROP 30" HOLE DIA. 8"

SURFACE ELEV.

CORE DIA.

CASING

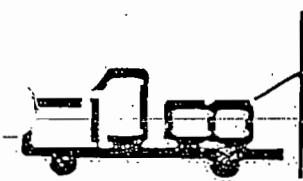
DATE STARTED 2-13-84

COMPLETED 2-13-84

DRILLING METHOD HSA

ELEV.	DESCRIPTION	STRATA	DEPTH		SAMPLES					NOTES
			DEPTH	SCALE	BLOWS FT.	NO.	TYPE	RECOV.	QP	
952.3			0.0	30						
951.7	1" coal refuse, brn. clayey silt, wf. f.c gravel	1.2								
949.2	occas. organic fibers fill moist	3.1			4-5-5	7	ss	34"	--	
946.4	Brn. f. sand, wf. occas. c. sand, f. gravel moist v. moist	5.9		5	3-2-4	2	ss	17	0.4	DT 8.0 2:50pm BAR 11.0 3:50pm AAR ----- WL 6.5' 5:45pm
943.9	Br. f-m sand, wf/ c sand wet	8.4			3-3-4	3	ss	18	0.6	
941.7	Brn. m-c sand, wf. f- c gravel occas. blk. coal refuse mottling	10.6		10	3-4-4	4	ss	18	0.9	Old metal drain pipe 1.0' west boring running from road to station
936.1	Brn.-gray m-c sand, wf. f-m gravel wet	14.2			0-3-3	5	ss	16	--	Screen 18.0'-5. 2" PVC pipe 5'. 3.0' stick Gravel 18.0'-4. Bentonite 4.0'. Backfilled 10'. 18.0' wf. gray Plus 2.0'-surf. -4" stand pipe
935.4	Brn.-gray sandstone, wf f-c sand occas. m-c sand v. moist	16.0		16-15	7	ss	12	--		#A Brn. gray m-c sand, wf. f-c gravel, or white rock fill
933.1	Gray sandstone	-		---22	78	ss	6	--		wet
	END OF BORING 19.2'		20		30-70	8	ss	8	4.5t	

TSD 000084



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LOG OF BORING

CONTRACTED WITH HANSON ENGINEERS

PROJECT NAME HUTSONVILLE POWER STATION
LOCATION PER PLAN

BORING NO.

二-六

DATUM HAMMER WT. 110± HAMMER DROP 30" HOLE DIA. 8"
SURFACE ELEV. CORE DIA. CASING
DATE STARTED 2-0-84 COMPLETED 2-9-84 DRILLING METHOD RSA

TSD 000085

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LOG OF BORING

CONTRACTED WITH HANSON ENGINEERS
PROJECT NAME HUTSONVILLE POWER STATION
LOCATION PER PLAN
DATUM HAMMER WT. 140# HAMMER DROP 30" HOLE DIA. 8"
SURFACE ELEV. CORE DIA. CASING
DATE STARTED 2-8-84 COMPLETED 2-8-84 DRILLING METHOD HSA

ELEV.	DESCRIPTION	STRATA		DEPTH	SAMPLES					NOTES
		DEPTH	SCALE		BLOWS	FT.	NO.	TYPE	RECOV.	
437.9		0.0	30							
436.5	Br. clayey silt, wf. tr. f. sand, occas. organic fibers moist	1.4								
434.0	Br. clayey silt, sand, wf. occas. blk. min- erals fill moist	3.0		3-2-7	1	ss	17"	--		
429.8	Lt. brn.-brn. sandy silt, wf. clay moist	5	2-3-4	2	ss	14	--			
425.0	Brn. sandy silt, wf. tr. clay very moist	8.1	3-3-5	3	ss	16	1.7			WATER 2-8-84
420.3	Brn. silt, wf. f. sand very moist-wet	10	2-2-3	4	ss	14	1.2			DD 11.5 11:45a BAR 11.5 3:00p AAR ---- WL 11.5 5:15p
		12.9	0-0-3	5	ss	15	1.3			Screen 25.0'-1 2" PVC pipe 15 5.0' stick n
		15	2-2-4	6	ss	15	1.7			Gravel 25.0'-1 Bentonite 14.0 12.0 Plum 2.0'-surf Bentonite-clay 12.0'-2.0' Standpipe 3.0' 5.1' stick
		17.5	2-2-3	7	ss	18	1.4			
		20	0-1-3	8	ss	17	1.2			

TSD 000086



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LOG OF BORING

CONTRACTED WITH HANSON ENGINEERS BORING NO. M-7
PROJECT NAME HUTSONVILLE POWER STATION
LOCATION PEH PLAN CONTRACT NO.
DATUM 740 ft HAMMER WT. 740 ft HAMMER DROP 30" HOLE DIA. 8"
SURFACE ELEV. 2-8-84 CORE DIA. 2-8-84 CASING
DATE STARTED 2-8-84 COMPLETED 2-8-84 DRILLING METHOD USA

ELEV.	DESCRIPTION	SUBSTRATA	DEPTH	SAMPLES					NOTES
		DEPTH	SCALE	BLOWS FT.	NO.	TYPE	RECOV.	QP	
437.9		0.0	30						
416.5	Brn. sandy silt wf. lenses, f. sand wet	21.4							
	Brn. f. sand								
414.5	wet	23.4							
	Brn. f-c gravel, wf. m-c sand, tr. silt wet	25.0		7-7-9	9	ss	12	--	
	END OF BORING 25.0'								

TSD 000087

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LOG OF BORING



CONTRACTED WITH HANSON ENGINEERS BORING NO. M-8
PROJECT NAME HUTSONVILLE POWER PLANT CONTRACT NO. _____
LOCATION PER PLAN
DATUM HAMMER WT. 140# HAMMER DROP 30" HOLE DIA. 8"
SURFACE ELEV. CORE DIA. CASING
DATE STARTED 2-7-84 COMPLETED 2-7-84 DRILLING METHOD HSA

ELEV.	DESCRIPTION	SUBSTRATA	DEPTH	SAMPLES					NOTES
		DEPTH	SCALE	BLOWS FT.	NO.	TYPE	RECOV.	QP	
739.4	Brn. clayey silt, wf. tr. f. sand, occas. organic fibers moist	0.0	30						
738.1	Brn. silty sand	-	-	2-5-7	1	ss	18"	1.6	
726.3	Brn. silty sand, wf. tr. f. sand moist	3.1	-	2-3-5	2	ss	17	1.4	
721.0	Brn. clayey silt, wf. tr. f. sand moist	8.4	-	3-5-5	3	ss	18	3.2	WATER 2-7-84
728.5	Brn. clayey silt, wf. tr. f. sand moist	10.9	-	2-3-3	4	ss	18	1.8	DD 13.0 11.4 5' BAR 19.0 3.4 5' AAR ----- WL 12.0 8:30 8 2-8-84
722.0	Brn. gray clayey silt, wf. tr. f. sand, sm. gray silt pockets moist	17.4	-	2-2-2	5	ss	18	1.2	Screen 21.5' - Gravel 21.5' - Bentonite 15' - Clay & Bentonite 13.5'-4.0' 2" PVC pipe 16 4.9' stick up Bentonite cement grout 4.0' - Plug 2.0' - Standpipe 3.0'
719.6	Brn. sandy silt, wf. occas. f. sand lens wet very moist	19.8	-	1-2-2	7	ss	18	1.2	Baled well at 5:15pm 2-9-84 11.0' water le



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LOG OF BORING

CONTRACTED WITH HANSON ENGINEERS
PROJECT NAME HUTSONVILLE POWER STATION
LOCATION PER PLAN
DATUM HAMMER WT. 140# HAMMER DROP 30" HOLE DIA. 8"
SURFACE ELEV. CORE DIA. CASING
DATE STARTED 2-7-84 COMPLETED 2-8-84 DRILLING METHOD HSA

ELEV.	DESCRIPTION	STRATA		DEPTH	SAMPLES					NOTES
		DEPTH	SCALE		BLOWS	FT.	NO.	TYPE	RECOV.	
439.9		0.0	30							
417.9	Br. silty sand wet	21.5		0-0-0	0		SS	18"	1.1	
	END OF BORING 21.5'									

TSD 000089



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LOG OF BORING

CONTRACTED WITH	HANSON ENGINEERS	BORING NO.	M-9					
PROJECT NAME	HUTSONVILLE POWER STATION	CONTRACT NO.						
LOCATION	33.0' E. OF STAKE							
DATUM	HAMMER WT. 140#	HAMMER DROP 30"	HOLE DIA. 8"					
SURFACE ELEV.	CORE DIA.	CASING						
DATE STARTED	2-14-84	COMPLETED	2-14-84					
		DRILLING METHOD	HSA					
ELEV.	DESCRIPTION	SAMPLES	NOTES					
STRATA	DEPTH	DEPTH	SCALE					
DEPTH	BLOWS FT.	NO.	TYPE	RECOV.	QP			
452.0	0.0	30						
451.2	See #A	0.8						
450.7	See #B	1.3						
	Brn. silty sand, wf. coal refuse, occas. f-m gravel fill moist	3.4		5-10-10	1 ss	18"	2.3	
448.6	Brn. sandy silt, wf. f-m gravel concrete	5		4-19-	2 ss	14	--	#A Brn.-blv f-sand, wf. coal refuse, 5.0" si
446.1	fill moist	5.0		18				wf. f. sand, organic fibers fill wet
	Brn. sandy silt, wf. ash coal refuse, tr. clay fill moist	8.1		2-1-2	3 ss	16	2.2	#B Brn. f-m sa wf. silt fill moist Water 2-14-84
443.9	Gray sandy silt, wf. occas. f. gravel	10		2-2-1	4 ss	10	1.0	DD 8.0 1:15pm BAR 17.0 2:30pm AAR --- WL 9.0 4:15pm
441.4	wet	0.6						Concrete fragme 3.5'-4.0'
	Brn. f. sand saturated	10		0-1-1	5 ss	8	--	2.6'-3.0.
438.6		3.4						Cobbles, concrete
	Gray clayey silt, wf. f. sand, occas. f. gravel	15		0-3-3	6 ss	14	2.3	Screen 18.5'-8. 2" PVC pipe 8.5
436.5		5.5						3.0 stick up Gravel 18.0'-8. Bentonite 8.0'- Cement Grout 6.
435.6	Br. m-c. sand, wf. f- c gravel wet	16.4		18-72-	7 ss	13	4.5	
	Brn. sandstone	18.8		22/1"				Plug 2.0'-8. Standpipe
				100/3"	8 ss	0	--	
	END OF BORING 18.8'	-20						

TSD 000090

Project Name/No. AmerenCIPS - Hutsonville				249-3	Boring No. MW-3D	Start Date 10/6/98	Page 1		
Driller AEC, Indianapolis, IN		Logged by: Steve Mueller/STMI			End Date 10/6/98		Depth to Water ~6 Feet		
Boring Depth 25.5 Feet		Boring Diameter 8* Inches		Surface Elevation 453.7 Feet	Drill Method HSA/air-rotary		Northing 3860.230		
Well Depth 25.1 Feet		Well Diameter 2-in. I.D.		TOC Elev. 455.28 Feet	Sample Method 2-ft. split-spoon		Easting 3952.034		
Sample	Blows/6 inches	Sample Depth (ft)	Recovery (%)	Graphic Log	Classification	Description			
Well Completion									
Comments									
	1, 2, 3, 6	—	75	ML	SANDY SILT, little fine-grained gravel, trace coal fragments, medium stiff, dark brown, moist (topsoil)		5-ft by 4-in square steel stick-up casing to ~1.8 ft; concrete seal 0-3 ft.		
	4, 4, 6, 4	—	88	SP	SAND, well sorted/rounded, fine-grained, quartz, loose, light brown, to medium brown, saturated below 6 ft		Bentonite/cement grout 3-16 ft; 1/4-in bentonite chips 16-17 ft.		
	1, 2, 3, 5	5	75	SW-GW	SILTY SAND & GRAVEL, poorly sorted, medium-grained sand, fine-grained subangular-to subround gravel, loose, light gray, saturated				
	2, 2, 2, 10	63	—	Ss	SANDSTONE, fine-grained, quartz				
	2, 2, 3, 5	50	—	END OF BORING - 25.5 feet			Sch. 40 PVC casing flush-threaded to 0.01-in factory-slotted PVC screen 20.1-25.1 ft; #7 fine silica sand 17-18 ft; #5 silica sand pack 18-25.5 ft.		
		25	—						
* 4-in diam. borehole drilled 16-25.5 ft using air-hammer.									

TSD 000091

Project Name/No. AmerenCIPS - Hutsonville				249-3	Boring No. MW-7D	Start Date 10/5/98	Page 1
Driller AEC, Indianapolis, IN			Logged by: Steve Mueller/STMI				End Date 10/5/98
Boring Depth 45.0 Feet	Boring Diameter 8 Inches		Surface Elevation 437.5 Feet		Drill Method HSA	Northing 3175.915	Depth to Water ~10 Feet
Well Depth 44.3 Feet	Well Diameter 2-in I.D.		TOC Elev. 438.45 Feet	Sample Method 2-ft. split-spoon		Easting 5676.110	
Sample	Blows/6 inches	Sample Depth (ft)	Recovery (%)	Graphic Log	Classification	Description	Well Completion
	1, 1, 2, 3	5	75			CLAYEY SILT, medium plasticity, trace roots fibers, soft, medium brown, moist, saturated below 10 ft.	
	1, 1, 1, 2	10	100		ML		
	1, 1, 2, 3	15	100				
	0, 0, 1, 2	20	100		SP	SILTY SAND, well sorted/rounded, fine-grained, quartz, grades from clayey silt above, loose, medium brown, saturated	
	3, 3, 4, 9	25	75			SILTY SAND & GRAVEL, well sorted medium-grained quartz sand, trace coarse sand, fine-grained angular to subangular gravel, medium dense, pale brown, saturated	Bentonite/cement grout 3-35 ft.
	5, 8, 6, 8	30	75		SP- GP		

TSD 000092

Project Name/No: AmerenCIPS - Hutsonville				Boring No. MW-7D	Start Date 10/5/98	Page 2
Driller AEC, Indianapolis, IN		Logged by: Steve Mueller/STMI			End Date 10/5/98	Depth to Water ~10 Feet
Boring Depth 45.0. Feet		Boring Diameter 8 Inches		Surface Elevation 437.5 Feet	Drill Method HSA	Northing 3175.915
Well Depth 44.3 Feet		Well Diameter 2-in I.D.		TOC Elev. 438.45 Feet	Sample Method 2-ft. split-spoon	Easting 5676.110
Sample	Blows/6 inches	Sample Depth (ft)	Recovery (%)	Graphic Log	Description	Well Completion
	sand heave	0	0			
	sand heave	40	0			
	16, 25, 7, 11	45	ML		CLAYEY SILT, medium plasticity, trace sand, stiff, brown, moist END OF BORING -45 feet	Sch. 40 PVC casing flush-threaded to 0.01-in factory-slotted PVC screen 39.3-44.3 ft; #7 fine silica sand 35-38 ft; #5 silica sand pack 38- 45 ft.
		50				
		55				
		60				
		65				

TSD 000093

Project Name/No. AmerenCIPS - Hutsonville				249-3	Boring No. MW-10	Start Date 10/7/98	Page 1
Driller AEC, Indianapolis, IN			Logged by: Steve Mueller/STMI			End Date 10/7/98	Depth to Water ~2.5 Feet
Boring Depth 11 Feet		Boring Diameter 8 Inches		Surface Elevation 452.9 Feet	Drill Method HSA	Northing 4730.478	
Well Depth 10.7 Feet		Well Diameter 2-in I.D.		TOC Elev. 454.23 Feet	Sample Method 2-ft. split-spoon	Easting 2559.807	
Sample	Blows/6 Inches	Sample Depth (ft)	Recovery (%)	Graphic Log	Classification	Description	Well Completion
							Comments
	1, 2, 2, 2	-	50		ML	CLAYEY SILT, vegetated with grass, soft, dark brown to black, moist (topsoil) SILTY SAND, well sorted/rounded, fine-grained, quartz, loose, yellowish orange with dark orange lamina (2-3 mm), saturated below ~2.5 ft	5-ft by 4-in square steel stick-up casing to ~1.5 ft.
	1, 2, 2, 6	-	50	SP	SILTY SAND, well sorted/rounded, fine-grained, quartz, laminated, dense, light gray to rust colored, predominantly light gray below 7.5 ft, saturated (weathered bedrock)	Bentonite/cement grout 0-3 ft; 1/4-in bentonite chips 3-4 ft.
	1, 2, 6, 25	5	100	SP	SANDSTONE, fine-grained, quartz	Sch. 40 PVC casing flush-threaded to 0' factory-slotted PVC screen 5.7-10.7 ft; #5 silica sand pack 4-11 ft.
	5, 20, 25, 50	-	63	Ss		
		10				END OF BORING -11 feet	
		15					
		20					
		25					
		30					

TSD 000094

Project Name/No. AmerenCIPS - Hutsonville				249-3	Boring No. MW-10D	Start Date 10/7/98	Page 1
Driller AEC, Indianapolis, IN		Logged by: Steve Mueller/STMI				End Date 10/7/98	Depth to Water ~2.5 Feet
Boring Depth 21.5 Feet		Boring Diameter 8 Inches.		Surface Elevation 452.9 Feet		Drill Method HSA	Northing 4729.427
Well Depth 21.3 Feet		Well Diameter 2-in I.D.		TOC Elev. 454.65 Feet		Sample Method see MW-10 log	Easting 2564.715
Sample	Blows/6 Inches	Sample Depth (ft)	Recovery (%)	Graphic Log	Classification	Description	
		see MW-10		ML	SP	CLAYEY SILT*, vegetated with grass, soft, dark brown to black, moist (topsoil) SILTY SAND*, well sorted/rounded, fine-grained, quartz, loose, yellowish orange with dark orange lamina (2-3 mm), saturated below ~2.5 ft	
		5		SP	SP	SILTY SAND*, well sorted/rounded, fine-grained, quartz, laminated; dense, light gray to rust colored, predominantly light gray below 7.5 ft, saturated (weathered bedrock)	
		10		SP	Ss	SANDSTONE, fine-grained, quartz, becomes medium-grained, trace gravel clasts, increasingly well cemented/hard (very difficult to auger) below 20 ft.	
		drill cuts				Sch. 40 PVC casing flush-threaded to 0.01-in factory-slotted PVC screen 16.3-21.3 ft; #7 silica sand 14-15 ft; #5 silica sand pack 15-21.5 ft.	
		20	1"			END OF BORING - 21.5 feet	
		25				* based on MW-10 boring log	
		30					

TSD 000095

Project Name/No. AmerenCIPS - Hutsonville				249-3	Boring No. MW-11	Start Date 10/6/98	Page 1
Driller AEC, Indianapolis, IN			Logged by: Steve Mueller/STMI				End Date 10/7/98
Boring Depth 15.0 Feet		Boring Diameter 8-Inches		Surface Elevation 443.8 Feet	Drill Method HSA	Depth to Water ~6 Feet	
Well Depth 14.5 Feet		Well Diameter 2-in I.D.		TOC Elev. 445.45 Feet	Sample Method 2-ft. split-spoon	Northing 3371.329	
Sample	Blows/6 inches	Sample Depth (ft)	Recovery (%)	Graphic Log	Classification	Description	Well Completion
							Comments
	1, 2, 3, 4	63		ML	SANDY SILT, little fine-grained gravel, trace coal fragments, medium stiff, medium brown, moist (topsoil)		5-ft by 4-in square steel stick-up casing to ~2.0 ft.
	1, 2, 6, 8	63		SM	SILTY SAND, medium- to coarse-grained, quartz, loose, light brown, moist		
	3, 5, 25, 50	75		SW-GW	SILTY SAND & GRAVEL, poorly sorted, dense, light brown, saturated		Bentonite/cement grout 0-3 ft; 1/4-in bentonite chips 3-4 ft.
					SANDSTONE		
		10		Ss			
		15			END OF BORING - 15 feet		
		20					
		25					
		30					

TSD 000096

Project Name/No. AmerenCIPS - Hutsonville				Boring No. MW-12	Start Date 10/8/98	Page 1
Driller AEC, Indianapolis, IN		Logged by: Steve Mueller/STMI			End Date 10/8/98	Depth to Water ~12 Feet
Boring Depth 17 Feet		Boring Diameter 8 Inches		Surface Elevation 455.5 Feet	Drill Method HSA	Northing 4053.583
Well Depth 16.9 Feet		Well Diameter 2-in I.D.		TOC Elev. 456.74 Feet	Sample Method 2-ft. split-spoon	Easting 4637.976
Sample	Blows/6 inches	Sample Depth (ft)	Recovery (%)	Graphic Log	Description	Well Completion
				Classification		Comments
	1, 1, 1, 1	63	63	ML	SANDY SILT, little clay, soft, dark brown, moist (topsoil) Coal Ash	5-ft by 4-in square steel stick-up casing to ~1.5 ft.
	2, 3, 10, 8	100	100	GM	SILTY SAND & GRAVEL, poorly sorted, medium dense, light brown, moist (fill)	
	1, 1, 2, 3	5	63	SP	SAND, well sorted/rounded, fine-grained, quartz, loose, light brown, moist	
	2, 2, 4, 3	75	75		SAND, poorly sorted, fine-to coarse-grained, subangular to subround, quartz, trace fine gravel, loose, light brown, saturated below ~12 ft	Bentonite/cement grout 0-3.5 ft; 1/4-in bentonite chips 3.5-5 ft.
	1, 2, 3, 2	50	50			
	1, 1, 1, 2	10	75			
	1, 2, 2, 3	75	75	SW		Sch. 40 PVC casing flush-threaded to 0.01-in factory-slotted PVC screen 6.9-16.9 ft; #7 fine silica sand 5-6 ft; #5 silica sand pack 6-17 ft.
	2, 3, 3, 4	15	100			
	10, 10, 35, 50	50	50	ML	SILT, stiff, light brown, moist END OF BORING - 17 feet (bedrock)	
		20				
		25				
		30				

TSD 000097

Project Name/No. AmerenCIPS - Hutsonville				249-3	Boring No. MW-13	Start Date 10/6/98	Page 1
Driller AEC, Indianapolis, IN			Logged by: Steve Mueller/STMI			End Date 10/6/98	Depth to Water ~7 Feet
Boring Depth 16.5 Feet		Boring Diameter 8 Inches		Surface Elevation 456.4 Feet	Drill Method HSA	Northing 3961.759	
Well Depth 16.0 Feet		Well Diameter 2-in I.D.		TOC Elev. 458.03 Feet	Sample Method 2-ft. split-spoon	Easting 4241.200	
Sample	Blows/6 inches	Sample Depth (ft)	Recovery (%)	Graphic Log	Classification	Description	Well Completion
							Comments
	1, 2, 3, 5	-	25	SM	SILTY SAND, with gravel, loose, dark brown, moist (topsoil)		5-ft by 4-in square steel stick-up casing to ~2.0 ft; concrete 0-3 ft.
		5		SP	SAND*, well sorted/rounded, fine- to medium-grained, quartz, light brown, saturated below ~9 ft.		
		10			* based on drill cuttings and geologic log for geoprobe GP-4		
	1, 2, 2, 2	50	50	SW-GW	CLAYEY SAND & GRAVEL, poorly sorted, fine- to coarse-grained sand, fine-grained subangular gravel, loose, light brown, saturated		Bentonite/cement grout 3-6.3 ft; 1/4-in bentonite chips 6.3-7 ft.
		15		Ss	SANDSTONE		
		20			END OF BORING - 16.5 feet		Sch. 40 PVC casing flush-threaded to 0.01-in factory-slotted PVC screen 9-14 ft; #7 fine silica sand 7-8 ft; #5 silica sand pack 8-16.5 ft.
		25					
		30					Unslotted casing/sediment sump 14-16 ft.

TSD 000098

Page 1 of 1

Facility/Project Name <i>IREN Energy Generating - Hutsonville Power Plant</i>				License/Permit/Monitoring Number <i>MW-IIR</i>			Boring Number <i>MW-IIR</i>									
Boring Drilled By (Firm name and name of crew chief) <i>Boart Longyear Randy Radke</i>				Date Drilling Started <i>10/03/01</i>		Date Drilling Completed <i>10/03/01</i>		Drilling Method <i>HSA</i>								
Facility Well No.	Unique Well No.	Common Well Name	Final Static Water Level Feet MSL <i>440.920 Feet MSL</i>		Surface Elevation <i>440.920 Feet MSL</i>		Borehole Diameter <i>8.25 inches</i>									
Boring Location State Plane <i>3217.083 4654.729</i>			Feet N <i>3217.083</i>	Feet E <i>4654.729</i>	Lat Long	Local Grid Location (If applicable)										
County <i>Crawford</i>					Civil Town/City/ or Village <i>Hutsonville</i>											
Sample	Number and Type	Length Att. & Recovered (in)	Blow Counts	Depth in Feet	Soil/Rock Description And Geologic Origin For Each Major Unit		USCS	Graphic Log	Well Diagram	P10/F10	Soil Properties				RGD/Comments	
					Compressive Strength	Moisture Content					Liquid Limit	Plasticity Index	P 200			
MW-IIR 0-2	I8	2 3 4 6		1	0'-5' FILL gray with orange mottling, coarse sand with clay, dry friable		FILL									
MW-IIR 2.5-4.5	I8	3 4 6 6		2	grades to sand with gravel, coarse		SP									
MW-IIR 7	I10	3 4 4 5		4	5'-8' SAND, orange, poorly graded, coarse		SP									
MW-IIR 7.5-8.5	I4	2 3 4 3		6	8'-10' SAND with GRAVEL brown, poorly graded, rounded, fine gravel/coarse sand		SP	O O O O O O O O								
MW-IIR 10-12	I8	2 2 3 2		8	10'-11'6" SAND, poorly graded, medium to coarse		SP									
MW-IIR 2.5-14.5	I20	2 3 3 3		10	11'6"-16' SAND with GRAVEL brown, poorly graded, rounded, fine gravel/coarse sand		SP	O O O O								
MW-IIR 15-17	I3	50/3		12	EOB @ 16' Auger Refusal											
				14												
				16												
				18												
				20												
				22												
I hereby certify that the information on this form is true and correct to the best of my knowledge.																
Signature <i>Mark S. Gilman</i>				Firm <i>Natural Resource Technology, Inc.</i>												

TSD 000099

Page 1 of 2

Facility/Project Name <i>AMEREN Energy Generating - Hutsonville Power Plant</i>				License/Permit/Monitoring Number <i>MW-14</i>			Boring Number <i>MW-14</i>							
Boring Drilled By (Firm name and name of crew chief) <i>Boart Longyear Randy Radke</i>				Date Drilling Started <i>10/03/01</i>		Date Drilling Completed <i>10/03/01</i>		Drilling Method <i>HSA</i>						
Facility Well No.	Unique Well No.	Common Well Name		Final Static Water Level Feet MSL		Surface Elevation 440.930 Feet MSL		Borehole Diameter 8.25 inches						
Boring Location State Plane <i>2811.508 5325.781</i>				Lat Long <i>Feet N Feet E</i>		Local Grid Location (if applicable) <input type="checkbox"/> N <input type="checkbox"/> E <input type="checkbox"/> S <input type="checkbox"/> W								
County <i>Crawford</i>						Civil Town/City/ or Village <i>Hutsonville</i>								
Sample Number and Type	Length Att. & Recovered (in)	Blow Counts	Depth in Feet	Soil/Rock Description And Geologic Origin For Each Major Unit	USCS	Graphic Log	Wall Diagram	PID/FID	Soil Properties				P 200	ROD/ Comments
									Compressive Strength	Moisture Content	Liquid Limit	Plasticity Index		
MW-14 2.5-4.5	18	2 3 2 3	2	0'-7'6" <u>SILT</u> , brown (10YR 4/3), moist, non-plastic	ML									
MW-14 5-7	18	1 1 2 2	4		ML									
MW-14 7.5-9.5	18	1 2 1 2	6		ML									
MW-14 10-12	24	1 1 1 1	8	7'6"-12'6" <u>SILT with SAND</u> , brown (10YR 4/3), low plasticity, moist	ML									
MW-14 12.5-14.5	18	1 1 1 2	10	yellowish brown (10YR 5/4), increase plasticity to medium	ML									
MW-14 15-17	22	1 1 1 1	12		CL									
MW-14 17.5-19.5	18	1 1 1 1	14	12'6"-18'6" <u>LEAN CLAY</u> , brown (7.5YR 4/2), 10-15% grey/orange mottling, medium plasticity	CL									
MW-14 20-22	18	1 1 1 1	16		SM									
MW-14 22.5-24.5	20	2 2 3 3	18	18'6"-26' <u>SAND WITH SILT</u> , wet, non-plastic	SP									
I hereby certify that the information on this form is true and correct to the best of my knowledge.														
Signature 				Firm <i>Natural Resource Technology, Inc.</i>										

TSD 000100

Facility/Project Name AMEREN Energy Generating - Hutsonville Power Plant				License/Permit/Monitoring Number			Boring Number TW				
Boring Drilled By (Firm name and name of crew chief) Boart Longyear Randy Radke				Date Drilling Started 10/02/01		Date Drilling Completed 10/02/01		Drilling Method HSA			
Facility Well No.		Unique Well No.	Common Well Name	Final Static Water Level Feet MSL		Surface Elevation 437.814 Feet MSL	Borehole Diameter 8.25 inches				
Boring Location State Plane 3717.203 Feet N 5805.471 Feet E				Lat Long		Local Grid Location (if applicable)					
County Crawford						Civil Town/City/ or Village Hutsonville					
Number and Type	Length Att & Recovered (in)	Blow Counts	Depth in Feet	Soil/Rock Description And Geologic Origin For Each Major Unit	USCS	Graphic Log	Well Diagram	Soil Properties			RQD/ Comments
								PID/FID	Compressive Strength	Moisture Content	
				0'-5'8" SILT with SAND, very dark brown (IOYR 2/2), grades from topsoil, trace organics throughout	ML						
TW 2.5-4.5	20	22 33	2 4								
TW 5-7	18	21 24	6	5'8"-23' LEAN CLAY, brown (IOYR 4/3), medium plasticity, moist							
TW 7.5-9.5	16	11 12	8	weak red (2.5Y 5/3), trace orange mottling							
TW 10-12	20	11 11	10								
TW 2.5-14.5	18	11 11	12	trace horizontal fracture, wet							
TW 15-17	18	11 11	14	CL							
TW 7.5-18.5	20	1/24	16	5-10% fine sand							
TW 20-22	24	1/24	18	very dark gray (2.5Y 3/1), trace wood and white shell fragments							
TW 22.5-24.5	10	1/24	20								
			22	23'-25'6" SAND, very dark gray (2.5Y 3/1),	SP						

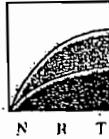
I hereby certify that the information on this form is true and correct to the best of my knowledge.

Signature

Firm

Natural Resource Technology, Inc.

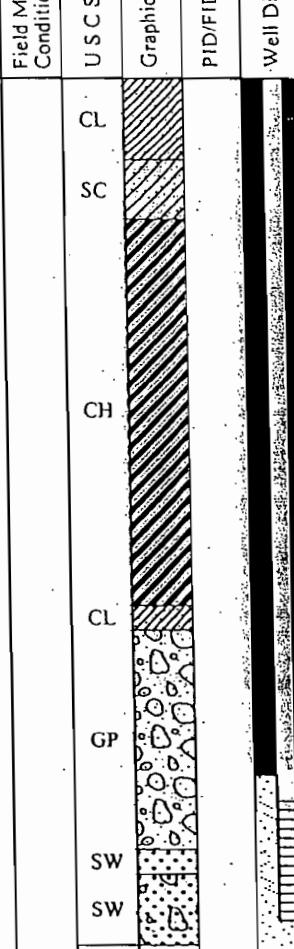
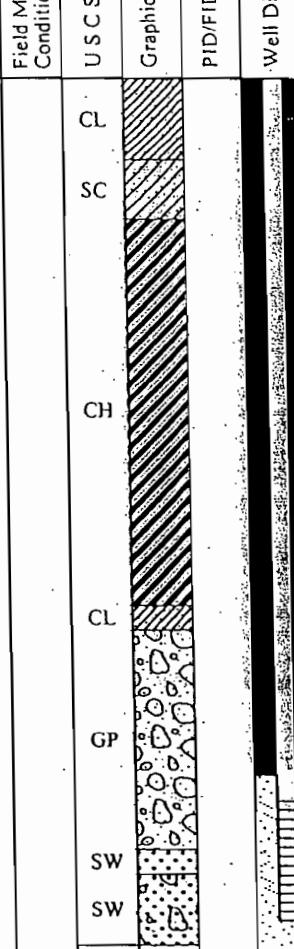
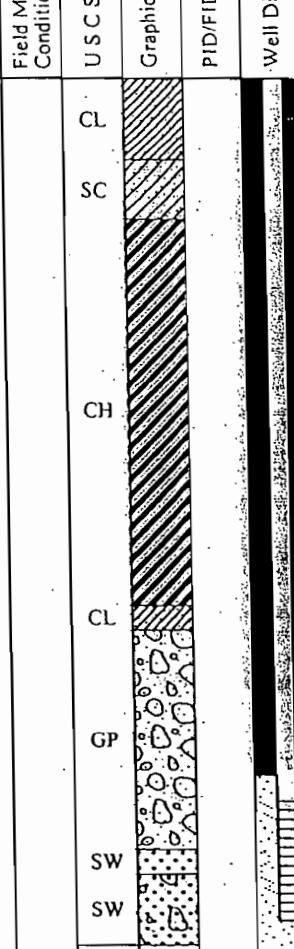
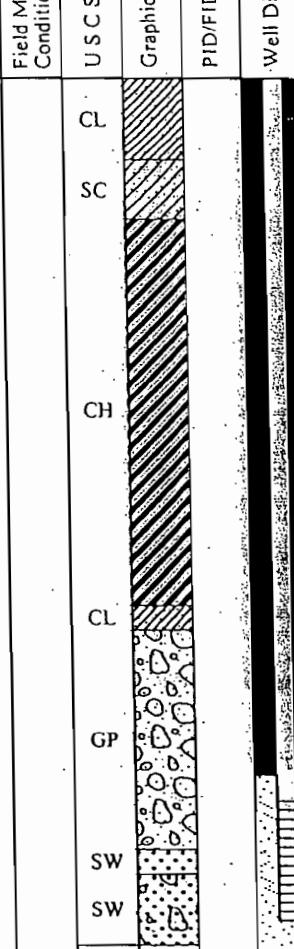
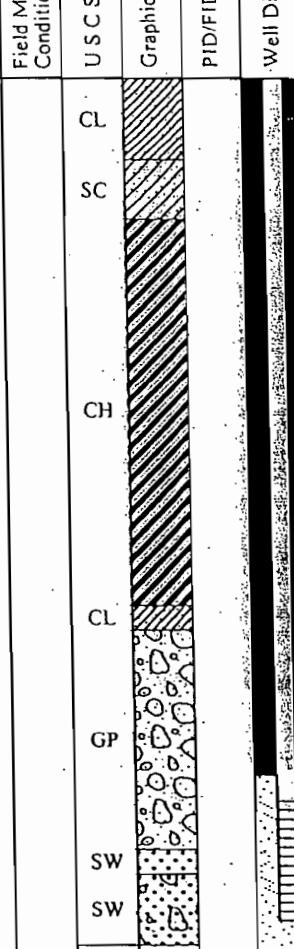
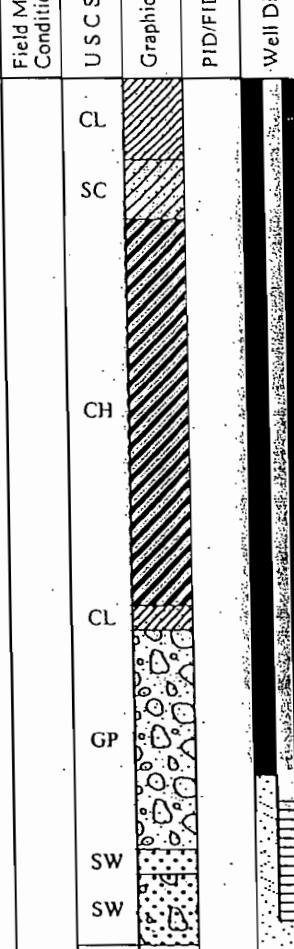
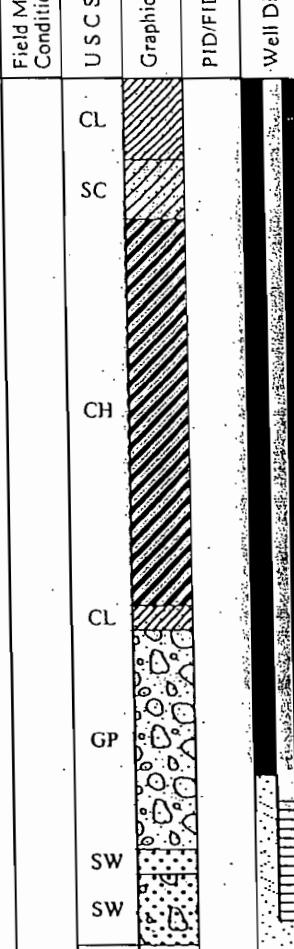
Sample	Num and Type	Length Alt. & Recovered (in)	Blow Counts	Depth in Feet	Soil/Rock Description And Geologic Origin For Each Major Unit				USCS	Graphic Log	Well Diagram	PID/FID	Soil Properties				RQD/ Comments
					Compressive Strength	Moisture Content	Liquid Limit	Plasticity Index					Compressive Strength	Moisture Content	Liquid Limit	Plasticity Index	
		10	1/24		medium, loose, wet				SP								P 200
TW 25-27		18	2 2 2 2	26	25'6"-26' LEAN CLAY, as above	CL			SP								RQD/ Comments
					26'-27'6" SAND with GRAVEL, poorly graded, coarse sand, fine gravel, rounded	SP	O O O O O O										
TW 27.5-29.5		20	3 5 0 10	28	27'6"-31' SAND, gray/black and white, poorly graded, medium to coarse, increased coarseness with depth	SP											
					31'-32'6" SAND and GRAVEL, coarse sand, poorly graded, fine gravel, rounded	SP	O O O O O O										
TW 32.5-34.5		12	4 6 0 9	32	32'6"-39'6" SAND, gray, poorly graded, medium to coarse, 5-15% gravel	SP											
						SP											
TW 35-37		24	2 2 3 4	36													
TW 37.5-39.5		24	3 6 6 10	38													
				40	EOB @ 39'6"												
				42													
				44													
				46													
				48													
				50													
				52													
				54													
				56													
				58													
				60													
				62													



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SOIL BORING LOG

Page 1 of 1

Facility/Project Name Ameren Hutsonville Power Station Drilling			License/Permit/Monitoring Number		Boring Number TW-115s				
Boring Drilled By: Name of crew chief (first, last) and Firm. Steve Boart Longyear			Date Drilling Started 5/1/2004	Date Drilling Completed 5/1/2004	Drilling Method hollow stem auger				
Unique Well No.	Well ID No.	Common Well Name TW-115s	Final Static Water Level Feet MSL 438.4 Feet MSL	Surface Elevation 438.4 Feet MSL	Borehole Diameter 8.3 inches				
Local Grid Origin <input checked="" type="checkbox"/> (estimated: <input type="checkbox"/>) or Boring Location <input type="checkbox"/>			Local Grid Location						
State Plane N, E S/C/N 1/4 of 1/4 of Section T R			Lat <input type="text"/> ° <input type="text"/> ' <input type="text"/> "	Long <input type="text"/> ° <input type="text"/> ' <input type="text"/> "	<input checked="" type="checkbox"/> N <input type="checkbox"/> E <input type="checkbox"/> S <input type="checkbox"/> N <input type="checkbox"/> W				
Facility ID		County	State		Civil Town/City/ or Village Hutsonville				
Sample		Soil/Rock Description And Geologic Origin For Each Major Unit			RQD/ Comments/ Lab Test				
Number and Type	Length Att. & Recovered (in)	Blow Counts	Depth From Surface (feet)	Hand Pen (tsf)	Field Moisture Condition	U S C S Symbol	Graphic Log	PID/FID (ppm)	Well Diagram
						CL			
						SC			
						CH			
						CL			
						GP			
						SW			
						SW			
									
0'-36' Drilled without sampling-see log TW-115d for complete description.									
END OF BORING AT 36' Well set at 35'									

I hereby certify that the information on this form is true and correct to the best of my knowledge.

Signature


Firm
Natural Resource Technology, Inc.
Paula Richardson 23713 W. Paul Road, Unit D, Pewaukee, WI 53072

Tel: (262) 523-9000
Fax: (262) 523-9001

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TSD 000104



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Page 1 of 5

Facility/Project Name Ameren Hutsonville Power Station Drilling			License/Permit/Monitoring Number		Boring Number TW-115d							
Boring Drilled By: Name of crew chief (first, last) and Firm Steve Boart Longyear			Date Drilling Started 4/29/2004	Date Drilling Completed 5/1/2004	Drilling Method hsa, core							
Unique Well No.	Well ID No.	Common Well Name TW-115d	Final Static Water Level Feet MSL	Surface Elevation 438.4 Feet MSL	Borehole Diameter 8.3 inches							
Local Grid Origin <input checked="" type="checkbox"/> (estimated: <input type="checkbox"/>) or Boring Location <input type="checkbox"/>			Local Grid Location									
State Plane N, E S/C/N			Lat <input type="text"/> ° <input type="text"/> "	<input checked="" type="checkbox"/> N <input checked="" type="checkbox"/> E								
1/4 of	1/4 of Section	T R	Long <input type="text"/> ° <input type="text"/> "	898052.56 Feet <input type="checkbox"/> S 1176882.3 Feet <input type="checkbox"/> W								
Facility ID		County	State		Civil Town/City/ or Village Hutsonville							
Sample	Number and Type	Length Att. & Recovered (in)	Blow Counts	Depth From Surface (feet)	Soil/Rock Description And Geologic Origin For Each Major Unit	Hand Pen (ls)	Field Moisture Condition	USCS Symbol	Graphic Log	PID/FID (ppm)	Well Diagram	RQD/Comments/Lab Test
1 SS	24 12				0'-3.5' SANDY CLAY , very dark greyish brown (10 YR 3/2), very fine sand, moist			CL				
2 SS	24 24				3.5'-6' CLAYEY SAND mottled grey-brown to tan, very fine sand, moist			SC				
3 SS	24 24			5	6'-22' FAT CLAY , brown (10 YR 4/3), soft, plastic, moist			CH				
4 SS	24 24				wet at 13'							
5 SS	24 24			10								
6 SS	24 4											
7 SS	24 24											
8 SS	24 24			15								

I hereby certify that the information on this form is true and correct to the best of my knowledge.

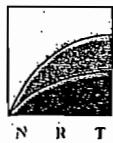
Signature
Paula Richardson

Firm Natural Resource Technology, Inc.
Paula Richardson 23713 W. Paul Road, Unit D, Pewaukee, WI 53072

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Boring Number TW-115 Page 2 of 5

Sample Number and Type	Length Att. & Recovered (in)	Blow Counts	Depth From Surface (feet)	Soil/Rock Description And Geologic Origin For Each Major Unit	Hand Pen (lsf)	Field Moisture Condition	U S C S Symbol	Graphic Log	PID/FID (ppm)	Well Diagram	RQD/Comments/ Lab Test
9 SS	24	24		6'-22' <u>FAT CLAY</u> , brown (10 YR 4/3), soft, plastic, moist at 16' color change to olive grey (5Y 5/2)							
10 SS	24	24					CH				
11 SS	24	24	20	at 19.8' 2" sand seam, very fine sand 20'-22' trace very fine sand							
12 SS	24	24		22'-22.9' <u>SANDY CLAY</u>			CL				
13 SS	24	0	25	22.9'-32' <u>POORLY GRADED GRAVEL WITH SAND</u> , olive grey (5Y 5/2), rounded, very fine to fine sand							
14 SS	24	8									
15 SS	24	7	30								
16 SS	24	4									
17 SS	24	5		32'-33' <u>WELL GRADED SAND</u> fine to coarse, trace rounded gravel			SW				
18 SS	24	14	35	33'-36' <u>WELL GRADED SAND WITH GRAVEL</u> , very fine to coarse sand, fine to medium gravel, rounded			SW				
19 SS	24	8		36'-39' <u>POORLY GRADED SAND</u> very fine to medium, trace gravel, rounded							
20 SS	24	14									
21 SS	24	11	40	39'-40' <u>WELL GRADED SAND WITH GRAVEL</u> , fine to coarse gravel and sand			SP				



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Boring Number TW-115 Page 3 of 5

Sample Number and Type	Length Att. & Recovered (in)	Blow Counts	Depth From Surface (feet)	Soil/Rock Description And Geologic Origin For Each Major Unit	Hand Pen (lsf)	Field Moisture Condition	U S C S Symbol	Graphic Log	PID/FID (ppm)	Well Diagram	RQD/Comments/ Lab Test
22 SS	24 12			40'-42' WELL GRADED GRAVEL WITH SAND, fine to coarse sand, fine to coarse gravel, rounded 42'-58' WELL GRADED SAND fine to coarse sand, trace gravel, rounded			GW				
23 SS	24 12		45	2" gravelly sand seam, fine to coarse gravel at 44'							
24 SS	24 13										
25 SS	24 14		50								
	24 13										
27 SS	24 16										
28 SS	24 15		55								
29 SS	24 9										
30 SS	24 3		60	58'-70' WELL GRADED GRAVEL WITH SAND, fine to coarse sand, fine to coarse gravel, rounded							
31 SS	24 7										
32 SS	24 24										
33 SS	24 12		65								
34 SS	24 4										

TSD 000107



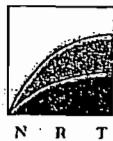
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Boring Number TW-1150 Page 4 of 5

Sample Number and Type	Length Att. & Recovered (in)	Blow Counts	Depth From Surface (feet)	Soil/Rock Description And Geologic Origin For Each Major Unit	Hand Pen (lsf)	Field Moisture Condition	U S C S Symbol	Graphic Log	PID/FID (ppm)	Well Diagram	RQD/Comments/ Lab Test
35 SS	24 0			58'-70' WELL GRADED GRAVEL WITH SAND, fine to coarse sand, fine to coarse gravel, rounded			GW				
36 SS	24 6		70	70'-74' WELL GRADED SAND fine to coarse			SW				
37 SS	24 4										
38 SS	24 0		75	74'-88' Logged from cuttings, WELL GRADED GRAVEL WITH SAND fine to coarse sand, fine to coarse gravel			GW				Gravel starts coming up in cuttings.
39 SS	24 0										
40 SS	24 0		80								
41 SS	24 0										
42 SS	24 0		85								
43 SS	24 0										
44 SS	24 0		90								
45 SS	24 12			88'-90' WELL GRADED SAND very fine to medium			SW				
CORE	180		90	90'-105' SHALE, grey-blue, friable, moist			SHALE				

TSD 000108



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N R T

Boring Number TW-115dage 5 of 5

Sample				Soil/Rock Description And Geologic Origin For Each Major Unit						RQD/Comments/Lab Test
Number and Type	Length Att. & Recovered (in)	Blow Counts	Depth From Surface (feet)	Hand Pen (ls)	Field Moisture Condition	U S C S Symbol	Graphic Log	PID/FID (ppm)	Well Diagram	
			90'-105'							
			SHALE, grey-blue, friable, moist							
			95							
			100							
			105							
			END OF BORING AT 105' Well set at 87'							

TSD 000109



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SOIL BORING LOG

Page 1 of 4

Facility/Project Name Ameren Hutsonville Power Station Drilling			License/Permit/Monitoring Number		Boring Number TW-116							
Boring Drilled By: Name of crew chief (first, last) and Firm Steve Boart Longyear			Date Drilling Started 4/26/2004	Date Drilling Completed 4/28/2004	Drilling Method hsa, core							
Unique Well No.	Well ID No. TW-116	Common Well Name	Final Static Water Level Feet MSL 437.5 Feet MSL	Surface Elevation 437.5 Feet MSL	Borehole Diameter 8.3 inches							
Local Grid Origin <input checked="" type="checkbox"/> (estimated: <input type="checkbox"/>) or Boring Location <input type="checkbox"/> State Plane N, E S/C/N			Lat 43° 10' 00"	Local Grid Location ☒ N ☒ E								
1/4 of I/4 of Section , T R			Long 89° 03' 41.384" E	896034.1384 Feet <input type="checkbox"/> S 1175442.33 Feet <input type="checkbox"/> W								
Facility ID		County	State		Civil Town/City/ or Village Hutsonville							
Sample	Number and Type	Length Att. & Recovered (in)	Blow Counts	Depth From Surface (feet)	Soil/Rock Description And Geologic Origin For Each Major Unit	Hand Pen (lsf)	Field Moisture Condition	USCS Symbol	Graphic Log	PID/FID (ppm)	Well Diagram	RQD/Comments/ Lab Test
1 SS	24 24				0'-3.5' <u>SILT</u> , very dark greyish brown (10 YR 3/2), rootlets to 6", firm, slightly moist			ML				
2 SS	24 12				3.5'-4.8' <u>SILTY CLAY</u> , very dark greyish brown, firm, slightly moist			CL/ML				
3 SS	24 24			5	4.8'-16' <u>FAT CLAY</u> , dark yellowish brown (10YR 4/4), soft, moist			CH				
4 SS	24 24			10								
5 SS	24 24											
6 SS	24 24											
7 SS	24 24											
8 SS	24 24			15	at 14' very moist							

I hereby certify that the information on this form is true and correct to the best of my knowledge.

Paula Richardson

Paula Richardson

Firm **Natural Resource Technology, Inc.**

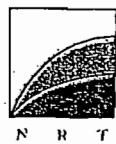
23713 W. Paul Road, Unit D, Pewaukee, WI 53072

Tel: (262) 523-9000

Fax: (262) 523-9001

Template: NRT BORING LOG - Project: 1375 LOGS.GPJ

TSD 000110



Natural
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N R T

Boring Number TW-116 Page 2 of 4

Sample	Number and Type	Length At & Recovered (in)	Blow Counts	Depth From Surface (feet)	Soil/Rock Description And Geologic Origin For Each Major Unit	Hand Pen (ts)	Field Moisture Condition	U S C S Symbol	Graphic Log	PID/FID (ppm)	Well Diagram	RQD/Comments/ Lab Test
9 SS		24 24			16'-20.5' <u>SANDY LEAN CLAY</u> , olive brown (2.5 Y 4/3), very fine sand, soft, wet			CL				
10 SS		24 24		20	color change to dark grey (2.5 Y 4/1) 20.5'-26.5' <u>CLAYEY SAND</u> , dark grey, very fine sand, wet			SC				
11 SS		24 24		25	26.5'-30' <u>CLAYEY GRAVEL</u> , fine gravel, few shell fragments, wet			GC				
12 SS		24 18		30	30'-60' <u>WELL GRADED SAND</u> , olive brown (2.5 Y 4/4), fine to coarse, subangular to rounded, wet			SW				
13 SS		24 12		35								
14 SS		24 0		40								

TSD 000111



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Boring Number TW-116 Page 3 of 4

TSD 000112



Natural
Resource
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Boring Number TW-116 Page 4 of 4

Sample	Blow Counts	Depth From Surface (feet)	Soil/Rock Description And Geologic Origin For Each Major Unit	Hand Pen (lsf)	Field Moisture Condition	U S C S Symbol	Graphic Log	PID/FID (ppm)	Well Diagram	RQD/Comments/Lab Test
			60'-79' <u>SHALE</u> grey-blue, slightly moist, friable							
		70								
		75								
			coal seam at 79', bit plugged-no water circulation for coring							
			END OF BORING AT 79.2' Well set at 30'							

TSD 000113



N R T
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SOIL BORING LOG

Page 1 of 4

Facility/Project Name Ameren Hutsonville Power Station Drilling			License/Permit/Monitoring Number		Boring Number TW-117							
Boring Drilled By: Name of crew chief (first, last) and Firm Steve Boart Longyear			Date Drilling Started 4/28/2004	Date Drilling Completed 4/29/2004	Drilling Method hollow stem auger							
Unique Well No.	Well ID No.	Common Well Name TW-117	Final Static Water Level Feet MSL	Surface Elevation 435.0 Feet MSL	Borehole Diameter 8.3 inches							
Local Grid Origin <input checked="" type="checkbox"/> (estimated: <input type="checkbox"/>) or Boring Location <input type="checkbox"/>			Local Grid Location									
State Plane N, E S/C/N 1/4 of 1/4 of Section , T R			Lat ° ' "	Long ° ' "	<input checked="" type="checkbox"/> N <input checked="" type="checkbox"/> E 895267.78 Feet <input type="checkbox"/> S 1179053.33 Feet <input type="checkbox"/> W							
Facility ID		County	State		Civil Town/City/ or Village Hutsonville							
Sample Number and Type	Length Att. & Recovered (in)	Blow Counts	Depth From Surface (feet)	Soil/Rock Description And Geologic Origin For Each Major Unit		Hand Pen (ls)	Field Moisture Condition	U S C S Symbol	Graphic Log	PID/FID (ppm)	Well Diagram	RQD/ Comments/ Lab Test
1 SS	24 12			0'-6' SANDY LEAN CLAY , dark olive brown (2.5 Y 3/3), very fine sand, slightly moist				CL				
2 SS	24 24			6'-7.8' FAT CLAY , dark olive brown, high toughness and plasticity, moist				CH				
3 SS	24 0		5									
4 SS	24 24			7.8'-25' POORLY GRADED SAND dark yellowish brown (10 YR 4/4), very fine, wet				SP				
5 SS	24 10		10									
6 SS	24 12											
7 SS	24 10		15									

I hereby certify that the information on this form is true and correct to the best of my knowledge.

Signature 	Firm Natural Resource Technology, Inc. Paula Richard 23713 W. Paul Road, Unit D, Pewaukee, WI 53072	Tel: (262) 523-9000 Fax: (262) 523-9001
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Template: NRT BORING LOG - Project: 1375 LOGS.GPJ

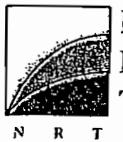
TSD 000114



Natural
Resource
Technology

Boring Number TW-117 Page 2 of 4

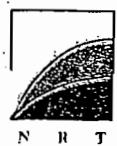
Sample Number and Type	Length Att. & Recovered (in)	Blow Counts	Depth From Surface (feet)	Soil/Rock Description And Geologic Origin For Each Major Unit	Hand Pen (tsf)	Field Moisture Condition	U.S.C.S Symbol	Graphic Log	PID/FID (ppm)	Well Diagram	RQD/Comments/ Lab Test
				7.8'-25' POORLY GRADED SAND dark yellowish brown (10 YR 4/4), very fine, wet trace shell fragments at 16'							
8 SS	24 0		20				SP				
9 S	24 8		25	25'-26' WELL GRADED SAND fine to medium, coarsens downward 26'-35' WELL GRADED GRAVEL, trace sand and shell fragments, rounded			SW				
10 SS	24 4		30	grey clay in shoe of split spoon			GW				
11 SS	24 6		35	35'-60' WELL GRADED SAND fine to coarse			SW				
12 SS	24 5		40								



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Boring Number TW-117 Page 3 of 4

Sample Number and Type	Length Att. & Recovered (in)	Blow Counts	Depth From Surface (feet)	Soil/Rock Description And Geologic Origin For Each Major Unit							
					Hand Pen (lsn)	Field Moisture Condition	U S C S Symbol	Graphic Log	PID/FID (ppm)	Well Diagram	RQD/ Comments/ Lab Test
X				35'-60' WELL GRADED SAND fine to coarse							
13 SS	24 14		45								
14 SS	24 17		50			SW.					
15 SS	24 0		55								
16 SS	24 0		60	60'-75' Logged from drill cuttings POORLY GRADED GRAVEL, coarse, rounded			GP				Went to larger sample interval due to drilling conditions.
			65								



Natural
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Boring Number TW-117 Page 4 of 4

Sample		Soil/Rock Description And Geologic Origin For Each Major Unit								
Number and Type	Length Att. & Recovered (in)	Blow Counts	Depth From Surface (feet)	Hand Pen (isf)	Field Moisture Condition	U S C S Symbol	Graphic Log	PID/FID (ppm)	Well Diagram	RQD/Comments/ Lab Test
17	24 0		60'-75' Logged from drill cuttings, <u>POORLY GRADED GRAVEL</u> , coarse, rounded			GP				No samples attempted after 77 feet due to drilling conditions.
			70							
			75			SW				
			75'-90' Logged from drill cuttings, <u>WELL GRADED SAND WITH GRAVEL</u>							
			80							
			85							
			90							
18	6 2		90'-90.5' SHALE			SHALE				
<u>END OF BORING AT 90.5' Well set at 20'</u>										

TSD 000117



Natural
Resource
Technology

SOIL BORING LOG

Page 1 of 2

Facility/Project Name Ameren Hutsonville Power Station Drilling			License/Permit/Monitoring Number		Boring Number TW-118						
Boring Drilled By: Name of crew chief (first, last) and Firm Steve Boat Longyear			Date Drilling Started 5/4/2004	Date Drilling Completed 5/4/2004	Drilling Method hollow stem auger						
Unique Well No.	Well ID No.	Common Well Name TW-118	Final Static Water Level Feet MSL	Surface Elevation 437.0 Feet MSL	Borehole Diameter 8.3 inches						
Local Grid Origin <input checked="" type="checkbox"/> (estimated: <input type="checkbox"/>) or Boring Location <input type="checkbox"/> State Plane N, E S/C/N 1/4 of 1/4 of Section, T R			Lat ° ' "	Local Grid Location Lat ° ' " N Long ° ' " E 898090.86 Feet <input type="checkbox"/> S1177978.73 Feet <input type="checkbox"/> W							
Facility ID		County	State		Civil Town/City/ or Village Hutsonville						
Sample	Soil/Rock Description And Geologic Origin For Each Major Unit			Hand Pen (tsf)	Field Moisture Condition	USCS Symbol	Graphic Log	PID/FID (ppm)	Well Diagram	RQD/ Comments/ Lab Test	
1 SS 24 24	Blow Counts	Depth From Surface (feet)	0'-3' <u>SILT</u> , brown (7.5 YR 4/2)			ML					
2 SS 24 24			3'-5' dark reddish grey (5 YR 4/2), trace sand wet at 4'			SW					
3 SS 24 24		5	5'-6' <u>WELL GRADED SAND</u> light reddish brown (5 YR 6/3), medium to fine			ML					
4 SS 24 24			6'-7.5' <u>SILT</u> , brown (7.5 YR 4/2)			SP-SM					
5 SS 24 18		5	7.5'-10' <u>POORLY GRADED SAND WITH SILT</u>			SP					
6 SS 24 24		10	10'-26' <u>POORLY GRADED SAND</u> brown (7.5 YR 5/2), medium grained								
7 SS 24 24											
8 SS 24 16		15									

I hereby certify that the information on this form is true and correct to the best of my knowledge.

Signature

Firm **Natural Resource Technology, Inc.**
Paula Richardson 23713 W. Paul Road, Unit D, Pewaukee, WI 53072

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Fax: (262) 523-9001

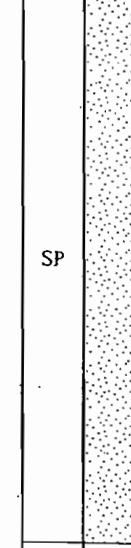
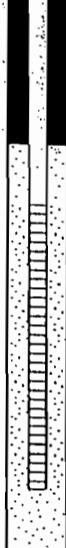
Template: NRT BORING LOG - Project: 1375 LOGS.GPJ

TSD 000118



Natural
Resource
Technology

Boring Number TW-118 Page 2 of 2

Sample	Number and Type	Length At & Recovered (in)	Blow Counts	Depth From Surface (feet)	Soil/Rock Description And Geologic Origin For Each Major Unit	Hand Pen (lsf)	Field Moisture Condition	U S C S Symbol	Graphic Log	PID/FID (ppm)	Well Diagram	RQD/Comments/Lab Test
9 SS		24 12		20	10'-26' POORLY GRADED SAND brown (7.5 YR 5/2), medium grained			SP				
10 SS		24 12		25	@ 22' coarse sand with few gravel							
					END OF BORING AT 26' Well set at 25'							

TSD 000119



Natural
Resource
Technology

SOIL BORING LOG

Page 1 of 5

Facility/Project Name Ameren Hutsonville Power Station Drilling			License/Permit/Monitoring Number		Boring Number TW-119					
Boring Drilled By: Name of crew chief (first, last) and Firm Steve Boart Longyear			Date Drilling Started 5/1/2004	Date Drilling Completed 5/3/2004	Drilling Method hsa, core					
Unique Well No.	Well ID No.	Common Well Name TW-119	Final Static Water Level Feet MSL	Surface Elevation 435.4 Feet MSL	Borehole Diameter 8.3 inches					
Local Grid Origin <input checked="" type="checkbox"/> (estimated: <input type="checkbox"/>) or Boring Location <input type="checkbox"/>			Local Grid Location							
State Plane N, E S/C/N			Lat _____ ° _____'	<input checked="" type="checkbox"/> N <input checked="" type="checkbox"/> E						
1/4 of 1/4 of Section , T R			Long _____ ° _____'	896030.54 Feet <input type="checkbox"/> S 1181339.05 Feet <input type="checkbox"/> W						
Facility ID		County	State		Civil Town/City/ or Village Hutsonville					
Sample	Soil/Rock Description And Geologic Origin For Each Major Unit			Hand Pen (tsf)	Field Moisture Condition	U S C Symbol	Graphic Log	PID/FID (ppm)	Well Diagram	RQD/ Comments/ Lab Test
1 SS	24 18		0'-4' SILTY CLAY, very dark greyish brown (10 YR 3/2), firm, moist			CL/ML				
2 SS	24 20		color change to dark greyish brown (2.5 Y 4/2)							
3 SS	24 24	5	4'-11.7' FAT CLAY, dark greyish brown, soft, moist			CH				
4 SS	24 21		at 6' very moist							
5 SS	24 24		at 9' wet							
6 SS	24 24	10								
7 SS	24 16	15	11.7'-41' POORLY GRADED SAND mottled orange brown and grey brown, very fine, wet at 12' color change to dark yellowish brown (10 YR 4/4)			SP				

I hereby certify that the information on this form is true and correct to the best of my knowledge.

Signature
Paula Richardson

Firm
Natural Resource Technology, Inc.
Paula Richardson 23713 W. Paul Road, Unit D, Pewaukee, WI 53072

Tel: (262) 523-9000
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Template: NRT BORING LOG - Project: J375 LOGS.GPJ

TSD 000120



Natural
Resource
Technology

N R T

Boring Number TW-119 Page 2 of 5

Sample	Number and Type	Length Att. & Recovered.(in)	Blow Counts	Depth From Surface (feet)	Soil/Rock Description And Geologic Origin For Each Major Unit	Hand Pen (isf)	Field Moisture Condition	U S C S Symbol	Graphic Log	PID/FID (ppm)	Well Diagram	RQD/Comments/Lab Test
8	SS	24 6		20	11.7'-41' POORLY GRADED SAND mottled orange brown and grey brown, very fine, wet							
9	SS	24 0		25								
10	SS	24 11		30	very fine to medium sand			SP				
11	SS	24 12		35	very fine to fine sand							
12	SS	24 22		40								

TSD 000121



Natural
Resource
Technology

N R T

Boring Number TW-119 Page 3 of 5

Sample Number and Type	Length Att. & Recovered (in)	Blow Counts	Depth From Surface (feet)	Soil/Rock Description And Geologic Origin For Each Major Unit	Hand Pen (is)	Field Moisture Condition	U S C S Symbol	Graphic Log	PID/FID (npm)	Well Diagram	RQD/Comments/Lab Test
				41'-45' WELL GRADED SAND very fine to coarse, trace rounded gravel			SW				
13 SS	24 17		45	45'-60' POORLY GRADED SAND very fine to medium			SP				
14 SS	24 12		50								
15 SS	24 0		55								
16 SS	24 0		60	60'-80' Logged by drill cuttings, WELL GRADED SAND WITH GRAVEL to WELL GRADED GRAVEL WITH SAND			SW				Gravel starts coming up in cuttings
17 SS	24 0		65								

TSD 000122



Natural
Resource
Technology

Boring Number TW-119 Page 4 of 5

Sample	Number and Type	Length Att. & Recovered (in)	Blow Counts	Depth From Surface (feet)	Soil/Rock Description And Geologic Origin For Each Major Unit	Hand Pen (lsf)	Field Moisture Condition	U S C S Symbol	Graphic Log	PID/FID (ppm)	Well Diagram	RQD/Comments/ Lab Test
18	SS	24 0		70	60'-80' Logged by drill cuttings, <u>WELL GRADED SAND WITH GRAVEL to WELL GRADED GRAVEL WITH SAND</u>							
19	S	24 0		75								
20	CORI	84 24		80	80'-100' SHALE, grey to black, laminated, poorly lithified, no circulation of drilling water							
21	CORI	72 30		85								
				90								



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Boring Number TW-119 Page 5 of 5

Sample	Number and Type	Length Att. & Recovered (in)	Blow Counts	Depth From Surface (feet)	Soil/Rock Description And Geologic Origin For Each Major Unit		Hand Pen (is?)	Field Moisture Condition	U S C S Symbol	Graphic Log	PID/FID (ppm)	Well Diagram	RQD/Comments/Lab Test
22	CORI	84 54		80'-100' SHALE, grey to black, laminated, poorly lithified, no circulation of drilling water									
				95									
				100	END OF BORING AT 100' Well set at 20'								

TSD 000124



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Resource
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SOIL BORING LOG

Page 1 of 2

Facility/Project Name Ameren Hutsonville Power Station Drilling			License/Permit/Monitoring Number		Boring Number TW-120						
Boring Drilled By: Name of crew chief (first, last) and Firm Steve Boart Longyear			Date Drilling Started 5/3/2004	Date Drilling Completed 5/4/2004	Drilling Method hollow stem auger						
Unique Well No.	Well ID No.	Common Well Name TW-120	Final Static Water Level Feet MSL	Surface Elevation 446.8 Feet MSL	Borehole Diameter 8.3 inches						
Local Grid Origin <input checked="" type="checkbox"/> (estimated: <input type="checkbox"/>) or Boring Location <input type="checkbox"/>			Local Grid Location								
State Plane N, E S/C/N 1/4 of 1/4 of Section, T R			Lat. ° _____	Long. ° _____	<input checked="" type="checkbox"/> N <input checked="" type="checkbox"/> E 898614.91 Feet <input type="checkbox"/> S1180157.14 Feet <input type="checkbox"/> W						
Facility ID		County	State		Civil Town/City/ or Village Hutsonville						
Sample	Soil/Rock Description And Geologic Origin For Each Major Unit			Hand Pen (tsi)	Field Moisture Condition	U S C S Symbol	Graphic Log	PID/FID (ppm)	Well Diagram	RQD/ Comments/ Lab Test	
1 SS	24 17	Blow Counts	Depth From Surface (feet)	0'-0.5' TOPSOIL 0.5'-14' POORLY GRADED SAND brownish yellow (10 YR 6/6), medium			SP	14'-15'			
2 SS	24 15										
3 SS	24 15										
4 SS	24 12			color change to reddish yellow (7.5 YR 6/6), moist							
5 SS	24 10			14'-36' POORLY GRADED SAND WITH GRAVEL, reddish yellow, medium sand, rounded gravel, moist			SP	14'-15'			

I hereby certify that the information on this form is true and correct to the best of my knowledge.

Signature
Paula Richardson

Firm
Natural Resource Technology, Inc.
Paula Richardson 23713 W. Paul Road, Unit D, Pewaukee, WI 53072

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Template: NRT BORING LOG - Project: 1375 LOGS.GPJ

TSD 000125



Natural
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Boring Number TW-120 Page 2 of 2

Sample	Number and Type	Length Att. & Recovered (in)	Blow Counts	Depth From Surface (feet)	Soil/Rock Description And Geologic Origin For Each Major Unit			RQD/Comments/Lab Test		
					Hand Pen (ft)	Field Moisture Condition	U S C S Symbol	Graphic Log	PID/FID (ppm)	Well Diagram
6 SS		24 24		14'-36'	<u>POORLY GRADED SAND WITH GRAVEL</u> , reddish yellow, medium sand, rounded gravel, moist					
				wet at 19'						
7 SS		24 24		20						
				25						
8 SS		24 24		30						
				35						
9 SS		24 24		34'-36'	coarse sand					
				35						
					<u>END OF BORING AT 36' Well set at 35'</u>					

TSD 000126

APPENDIX A-2

**MONITORING WELL COMPLETION REPORTS
AND ABANDONMENT LOG**



MONITORING WELLS

M-1

ELEVATION 456.5

PIPE & SCREEN

7' pipe	459.5 - 452.5
5' screen	452.5 - 447.5

BACKFILL MATERIALS

concrete grout collar	456.5 - 455.0
bentonite seal	455.0 - 453.5
1/8" gravel pack	453.5 - 447.4

M-2

ELEVATION 453.3

PIPE & SCREEN

8' pipe	456.3 - 448.3
13' screen	448.3 - 435.3

BACKFILL MATERIALS

concrete grout collar	453.3 - 451.3
bentonite seal	451.3 - 449.3
1/8" gravel pack	449.3 - 431.8

TSD 000128

NOW IN OUR FOURTEENTH YEAR OF SERVICE

1525 SOUTH SIXTH STREET ■ SPRINGFIELD, ILLINOIS 62703-2886 ■ 217/788-2450 ■ TWX 910-242-0519

SPRINGFIELD, ILLINOIS ■ BOSTON ■ CHICAGO ■ MINNEAPOLIS ■ PORTLAND



MONITORING WELLS

M-3

ELEVATION 452.1

PIPE & SCREEN

7.9' pipe	455.6 - 447.7
5' screen	447.7 - 442.7

BACKFILL MATERIALS

concrete grout collar	452.1 - 450.1
bentonite seal	450.1 - 448.1
1/8" gravel pack	442.7 - 448.1

M-4

ELEVATION 454.4

PIPE & SCREEN

8' pipe	457.4 - 449.4
7.5' screen	449.4 - 441.9

BACKFILL MATERIALS

concrete grout collar	454.4 - 452.4
bentonite seal	452.4 - 450.4
1/8" gravel pack	450.4 - 441.0

TSD 000129

NOW IN OUR THIRTY EIGHT YEAR OF SERVICE

1525 SOUTH SIXTH STREET ■ SPRINGFIELD, ILLINOIS 62703-2886 ■ 217/788-2450 ■ TWX 910-242-0519

PRINCIPALS: RICHARD L. HANSON - ROBERT W. HANSON - ROBERT C. HANSON



MONITORING WELLS

M-5

ELEVATION 452.3

PIPE & SCREEN

8' pipe	455.3 - 447.3
13' screen	447.3 - 434.3

BACKFILL MATERIALS

concrete grout collar	452.3 - 450.3
bentonite seal	450.3 - 448.3
1/8" gravel pack	448.3 - 433.1

M-6

ELEVATION 438.9

PIPE & SCREEN

10' pipe	443.9 - 433.9
6.4' screen	433.9 - 427.5

BACKFILL MATERIALS

concrete grout collar	438.9 - 436.9
bentonite seal	436.9 - 434.9
1/8" gravel pack	434.9 - 427.5

TSD 000130

NOW IN OUR THIRTY EIGHT YEAR OF SERVICE

1525 SOUTH SIXTH STREET ■ SPRINGFIELD, ILLINOIS 62703-2886 ■ 217/788-2450 ■ TWX 910-242-0519

SPRINGFIELD ■ ILLINOIS ■ PEORIA ■ MOLINE ■ DODGE CITY



MONITORING WELLS

M-7

ELEVATION 437.9

PIPE & SCREEN

20' pipe	442.9 - 422.9
10' screen	422.9 - 412.9

BACKFILL MATERIALS

concrete grout collar	437.9 - 435.9
bentonite & auger cutting	435.9 - 425.9
bentonite seal	425.9 - 423.9
1/8" gravel pack	423.9 - 412.9

M-8

ELEVATION 439.4

PIPE & SCREEN

21.4' pipe	444.3 - 422.9
5.0' screen	422.9 - 417.9

BACKFILL MATERIALS

concrete grout collar	439.4 - 437.4
bentonite & auger cutting	437.4 - 425.9
bentonite seal	425.9 - 423.9
1/8" gravel pack	423.9 - 417.9

TSD 000131

WE'RE IN OUR THIRTY EIGHT YEAR OF SERVICE

1525 SOUTH SIXTH STREET ■ SPRINGFIELD, ILLINOIS 62703-2886 ■ 217/788-2450 ■ TWX 910-242-0519

SPRINGFIELD, ILLINOIS - DECATUR, ILLINOIS - CHAMPAIGN, ILLINOIS



MONITORING WELLS

M-9

ELEVATION 452.0

PIPE & SCREEN

11.5' pipe	455.0 - 443.5
10' screen	443.5 - 433.5

BACKFILL MATERIALS

concrete grout collar	452 - 450
bentonite, cement & sand	450 - 446
bentonite seal	446 - 444
1/8" gravel pack	444 - 433.2

TSD 000132

NOW IN OUR THIRTY EIGHT YEAR OF SERVICE

1525 SOUTH SIXTH STREET ■ SPRINGFIELD, ILLINOIS 62703-2886 ■ 217/788-2450 ■ TWX 910-242-0519



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MONITORING WELL CONSTRUCTION

Facility/Project Name A. On Hutsonville Power Station Drilling		Local Grid Location of Well 898046.72 ft. <input checked="" type="checkbox"/> N. <input type="checkbox"/> S. 1176886.34 ft. <input checked="" type="checkbox"/> E. <input type="checkbox"/> W.	Well Name TW-115s
Fac. License, Permit or Monitoring No.		Local Grid Origin <input checked="" type="checkbox"/> (estimated: <input type="checkbox"/>) or Well Location <input type="checkbox"/> Lat. _____ " Long. _____ "	Unique Well No. _____ Well Number _____
Facility ID		St. Plane _____ ft. N. _____ ft. E.	Date Well Installed 05/01/2004
Type of Well		Section Location _____ 1/4 of _____ 1/4 of Sec. _____ T. _____ R. _____	Well Installed By: (Person's Name and Firm) Steve Boart Longyear
Distance from Waste/Source ft.		Location of Well Relative to Waste/Source u <input type="checkbox"/> Upgradient s <input type="checkbox"/> Sidegradient d <input checked="" type="checkbox"/> Downgradient n <input type="checkbox"/> Not Known	Gov. Lot Number _____
A. Protective pipe, top elevation		ft. MSL _____	1. Cap and lock? <input checked="" type="checkbox"/> Yes <input type="checkbox"/> No
B. Well casing, top elevation		440.89 ft. MSL _____	2. Protective cover pipe: a. Inside diameter: 4.0 in. b. Length: 6.0 ft. c. Material: Steel <input checked="" type="checkbox"/> 0.4 Other <input type="checkbox"/>
C. Land surface elevation		438.4 ft. MSL _____	d. Additional protection? <input type="checkbox"/> Yes <input checked="" type="checkbox"/> No If yes, describe: _____ Bentonite <input checked="" type="checkbox"/> 3.0 Concrete <input type="checkbox"/> 0.1 Other <input type="checkbox"/>
D. Surface seal, bottom		437.4 ft. MSL or 1.0 ft. _____	3. Surface seal: _____
12. USCS classification of soil near screen:		GP <input type="checkbox"/> GM <input type="checkbox"/> GC <input type="checkbox"/> GW <input checked="" type="checkbox"/> SW <input type="checkbox"/> SP <input checked="" type="checkbox"/> SM <input type="checkbox"/> SC <input type="checkbox"/> ML <input type="checkbox"/> MH <input type="checkbox"/> CL <input type="checkbox"/> CH <input type="checkbox"/> Bedrock <input type="checkbox"/>	
13. Sieve analysis attached?		<input type="checkbox"/> Yes <input checked="" type="checkbox"/> No	
14. Drilling method used:		Rotary <input type="checkbox"/> 50 Hollow Stem Auger <input checked="" type="checkbox"/> 41 Other <input type="checkbox"/>	
15. Drilling fluid used:		Water <input type="checkbox"/> 0.2 Air <input type="checkbox"/> 0.1 Drilling Mud <input type="checkbox"/> 0.3 None <input checked="" type="checkbox"/> 9.9	4. Material between well casing and protective pipe: Bentonite <input type="checkbox"/> 3.0 Other <input type="checkbox"/>
16. Drilling additives used?		<input type="checkbox"/> Yes <input checked="" type="checkbox"/> No	
Describe _____			
17. Source of water (attach analysis, if required):		_____	
E. Bentonite seal, top		ft. MSL or _____ ft.	5. Annular space seal: a. Granular/Chipped Bentonite <input checked="" type="checkbox"/> 3.3 b. _____ Lbs/gal mud weight ... Bentonite-sand slurry <input type="checkbox"/> 3.5 c. _____ Lbs/gal mud weight ... Bentonite slurry <input type="checkbox"/> 3.1 d. _____ % Bentonite ... Bentonite-cement grout <input type="checkbox"/> 5.0 e. _____ ft ³ volume added for any of the above f. How installed: Tremie <input type="checkbox"/> 0.1 Tremie pumped <input type="checkbox"/> 0.2 Gravity <input type="checkbox"/> 0.8
F. Fine sand, top		410.4 ft. MSL or 28.0 ft.	6. Bentonite seal: a. Bentonite granules <input type="checkbox"/> 3.3 b. <input type="checkbox"/> 1/4 in. <input type="checkbox"/> 3/8 in. <input type="checkbox"/> 1/2 in. Bentonite chips <input type="checkbox"/> 3.2 c. _____ Other <input type="checkbox"/>
G. Filter pack, top		409.4 ft. MSL or 29.0 ft.	7. Fine sand material: Manufacturer, product name & mesh size a. #7 Badger _____
H. Screen joint, top		408.4 ft. MSL or 30.0 ft.	8. Filter pack material: Manufacturer, product name & mesh size a. #40 Badger _____
I. Well bottom		403.4 ft. MSL or 35.0 ft.	9. Well casing: Flush threaded PVC schedule 40 <input checked="" type="checkbox"/> 2.3 Flush threaded PVC schedule 80 <input type="checkbox"/> 2.4 Other <input type="checkbox"/>
J. Filter pack, bottom		402.4 ft. MSL or 36.0 ft.	10. Screen material: PVC a. Screen Type: Factory cut <input checked="" type="checkbox"/> 1.1 Continuous slot <input type="checkbox"/> 0.1 Other <input type="checkbox"/>
K. Borehole, bottom		402.4 ft. MSL or 36.0 ft.	b. Manufacturer Boart Longyear c. Slot size: 0.010 in. d. Slotted length: 5.0 ft.
L. Borehole, diameter		8.3 in.	11. Backfill material (below filter pack): None <input checked="" type="checkbox"/> 1.4 Other <input type="checkbox"/>
M. O.D. well casing		2.33 in.	
N. Well casing		2.00 in.	

I hereby certify that the information on this form is true and correct to the best of my knowledge.

Signature

Paula Richardson

Firm

Natural Resource Technology, Inc.

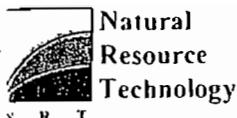
23713 W. Paul Road, Unit D, Pewaukee, WI 53072

Tel: (262) 523-9000

Fax: (262) 523-9001

Template: NRT WELL CONSTRUCTION - Project: 1375 LOGS.GPJ

TSD 000133



MONITORING WELL CONSTRUCTION

Facility/Project Name A. Huiserville Power Station Drilling Fac. License, Permit or Monitoring No.		Local Grid Location of Well 898052.56 ft. N. 1176882.3 ft. E. Local Grid Origin <input checked="" type="checkbox"/> (estimated: <input type="checkbox"/>) or Well Location <input type="checkbox"/> Lat. _____ " Long. _____ " or	Well Name TW-115d Unique Well No. _____ Well Number _____
Facility ID Type of Well Well Code 12/pz		St. Plane _____ ft. N, _____ ft. E. Section Location 1/4 of _____ 1/4 of Sec. _____ T. _____ R. _____	Date Well Installed 05/01/2004 Well Installed By: (Person's Name and Firm) Steve Boart Longyear
Distance from Waste/Source ft.		Location of Well Relative to Waste/Source u <input type="checkbox"/> Upgradient s <input type="checkbox"/> Sidegradient d <input checked="" type="checkbox"/> Downgradient n <input type="checkbox"/> Not Known Gov. Lot Number _____	
A. Protective pipe, top elevation _____ ft. MSL B. Well casing, top elevation _____ 440.80 ft. MSL C. Land surface elevation _____ 438.4 ft. MSL D. Surface seal, bottom _____ 437.4 ft. MSL or 1.0 ft.		<p>1. Cap and lock? <input checked="" type="checkbox"/> Yes <input type="checkbox"/> No</p> <p>2. Protective cover pipe: a. Inside diameter: 4.0 in. b. Length: 6.0 ft. c. Material: Steel <input checked="" type="checkbox"/> 04 Other <input type="checkbox"/> </p> <p>d. Additional protection? If yes, describe: _____ <input type="checkbox"/> Yes <input checked="" type="checkbox"/> No Bentonite <input checked="" type="checkbox"/> 3.0 Concrete <input type="checkbox"/> 01 Other <input type="checkbox"/> </p> <p>3. Surface seal: _____ Bentonite <input checked="" type="checkbox"/> 3.0 Concrete <input type="checkbox"/> 01 Other <input type="checkbox"/> </p> <p>4. Material between well casing and protective pipe: Sand Bentonite <input type="checkbox"/> 3.0 Other <input type="checkbox"/> </p> <p>5. Annular space seal: a. Granular/Chipped Bentonite <input checked="" type="checkbox"/> 3.3 b. _____ Lbs/gal mud weight ... Bentonite-sand slurry <input type="checkbox"/> 3.5 c. _____ Lbs/gal mud weight ... Bentonite slurry <input type="checkbox"/> 3.1 d. _____ % Bentonite ... Bentonite-cement grout <input type="checkbox"/> 5.0 e. _____ ft³ volume added for any of the above</p> <p>f. How installed: Tremie <input type="checkbox"/> 0.1 Tremie pumped <input checked="" type="checkbox"/> 0.2 Gravity <input type="checkbox"/> 0.8</p> <p>6. Bentonite seal: a. Bentonite granules <input type="checkbox"/> 3.3 b. <input type="checkbox"/> 1/4 in. <input checked="" type="checkbox"/> 3/8 in. <input type="checkbox"/> 1/2 in. Bentonite chips <input checked="" type="checkbox"/> 3.2 c. _____ Other <input type="checkbox"/> </p> <p>7. Fine sand material: Manufacturer, product name & mesh size a. #7 Badger b. Volume added: _____ ft³</p> <p>8. Filter pack material: Manufacturer, product name & mesh size a. #40 Badger b. Volume added: _____ ft³</p> <p>9. Well casing: Flush threaded PVC schedule 40 <input checked="" type="checkbox"/> 2.3 Flush threaded PVC schedule 80 <input type="checkbox"/> 2.4 Other <input type="checkbox"/> </p> <p>10. Screen material: PVC a. Screen Type: Factory cut <input checked="" type="checkbox"/> 1.1 Continuous slot <input type="checkbox"/> 0.1 Other <input type="checkbox"/> </p> <p>b. Manufacturer: Boart Longyear c. Slot size: 0.010 in. d. Slotted length: 5.0 ft.</p> <p>11. Backfill material (below filter pack): None <input type="checkbox"/> 1.4 Bentonite <input type="checkbox"/> 0.0 Other <input checked="" type="checkbox"/> </p>	
<p>12. USCS classification of soil near screen: GP <input type="checkbox"/> GM <input checked="" type="checkbox"/> GC <input type="checkbox"/> GW <input checked="" type="checkbox"/> SW <input type="checkbox"/> SP <input type="checkbox"/> SM <input type="checkbox"/> SC <input type="checkbox"/> ML <input type="checkbox"/> MH <input type="checkbox"/> CL <input type="checkbox"/> CH <input type="checkbox"/> Bedrock <input type="checkbox"/></p> <p>13. Sieve analysis attached? <input type="checkbox"/> Yes <input checked="" type="checkbox"/> No</p> <p>14. Drilling method used: Rotary <input type="checkbox"/> 5.0 Hollow Stem Auger <input checked="" type="checkbox"/> 4.1 rock core <input type="checkbox"/> Other <input checked="" type="checkbox"/> </p> <p>15. Drilling fluid used: Water <input checked="" type="checkbox"/> 0.2 Air <input type="checkbox"/> 0.1 Drilling Mud <input type="checkbox"/> 0.3 None <input type="checkbox"/> 9.9</p> <p>16. Drilling additives used? <input type="checkbox"/> Yes <input checked="" type="checkbox"/> No</p> <p>Describe _____</p> <p>17. Source of water (attach analysis, if required): Ameren well</p>			
E. Bentonite seal, top _____ 361.4 ft. MSL or 77.0 ft. F. Fine sand, top _____ 358.4 ft. MSL or 80.0 ft. G. Filter pack, top _____ 357.4 ft. MSL or 81.0 ft. H. Screen joint, top _____ 356.4 ft. MSL or 82.0 ft. I. Well bottom _____ 351.4 ft. MSL or 87.0 ft. J. Filter pack, bottom _____ 350.4 ft. MSL or 88.0 ft. K. Borehole, bottom _____ 333.4 ft. MSL or 105.0 ft. L. Borehole, diameter _____ 8.3 in. M. O.D. well casing _____ 2.33 in. N. Well casing _____ 2.00 in.			

I hereby certify that the information on this form is true and correct to the best of my knowledge.

Signature Paula Richardson Firm Natural Resource Technology, Inc.
 23713 W. Paul Road, Unit D, Pewaukee, WI 53072 Tel: (262) 523-9000
 Fax: (262) 523-9001

Template: NRT WELL CONSTRUCTION - Project: 1375 LOGS.GPJ



MONITORING WELL CONSTRUCTION

Facility/Project Name <u>Ameren Huskville Power Station Drilling</u>		Local Grid Location of Well 896034.1384 ft. N. <input checked="" type="checkbox"/> S. <input type="checkbox"/> 1175442.33 ft. E. <input checked="" type="checkbox"/> W. <input type="checkbox"/>	Well Name TW-116
Facility License, Permit or Monitoring No.		Local Grid Origin <input checked="" type="checkbox"/> (estimated: <input type="checkbox"/>) or Well Location <input type="checkbox"/> Lat. _____ " Long. _____ " or St. Plane _____ ft. N. _____ ft. E.	Unique Well No. _____ Well Number _____
Facility ID		Date Well Installed 04/28/2004	
Type of Well		Well Installed By: (Person's Name and Firm) Steve Boari Longyear	
Well Code 12/pz			
Distance from Waste/Source ft.		Location of Well Relative to Waste/Source <input type="checkbox"/> Upgradient <input checked="" type="checkbox"/> Sidegradient <input type="checkbox"/> Downgradient <input type="checkbox"/> Not Known	Gov. Lot Number _____
<p>A. Protective pipe, top elevation _____ ft. MSL 1. Cap and lock? <input checked="" type="checkbox"/> Yes <input type="checkbox"/> No</p> <p>B. Well casing, top elevation 439.77 ft. MSL 2. Protective cover pipe: a. Inside diameter: 4.0 in. b. Length: 6.0 ft. c. Material: Steel <input checked="" type="checkbox"/> 0.4 Other <input type="checkbox"/> _____</p> <p>C. Land surface elevation 437.5 ft. MSL 3. Surface seal: Bentonite <input checked="" type="checkbox"/> 3.0 Concrete <input type="checkbox"/> 0.1 Other <input type="checkbox"/> _____</p> <p>D. Surface seal, bottom 436.5 ft. MSL or 1.0 ft. 4. Material between well casing and protective pipe: Bentonite <input type="checkbox"/> 3.0 Sand <input type="checkbox"/> 0.1 Other <input type="checkbox"/> _____</p> <p>12. USCS classification of soil near screen: GP <input type="checkbox"/> GM <input checked="" type="checkbox"/> GC <input checked="" type="checkbox"/> GW <input type="checkbox"/> SW <input checked="" type="checkbox"/> SP <input type="checkbox"/> SM <input type="checkbox"/> SC <input checked="" type="checkbox"/> ML <input type="checkbox"/> MH <input type="checkbox"/> CL <input type="checkbox"/> CH <input type="checkbox"/> Bedrock <input type="checkbox"/></p> <p>13. Sieve analysis attached? <input type="checkbox"/> Yes <input checked="" type="checkbox"/> No</p> <p>14. Drilling method used: Rotary <input type="checkbox"/> 50 Hollow Stem Auger <input checked="" type="checkbox"/> 41 rock core <input type="checkbox"/> Other <input checked="" type="checkbox"/> _____</p> <p>15. Drilling fluid used: Water <input checked="" type="checkbox"/> 0.2 Air <input type="checkbox"/> 0.1 Drilling Mud <input type="checkbox"/> 0.3 None <input type="checkbox"/> 0.9</p> <p>16. Drilling additives used? <input type="checkbox"/> Yes <input checked="" type="checkbox"/> No Describe _____</p> <p>17. Source of water (attach analysis, if required): <u>Ameren well</u></p>			
E. Bentonite seal, top _____ ft. MSL or _____ ft.	5. Annular space seal: a. Granular/Chipped Bentonite <input checked="" type="checkbox"/> 3.3 b. _____ Lbs/gal mud weight ... Bentonite-sand slurry <input type="checkbox"/> 3.5 c. _____ Lbs/gal mud weight ... Bentonite slurry <input type="checkbox"/> 3.1 d. _____ % Bentonite ... Bentonite-cement grout <input type="checkbox"/> 5.0 e. _____ ft ³ volume added for any of the above f. How installed: Tremie <input type="checkbox"/> 0.1 Tremie pumped <input type="checkbox"/> 0.2 Gravity <input checked="" type="checkbox"/> 0.8		
F. Fine sand, top 414.5 ft. MSL or 23.0 ft.	6. Bentonite seal: a. Bentonite granules <input type="checkbox"/> 3.3 b. <input type="checkbox"/> 1/4 in. <input type="checkbox"/> 3/8 in. <input type="checkbox"/> 1/2 in. Bentonite chips <input type="checkbox"/> 3.2 c. _____ Other <input type="checkbox"/> _____		
G. Filter pack, top 413.5 ft. MSL or 24.0 ft.	7. Fine sand material: Manufacturer, product name & mesh size a. _____ #7 Badger b. Volume added _____ ft ³		
H. Screen joint, top 412.5 ft. MSL or 25.0 ft.	8. Filter pack material: Manufacturer, product name & mesh size a. _____ #40 Badger b. Volume added _____ ft ³		
I. Well bottom 407.5 ft. MSL or 30.0 ft.	9. Well casing: Flush threaded PVC schedule 40 <input checked="" type="checkbox"/> 2.3 Flush threaded PVC schedule 80 <input type="checkbox"/> 2.4 Other <input type="checkbox"/> _____		
J. Filter pack, bottom 406.5 ft. MSL or 31.0 ft.	10. Screen material: PVC a. Screen Type: Factory cut <input checked="" type="checkbox"/> 1.1 Continuous slot <input type="checkbox"/> 0.1 Other <input type="checkbox"/> _____		
K. Borehole, bottom 358.5 ft. MSL or 79.0 ft.	b. Manufacturer <u>Boart Longyear</u> c. Slot size: 0.010 in. d. Slotted length: 5.0 ft.		
L. Borehole, diameter 8.3 in.	11. Backfill material (below filter pack): None <input type="checkbox"/> 1.4 bentonite, stuff <input checked="" type="checkbox"/> 0.1 Other <input type="checkbox"/> _____		
M. O.D. well casing 2.33 in.			
N. Well casing 2.00 in.			

I hereby certify that the information on this form is true and correct to the best of my knowledge.

Signature

Paula Richardson

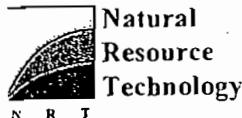
Firm

Natural Resource Technology, Inc.
23713 W. Paul Road, Unit D, Pewaukee, WI 53072

Tel: (262) 523-9000

Fax: (262) 523-9001

Template: NRT WELL CONSTRUCTION - Project: 1375 LOGS.GPJ



MONITORING WELL CONSTRUCTION

Facility/Project Name Arrowhead Hutsonville Power Station Drilling	Local Grid Location of Well 895267.78 ft. <input checked="" type="checkbox"/> N. <input type="checkbox"/> S. 1179053.33 ft. <input checked="" type="checkbox"/> E. <input type="checkbox"/> W.	Well Name TW-117
Facility ID Boart Longyear	Local Grid Origin <input checked="" type="checkbox"/> (estimated: <input type="checkbox"/>) or Well Location <input type="checkbox"/> Lat. _____ Long. _____	Unique Well No. _____ Well Number _____
Type of Well Water Well	St. Plane _____ ft. N. _____ ft. E. Section Location ____ 1/4 of ____ 1/4 of Sec. _____ T. _____ R. _____	Date Well Installed 04/29/2004
Well Code 12/pz Distance from Waste/ Source ft.	Location of Well Relative to Waste/Source u <input type="checkbox"/> Upgradient s <input checked="" type="checkbox"/> Sidegradient d <input type="checkbox"/> Downgradient n <input type="checkbox"/> Not Known	Gov. Lot Number _____
A. Protective pipe, top elevation _____ ft. MSL	1. Cap and lock? <input checked="" type="checkbox"/> Yes <input type="checkbox"/> No	
B. Well casing, top elevation 438.09 ft. MSL	2. Protective cover pipe: a. Inside diameter: 4.0 in. b. Length: .60 ft. c. Material: Steel <input checked="" type="checkbox"/> 0.4 Other <input checked="" type="checkbox"/> 0.5	
C. Land surface elevation 435.0 ft. MSL	d. Additional protection? <input type="checkbox"/> Yes <input checked="" type="checkbox"/> No If yes, describe: _____	
D. Surface seal, bottom 434.0 ft. MSL or 1.0 ft.	e. Surface seal: Bentonite <input checked="" type="checkbox"/> 3.0 Concrete <input type="checkbox"/> 0.1 Other <input type="checkbox"/> 0.5	
12. USCS classification of soil near screen: GP <input type="checkbox"/> GM <input type="checkbox"/> GC <input type="checkbox"/> GW <input type="checkbox"/> SW <input type="checkbox"/> SP <input checked="" type="checkbox"/> SM <input type="checkbox"/> SC <input type="checkbox"/> ML <input type="checkbox"/> MH <input type="checkbox"/> CL <input type="checkbox"/> CH <input type="checkbox"/> Bedrock <input type="checkbox"/>	f. Material between well casing and protective pipe: Bentonite <input type="checkbox"/> 3.0 Sand Other <input checked="" type="checkbox"/> 0.5	
13. Sieve analysis attached? <input type="checkbox"/> Yes <input checked="" type="checkbox"/> No	g. Annular space seal: a. Granular/Chipped Bentonite <input checked="" type="checkbox"/> 3.3 b. _____ Lbs/gal mud weight ... Bentonite-sand slurry <input type="checkbox"/> 3.5 c. _____ Lbs/gal mud weight ... Bentonite slurry <input type="checkbox"/> 3.1 d. _____ % Bentonite ... Bentonite-cement grout <input type="checkbox"/> 5.0 e. _____ ft ³ volume added for any of the above	
14. Drilling method used: Rotary <input type="checkbox"/> S.0 Hollow Stem Auger <input checked="" type="checkbox"/> 4.1 Other <input type="checkbox"/>	f. How installed: Tremie <input type="checkbox"/> 0.1 Tremie pumped <input type="checkbox"/> 0.2 Gravity <input checked="" type="checkbox"/> 0.8	
15. Drilling fluid used: Water <input type="checkbox"/> 0.2 Air <input type="checkbox"/> 0.1 Drilling Mud <input type="checkbox"/> 0.3 None <input checked="" type="checkbox"/> 9.9	g. Bentonite seal: a. Bentonite granules <input type="checkbox"/> 3.3 b. <input type="checkbox"/> 1/4 in. <input type="checkbox"/> 3/8 in. <input type="checkbox"/> 1/2 in. Bentonite chips <input type="checkbox"/> 3.2 c. _____ Other <input type="checkbox"/> 0.5	
16. Drilling additives used? <input type="checkbox"/> Yes <input checked="" type="checkbox"/> No	h. Fine sand material: Manufacturer, product name & mesh size a. _____ #7 Badger _____	
Describe _____	b. Volume added _____ ft ³	
17. Source of water (attach analysis, if required): _____	i. Filter pack material: Manufacturer, product name & mesh size a. _____ #40 Badger _____	
E. Bentonite seal, top _____ ft. MSL or _____ ft.	j. Well casing: Flush threaded PVC schedule 40 <input checked="" type="checkbox"/> 2.3 Flush threaded PVC schedule 80 <input type="checkbox"/> 2.4 Other <input type="checkbox"/> 0.5	
F. Fine sand, top 422.0 ft. MSL or 13.0 ft.	k. Screen material: _____ PVC a. Screen Type: Factory cut <input checked="" type="checkbox"/> 1.1 Continuous slot <input type="checkbox"/> 0.1 Other <input type="checkbox"/> 0.5	
G. Filter pack, top 421.0 ft. MSL or 14.0 ft.	l. Manufacturer Boart Longyear c. Slot size: 0.010 in. d. Slotted length: 5.0 ft.	
H. Screen joint, top 420.0 ft. MSL or 15.0 ft.	m. Backfill material (below filter pack): None <input type="checkbox"/> 1.4 Sluff Other <input checked="" type="checkbox"/> 0.5	
I. Well bottom 415.0 ft. MSL or 20.0 ft.		
J. Filter pack, bottom 414.0 ft. MSL or 21.0 ft.		
K. Borehole, bottom 345.0 ft. MSL or 90.0 ft.		
L. Borehole, diameter 8.3 in.		
M. O.D. well casing 2.33 in.		
N. Well casing 2.00 in.		

I hereby certify that the information on this form is true and correct to the best of my knowledge.

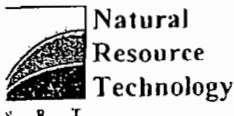
Signature Paula Richardson Paula Richardson

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23713 W. Paul Road, Unit D, Pewaukee, WI 53072

Tel: (262) 523-9000
Fax: (262) 523-9001

Template: NRT WELL CONSTRUCTION - Project: 1375 LOGS.GPJ

TSD 000136



MONITORING WELL CONSTRUCTION

Facility/Project Name A. Hudsonville Power Station Drilling Fac. License, Permit or Monitoring No.	Local Grid Location of Well 898090.86 ft. <input checked="" type="checkbox"/> N. <input type="checkbox"/> S. 1177978.73 ft. <input checked="" type="checkbox"/> E. <input type="checkbox"/> W.	Well Name TW-118
Facility ID	Local Grid Origin <input checked="" type="checkbox"/> (estimated: <input type="checkbox"/>) or Well Location <input type="checkbox"/> Lat. _____ " Long. _____ " or St. Plane _____ ft. N. _____ ft. E.	Unique Well No. _____ Well Number _____
Type of Well	Section Location 1/4 of _____ 1/4 of Sec. _____ T. _____ R. _____	Date Well Installed 05/04/2004
Well Code 12/pz Distance from Waste/ Source ft.	Location of Well Relative to Waste/Source u <input type="checkbox"/> Upgradient s <input type="checkbox"/> Sidegradient d <input type="checkbox"/> Downgradient n <input checked="" type="checkbox"/> Not Known	Well Installed By: (Person's Name and Firm) Steve Boart Longyear

A. Protective pipe, top elevation _____ ft. MSL	1. Cap and lock? <input checked="" type="checkbox"/> Yes <input type="checkbox"/> No
B. Well casing, top elevation 439.21 ft. MSL	2. Protective cover pipe: a. Inside diameter: 4.0 in. b. Length: 6.0 ft. c. Material: Steel <input checked="" type="checkbox"/> 0.4 in. Other <input type="checkbox"/>
C. Land surface elevation 437.0 ft. MSL	d. Additional protection? <input type="checkbox"/> Yes <input checked="" type="checkbox"/> No If yes, describe: _____ Bentonite <input checked="" type="checkbox"/> 3.0 Concrete <input type="checkbox"/> 0.1 Other <input type="checkbox"/>
D. Surface seal, bottom 436.0 ft. MSL or 1.0 ft.	3. Surface seal: _____
12. USCS classification of soil near screen: GP <input type="checkbox"/> GM <input type="checkbox"/> GC <input type="checkbox"/> GW <input type="checkbox"/> SW <input type="checkbox"/> SP <input checked="" type="checkbox"/> SM <input type="checkbox"/> SC <input type="checkbox"/> ML <input type="checkbox"/> MH <input type="checkbox"/> CL <input type="checkbox"/> CH <input type="checkbox"/> Bedrock <input type="checkbox"/>	4. Material between well casing and protective pipe: Bentonite <input type="checkbox"/> 3.0 Other <input checked="" type="checkbox"/>
13. Sieve analysis attached? <input type="checkbox"/> Yes <input checked="" type="checkbox"/> No	5. Annular space seal: a. Granular/Chipped Bentonite <input checked="" type="checkbox"/> 3.3 b. _____ Lbs/gal mud weight ... Bentonite-sand slurry <input type="checkbox"/> 3.5 c. _____ Lbs/gal mud weight ... Bentonite slurry <input type="checkbox"/> 3.1 d. _____ % Bentonite ... Bentonite-cement grout <input type="checkbox"/> 5.0 e. _____ ft ³ volume added for any of the above
14. Drilling method used: Rotary <input type="checkbox"/> 5.0 Hollow Stem Auger <input checked="" type="checkbox"/> 4.1 Other <input type="checkbox"/>	f. How installed: Tremie <input type="checkbox"/> 0.1 Tremie pumped <input type="checkbox"/> 0.2 Gravity <input checked="" type="checkbox"/> 0.8
15. Drilling fluid used: Water <input type="checkbox"/> 0.2 Air <input type="checkbox"/> 0.1 Drilling Mud <input type="checkbox"/> 0.3 None <input checked="" type="checkbox"/> 9.9	6. Bentonite seal: a. Bentonite granules <input type="checkbox"/> 3.3 b. <input type="checkbox"/> 1/4 in. <input type="checkbox"/> 3/8 in. <input type="checkbox"/> 1/2 in. Bentonite chips <input type="checkbox"/> 3.2 c. _____ Other <input type="checkbox"/>
16. Drilling additives used? <input type="checkbox"/> Yes <input checked="" type="checkbox"/> No	7. Fine sand material: Manufacturer, product name & mesh size a. _____ #7 Badger
Describe _____	b. Volume added _____ ft ³
17. Source of water (attach analysis, if required): _____	8. Filter pack material: Manufacturer, product name & mesh size a. _____ #40 Badger
E. Bentonite seal, top _____ ft. MSL or _____ ft.	9. Well casing: Flush threaded PVC schedule 40 <input checked="" type="checkbox"/> 2.3 Flush threaded PVC schedule 80 <input type="checkbox"/> 2.4 Other <input type="checkbox"/>
F. Fine sand, top 419.0 ft. MSL or 18.0 ft.	10. Screen material: PVC a. Screen Type: Factory cut <input checked="" type="checkbox"/> 1.1 Continuous slot <input type="checkbox"/> 0.1 Other <input type="checkbox"/>
G. Filter pack, top 418.0 ft. MSL or 19.0 ft.	b. Manufacturer Boart Longyear c. Slot size: 0.010 in. d. Slotted length: 5.0 ft.
H. Screen joint, top 417.0 ft. MSL or 20.0 ft.	11. Backfill material (below filter pack): None <input checked="" type="checkbox"/> 1.4 Other <input type="checkbox"/>
I. Well bottom 412.0 ft. MSL or 25.0 ft.	
J. Filter pack, bottom 411.0 ft. MSL or 26.0 ft.	
K. Borehole, bottom 411.0 ft. MSL or 26.0 ft.	
L. Borehole, diameter 8.3 in.	
M. O.D. well casing 2.33 in.	
N. Well casing 2.00 in.	

I hereby certify that the information on this form is true and correct to the best of my knowledge.

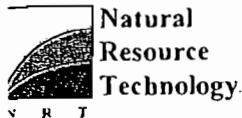
Signature
Paula Richardson

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23713 W. Paul Road, Unit D, Pewaukee, WI 53072

Tel: (262) 523-9000
Fax: (262) 523-9001

Template: NRT WELL CONSTRUCTION - Project: 1375 LOGS.GPJ

TSD 000137



MONITORING WELL CONSTRUCTION

Facility/Project Name Ameren Husonville Power Station Drilling		Local Grid Location of Well 896030.54 ft. <input checked="" type="checkbox"/> N. 1181339.05 ft. <input checked="" type="checkbox"/> E.	Well Name TW-119
Facility ID Type of Well Well Code 12/pz		Local Grid Origin <input checked="" type="checkbox"/> (estimated: <input type="checkbox"/>) or Well Location <input type="checkbox"/> Lat. _____ Long. _____ or St. Plane _____ ft. N, _____ ft. E. Section Location 1/4 of _____ 1/4 of Sec. _____ T. _____ R. _____	Unique Well No. _____ Well Number _____ Date Well Installed 05/03/2004 Well Installed By: (Person's Name and Firm) Steve Boart Longyear
Distance from Waste/ Source ft.		Location of Well Relative to Waste/Source u <input type="checkbox"/> Upgradient s <input type="checkbox"/> Sidegradient d <input type="checkbox"/> Downgradient n <input checked="" type="checkbox"/> Not Known	Gov. Lot Number _____
A. Protective pipe, top elevation _____ ft. MSL B. Well casing, top elevation _____ 438.12 ft. MSL C. Land surface elevation _____ 435.4 ft. MSL D. Surface seal, bottom _____ 434.4 ft. MSL or 1.0 ft.		<p>1. Cap and lock? <input checked="" type="checkbox"/> Yes <input type="checkbox"/> No</p> <p>2. Protective cover pipe: a. Inside diameter: 4.0 in. b. Length: 6.0 ft. c. Material: Steel <input checked="" type="checkbox"/> 0.4 Other <input type="checkbox"/> </p> <p>d. Additional protection? If yes, describe: _____ Bentonite <input checked="" type="checkbox"/> 3.0 Concrete <input type="checkbox"/> 0.1 Other <input type="checkbox"/> </p> <p>3. Surface seal: _____ Bentonite <input checked="" type="checkbox"/> 3.0 Concrete <input type="checkbox"/> 0.1 Other <input type="checkbox"/> </p> <p>4. Material between well casing and protective pipe: Sand <input type="checkbox"/> 3.0 Bentonite <input type="checkbox"/> 0.1 Other <input checked="" type="checkbox"/> </p> <p>5. Annular space seal: a. Granular/Chipped Bentonite <input checked="" type="checkbox"/> 3.3 b. _____ Lbs/gal mud weight ... Bentonite-sand slurry <input type="checkbox"/> 3.5 c. _____ Lbs/gal mud weight ... Bentonite slurry <input type="checkbox"/> 3.1 d. _____ % Bentonite ... Bentonite-cement grout <input type="checkbox"/> 5.0 e. _____ ft³ volume added for any of the above</p> <p>f. How installed: Tremie <input type="checkbox"/> 0.1 Tremie pumped <input type="checkbox"/> 0.2 Gravity <input checked="" type="checkbox"/> 0.8</p> <p>6. Bentonite seal: a. Bentonite granules <input type="checkbox"/> 3.3 b. <input type="checkbox"/> 1/4 in. <input type="checkbox"/> 3/8 in. <input type="checkbox"/> 1/2 in. Bentonite chips <input type="checkbox"/> 3.2 c. _____ Other <input type="checkbox"/> </p> <p>7. Fine sand material: Manufacturer, product name & mesh size a. #7 Badger b. Volume added _____ ft³</p> <p>8. Filter pack material: Manufacturer, product name & mesh size a. #40 Badger b. Volume added _____ ft³</p> <p>9. Well casing: Flush threaded PVC schedule 40 <input checked="" type="checkbox"/> 2.3 Flush threaded PVC schedule 80 <input type="checkbox"/> 2.4 Other <input type="checkbox"/> </p> <p>10. Screen material: a. Screen Type: Factory cut <input checked="" type="checkbox"/> 1.1 Continuous slot <input type="checkbox"/> 0.1 Other <input type="checkbox"/> b. Manufacturer Boart Longyear c. Slot size: 0.010 in. d. Slotted length: 5.0 ft.</p> <p>11. Backfill material (below filter pack): Bentonite, stuff <input type="checkbox"/> 1.4 None <input type="checkbox"/> 1.4 Other <input type="checkbox"/> </p>	
<p>12. USCS classification of soil near screen:</p> <p>GP <input type="checkbox"/> GM <input type="checkbox"/> GC <input type="checkbox"/> GW <input type="checkbox"/> SW <input type="checkbox"/> SP <input checked="" type="checkbox"/> SM <input type="checkbox"/> SC <input type="checkbox"/> ML <input type="checkbox"/> MH <input type="checkbox"/> CL <input type="checkbox"/> CH <input type="checkbox"/> Bedrock <input type="checkbox"/></p> <p>13. Sieve analysis attached? <input type="checkbox"/> Yes <input checked="" type="checkbox"/> No</p> <p>14. Drilling method used: Rotary <input type="checkbox"/> 5.0 Hollow Stem Auger <input checked="" type="checkbox"/> 4.1 rock core <input type="checkbox"/> Other <input checked="" type="checkbox"/> </p> <p>15. Drilling fluid used: Water <input checked="" type="checkbox"/> 0.2 Air <input type="checkbox"/> 0.1 Drilling Mud <input type="checkbox"/> 0.3 None <input type="checkbox"/> 9.9</p> <p>16. Drilling additives used? <input type="checkbox"/> Yes <input checked="" type="checkbox"/> No Describe _____</p> <p>17. Source of water (attach analysis, if required): Town of Husonville well</p> <p>E. Bentonite seal, top _____ ft. MSL or _____ ft. F. Fine sand, top _____ 422.4 ft. MSL or 13.0 ft. G. Filter pack, top _____ 421.4 ft. MSL or 14.0 ft. H. Screen joint, top _____ 420.4 ft. MSL or 15.0 ft. I. Well bottom _____ 415.4 ft. MSL or 20.0 ft. J. Filter pack, bottom _____ 414.4 ft. MSL or 21.0 ft. K. Borehole, bottom _____ 335.4 ft. MSL or 100.0 ft. L. Borehole, diameter _____ 8.3 in. M. O.D. well casing _____ 2.33 in. N. well casing _____ 2.00 in.</p>			

I hereby certify that the information on this form is true and correct to the best of my knowledge.

Signature

Paula Richardson

Firm Natural Resource Technology, Inc.

23713 W. Paul Road, Unit D, Pewaukee, WI 53072

Tel: (262) 523-9000

Fax: (262) 523-9001

Template: NRT WELL CONSTRUCTION - Project: 1375 LOGS.GPJ

TSD 000138

MONITORING WELL CONSTRUCTION

Facility/Project Name Ameren Huronville Power Station Drilling	Local Grid Location of Well 898614.91 ft. <input checked="" type="checkbox"/> N. 1180157.14 ft. <input checked="" type="checkbox"/> E. <input type="checkbox"/> S. <input type="checkbox"/> W.	Well Name TW-120
Far License, Permit or Monitoring No.	Local Grid Origin <input checked="" type="checkbox"/> (estimated: <input type="checkbox"/>) or Well Location <input type="checkbox"/> Lat. _____ Long. _____ or St. Plane _____ ft. N, _____ ft. E.	Unique Well No. _____ Well Number _____
Facility ID	Section Location 1/4 of _____ 1/4 of Sec. _____ T. _____ R. _____	Date Well Installed 05/04/2004
Type of Well Well Code 12/pz	Location of Well Relative to Waste/Source u <input type="checkbox"/> Upgradient s <input type="checkbox"/> Sidegradient d <input type="checkbox"/> Downgradient n <input checked="" type="checkbox"/> Not Known	Well Installed By: (Person's Name and Firm) Steve Boart Longyear
Distance from Waste/ Source ft.	Gov. Lot Number _____	

- A. Protective pipe, top elevation _____ ft. MSL
 B. Well casing, top elevation 449.00 ft. MSL
 C. Land surface elevation 446.8 ft. MSL
 D. Surface seal, bottom 445.8 ft. MSL or 1.0 ft.

12. USCS classification of soil near screen:
 GP GM GC GW SW SP
 SM SC ML MH CL CH
 Bedrock

13. Sieve analysis attached? Yes No

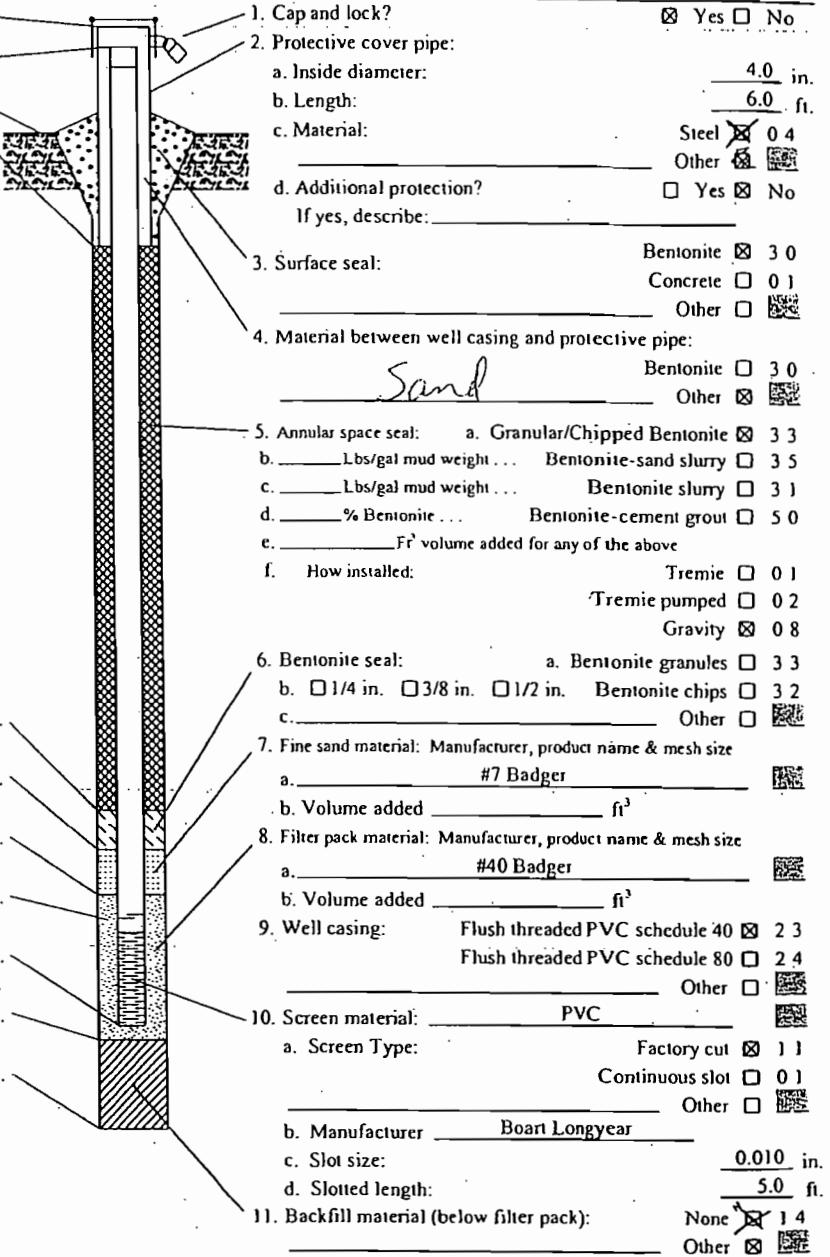
14. Drilling method used: Rotary 50
 Hollow Stem Auger 41
 Other

15. Drilling fluid used: Water 0.2 Air 0.1
 Drilling Mud 0.3 None 9.9

16. Drilling additives used? Yes No
 Describe _____

17. Source of water (attach analysis, if required):

- E. Bentonite seal, top 421.8 ft. MSL or 25.0 ft.
 F. Fine sand, top 418.8 ft. MSL or 28.0 ft.
 G. Filter pack, top 417.8 ft. MSL or 29.0 ft.
 H. Screen joint, top 416.8 ft. MSL or 30.0 ft.
 I. Well bottom 411.8 ft. MSL or 35.0 ft.
 J. Filter pack, bottom 410.8 ft. MSL or 36.0 ft.
 K. Borehole, bottom 410.8 ft. MSL or 36.0 ft.
 L. Borehole, diameter 8.3 in.
 M. O.D. well casing 2.33 in.
 N. well casing 2.00 in.



I hereby certify that the information on this form is true and correct to the best of my knowledge.

Signature Paula Richardson Firm Natural Resource Technology, Inc.
 23713 W. Paul Road, Unit D, Pewaukee, WI 53072 Tel: (262) 523-9000
 Fax: (262) 523-9001

Template: NRT WELL CONSTRUCTION - Project: 1375 LOGS.GPJ

Route to: Watershed/Wastewater Waste Management
 Remediation/Redevelopment Other

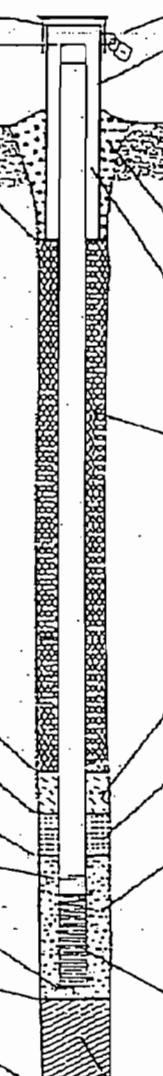
MONITORING WELL CONSTRUCTION

Facility/Project Name Hutsonville Power STATION		Local Grid Location of Well N. <input type="checkbox"/> S. <input type="checkbox"/> E. <input type="checkbox"/> W. <input type="checkbox"/>		ft. <input type="checkbox"/> m. <input type="checkbox"/>	Well Name MW-11R
City License, Permit or Monitoring No.		Local Grid Origin <input type="checkbox"/> (estimated: <input type="checkbox"/>) or Well Location <input type="checkbox"/> Lat. <input type="checkbox"/> long. <input type="checkbox"/> or		Unique Well No. IDNR Well ID No.	
Facility ID		St. Plane	ft. N. <input type="checkbox"/> ft. E. <input type="checkbox"/> S/C/N	Date Well Installed 10/03/2001	
Type of Well Well Code 11 / MW		Section Location of Waste/Source 1/4 of <input type="checkbox"/> 1/4 of <input type="checkbox"/> Section T. <input type="checkbox"/> N.R. <input type="checkbox"/> S.W.		Well Installed By: Name (first, last) and Fld R. Radke	
Distance from Waste/Source	Envi Stds. 80 ft	Location of Well Relative to Waste/Source <input type="checkbox"/> Upgradient <input checked="" type="checkbox"/> Sidegradient <input type="checkbox"/> Downgradient <input type="checkbox"/> Not Known	Gov. Lot Number	Bart Longyear	

- A. Protective pipe, top elevation _____ ft. MSL
 B. Well casing, top elevation -443.55 ft MSL
 C. Land surface elevation -490.92 ft MSL
 D. Surface seal, bottom _____ ft MSL or -0.5 ft

12. USCS classification of soil near screen:
 GP GM GC GW SW SP
 SM SC ML MH CL CH
 Bedrock
 13. Sieve analysis performed? Yes No
 14. Drilling method used: Rotary 50
 Hollow Stem Auger 41
 Other
 15. Drilling fluid used: Water 02 Air 01
 Drilling Mud 03 None 99
 16. Drilling additives used? Yes No
 Describe _____
 17. Sources of water (attach analysis, if required):

- E. Bentonite seal, top _____ ft MSL or -4.0 ft
 F. Fine sand, top _____ ft MSL or -4.0 ft
 G. Filter pack, top _____ ft MSL or -4.5 ft
 H. Screen joint, top _____ ft MSL or -5.5 ft
 I. Well bottom _____ ft MSL or -15.5 ft
 J. Filter pack, bottom _____ ft MSL or -16.0 ft
 K. Borehole, bottom _____ ft MSL or -16.0 ft
 L. Borehole, diameter -8.3 in.
 M. O.D. well casing -2.35 in.
 N. I.D. well casing -2.15 in.



1. Cap and lock? Yes No
 2. Protective cover pipe:
 a. Inside diameter: -4.0 in.
 b. Length: -7.0 ft
 c. Material: Steel 04
 Other
 d. Additional protection? Yes No
 If yes, describe: 3" Bumper Post
 3. Surface seal:
 Bentonite 30
 Concretic 01
 Other
 4. Material between well casing and protective pipe:
 Bentonite 30
 SAND
 Other
 5. Annular space seal:
 a. Granular/Chipped Bentonite 33
 b. ____ Lbs/gal mud weight ... Bentonite-sand slurry 35
 c. ____ Lbs/gal mud weight Bentonite slurry 31
 d. ____ % Bentonite Bentonite-cement grout 50
 e. ____ ft³ volume added for any of the above
 f. How installed:
 Tropic 01
 Tropic pumped 02
 Gravity 08
 6. Bentonite seal:
 a. Bentonite granules 33
 b. 1/4 in. 3/8 in. 1/2 in. Bentonite chips 32
 c. _____ Other
 7. Fine sand material: Manufacturer, product name & mesh size
 a. #7 BADER MATERIAL
 b. Volume added _____ ft³
 8. Filter pack material: Manufacturer, product name & mesh size
 a. #40 AMERICAN MATERIAL
 b. Volume added _____ ft³
 9. Well casing:
 Flush threaded PVC schedule 40 23
 Flush threaded PVC schedule 80 24
 Other
 10. Screen material: PVC
 a. Screen type
 Factory cut 11
 Continuous slot 01
 Other
 b. Manufacturer Johnson
 c. Slot size: 0.010 in.
 d. Slotted length: 19.0 ft
 11. Backfill material (below filter pack):
 None 14
 Other

I certify that the information on this form is true and correct to the best of my knowledge.

Signature

From

NATURAL RESOURCE TECHNOLOGY INC.

Route to: Watershed/Wastewater Waste Management
 Remediation/Redevelopment Other

MONITORING WELL CONSTRUCTION

Facility/Project Name Hutsonville Power Station		Local Grid Location of Well Lat. <input type="checkbox"/> N. <input checked="" type="checkbox"/> S. Long. <input type="checkbox"/> E. <input checked="" type="checkbox"/> W.		Well Name MW-14
Utility License, Permit or Monitoring No.		Local Grid Origin <input type="checkbox"/> (estimated: <input type="checkbox"/>) or Well Location <input type="checkbox"/> Lat. "Long. " or		Unique Well No. DNR Well ID No.
Facility ID		SL Plane	ft. N. ft. E. S/C/N	Date Well Installed 10/03/2001 m m d d v v v
Type of Well	Well Code 12 / P2	Section Location of Waste/Source 1/4 of ... 1/4 of Sec. T. N. R. <input type="checkbox"/> E. <input checked="" type="checkbox"/> W.		Well Installed By: Name (first, last) and File R. Barke
Distance from Waste/Source	80 ft	Enr. Stds. Apply <input type="checkbox"/>	Location of Well Relative to Waste/Source u <input type="checkbox"/> Upgradient s <input type="checkbox"/> Sidegradient d <input checked="" type="checkbox"/> Downgradient n <input type="checkbox"/> Not Known	Gov. Lot Number B007 L004-R

A. Protective pipe, top elevation	ft. MSL	1. Cap and lock? <input type="checkbox"/> Yes <input checked="" type="checkbox"/> No
B. Well casing, top elevation	- 443.35 ft. MSL	2. Protective cover pipe: a. Inside diameter: 4.0 in. b. Length: 7.0 ft. c. Material: Steel <input checked="" type="checkbox"/> 04 Other <input type="checkbox"/> 05
C. Land surface elevation	- 440.93 ft. MSL	d. Additional protection? <input type="checkbox"/> Yes <input checked="" type="checkbox"/> No If yes, describe: 3" Bumper Post
D. Surface seal, bottom	ft. MSL or - 0.0 ft.	3. Surface seal: Bentonite <input checked="" type="checkbox"/> 30 Concrete <input type="checkbox"/> 01 Other <input type="checkbox"/> 02
12. USCS classification of soil near screen: GP <input type="checkbox"/> GM <input type="checkbox"/> GC <input type="checkbox"/> GW <input type="checkbox"/> SW <input type="checkbox"/> SP <input checked="" type="checkbox"/> SM <input type="checkbox"/> SC <input type="checkbox"/> ML <input type="checkbox"/> MH <input type="checkbox"/> CL <input type="checkbox"/> CH <input type="checkbox"/> Bedrock: <input type="checkbox"/>		4. Material between well casing and protective pipe: Bentonite <input type="checkbox"/> 30 SAND <input type="checkbox"/> 01 Other <input checked="" type="checkbox"/> 02
13. Sieve analysis performed? <input type="checkbox"/> Yes <input checked="" type="checkbox"/> No		5. Annular space seal: a. Granular/Chipped Bentonite <input checked="" type="checkbox"/> 33 b. ____ Lbs/gal mud weight ... Bentonite-sand slurry <input type="checkbox"/> 35 c. ____ Lbs/gal mud weight Bentonite slurry <input type="checkbox"/> 31 d. ____ % Bentonite Bentonite-cement grout <input type="checkbox"/> 50 e. ____ ft ³ volume added for any of the above f. How installed: Tramit <input type="checkbox"/> 01 Tramit pumped <input type="checkbox"/> 02 Gravity <input checked="" type="checkbox"/> 08
14. Drilling method used: Rotary <input type="checkbox"/> 50 Hollow Stem Auger <input checked="" type="checkbox"/> 41 Other <input type="checkbox"/> 08		6. Bentonite seal: a. Bentonite granules <input checked="" type="checkbox"/> 33 b. <input type="checkbox"/> 1/4 in. <input type="checkbox"/> 3/8 in. <input type="checkbox"/> 1/2 in. Bentonite chips <input type="checkbox"/> 32 c. _____ Other <input type="checkbox"/> 02
15. Drilling fluid used: Water <input type="checkbox"/> 02 Air <input type="checkbox"/> 01 Drilling Mud <input type="checkbox"/> 03 None <input checked="" type="checkbox"/> 99		7. Fine sand material: Manufacturer, product name & mesh size a. # 7 BADGER
16. Drilling additives used? <input type="checkbox"/> Yes <input checked="" type="checkbox"/> No		b. Volume added _____ ft ³
17. Sources of water (match analysis, if required):		8. Filter pack material: Manufacturer, product name & mesh size a. # 40 AMERICAN MATERIAL
E. Bentonite seal, top	ft. MSL or - 24.0 ft.	b. Volume added _____ ft ³
F. Fine sand, top	ft. MSL or - 24.0 ft.	9. Well casing: Flush threaded PVC schedule 40 <input checked="" type="checkbox"/> 23 Flush threaded PVC schedule 80 <input type="checkbox"/> 24 Other <input type="checkbox"/> 02
G. Filter pack, top	ft. MSL or - 26.0 ft.	10. Screen material: PVC a. Screen type: Factory cut <input checked="" type="checkbox"/> 11 Continuous slot <input type="checkbox"/> 01 Other <input type="checkbox"/> 02
H. Screen joint, top	ft. MSL or - 28.0 ft.	b. Manufacturer Johnson c. Slot size: 0.01 in. d. Slotted length: 5.9 ft
I. Well bottom	ft. MSL or - 33.0 ft.	11. Backfill material (below filter pack): None <input type="checkbox"/> 14 FORMATION COLLAPSE Other <input type="checkbox"/> 05
J. Filter pack, bottom	ft. MSL or - 35.0 ft.	
K. Borehole, bottom	ft. MSL or - 39.0 ft.	
L. Borehole, diameter	8.3 in.	
M. O.D. well casing	2.35 in.	
N. I.D. well casing	2.10 in.	

I certify that the information on this form is true and correct to the best of my knowledge.

Name Mark Shylock Firm NATURAL RESOURCE TECHNOLOGY INC.

MONITORING WELL CONSTRUCTION

Route to:	Watershed/Wastewater <input type="checkbox"/>	Waste Management <input type="checkbox"/>
Facility/Project Name	Local Grid Location of Well N. <input type="checkbox"/> S. <input type="checkbox"/> E. <input type="checkbox"/> W. <input type="checkbox"/>	
Facility License, Permit or Monitoring No.	Local Grid Origin <input type="checkbox"/> (estimated: <input type="checkbox"/>) or Well Location <input type="checkbox"/> Lat. <input type="checkbox"/> Long. <input type="checkbox"/> or SL Plane <input type="checkbox"/> ft N. <input type="checkbox"/> ft E. <input type="checkbox"/> S/C/N	
Facility ID	Section Location of Waste/Source 1/4 of <input type="checkbox"/> 1/4 of Sec. <input type="checkbox"/> T. <input type="checkbox"/> N.R. <input type="checkbox"/> E. <input type="checkbox"/> W.	
Type of Well	Well Code <u>12 / PZ</u>	Location of Well Relative to Waste/Source u <input type="checkbox"/> Upgradient s <input type="checkbox"/> Sidegradient d <input checked="" type="checkbox"/> Downgradient n <input type="checkbox"/> Not Known
Distance from Waste/Source	Envi. Stds. <u>80</u> ft	Gov. Lot Number
A. Protective pipe, top elevation	ft MSL	
B. Well casing, top elevation	<u>- 440.59</u> ft MSL	
C. Land surface elevation	<u>- 437.81</u> ft MSL	
D. Surface seal, bottom	ft MSL or <u>- 0.0</u> ft	
12. USCS classification of soil near screen:	GP <input type="checkbox"/> GM <input type="checkbox"/> GC <input type="checkbox"/> GW <input type="checkbox"/> SW <input type="checkbox"/> SP <input checked="" type="checkbox"/> SM <input type="checkbox"/> SC <input type="checkbox"/> ML <input type="checkbox"/> MH <input type="checkbox"/> CL <input type="checkbox"/> CH <input type="checkbox"/> Bedrock <input type="checkbox"/>	
13. Sieve analysis performed?	<input type="checkbox"/> Yes <input checked="" type="checkbox"/> No	
14. Drilling method used:	Rotary <input type="checkbox"/> 50 Hollow Stem Auger <input checked="" type="checkbox"/> 41 Other <input type="checkbox"/>	
15. Drilling fluid used:	Water <input type="checkbox"/> 02	Air <input type="checkbox"/> 01
	Drilling Mud <input type="checkbox"/> 03	Name <input checked="" type="checkbox"/> 99
16. Drilling additives used?	<input type="checkbox"/> Yes <input checked="" type="checkbox"/> No	
Describe _____		
17. Source of water (attach analysis, if required):	_____	
E. Bentonite seal, top	ft MSL or <u>- 30.0</u> ft	
F. Fine sand, top	ft MSL or <u>- 30.0</u> ft	
G. Filter pack, top	ft MSL or <u>- 32.0</u> ft	
H. Screen joints, top	ft MSL or <u>- 34.0</u> ft	
I. Well bottom	ft MSL or <u>- 39.0</u> ft	
J. Filter pack, bottom	ft MSL or <u>- 39.5</u> ft	
K. Borehole, bottom	ft MSL or <u>- 39.5</u> ft	
L. Borehole, diameter	<u>8.3</u> in.	
M. O.D. well casing	<u>2.35</u> in.	
N. I.D. well casing	<u>2.15</u> in.	
I certify that the information on this form is true and correct to the best of my knowledge.		
Signature	Firm <u>Mark Shaffer</u> <u>NATURAL RESOURCE TECHNOLOGY, INC.</u>	

TSD 000142



Well/Boring Abandonment Form

Client

NRT

NOV - 1 2001

Location

Hutsonville, IL

Job Name

Hutsonville Project

Job Number

Y903 E111 0372AM
3410-1624

Well/Boring Number

MW-11

.03

Date of Abandonment

10/03/01

Reason for Abandonment

Study Complete

Abandonment Done By

R. Radke

Hole Type: Monitoring Well Drillhole Pumping WellConstruction Type: Drilled Driven Other _____Formation Type: Unconsolidated BedrockSealing Method: Gravity Pumped Other _____Sealing Materials: Bentonite Chips Cement-Bent Grout Other _____

Sealing Material	From (ft)	To (ft)	Quantity	Gallon(s) Bag(s)
Topsoil	Surface	0.5		Gallon(s)
Bentonite Chips	0.5	16.2	1	Bag(s)

Well Information ONLY

All measurements are from ground surface

Total Well Depth 16.2 ft.

Screen Removed

Yes	No
	x
	x
x	
x	

Casing Diameter 2 in.

Overdrilled

Casing Depth 16.2 ft.

Casing Left in Place

Depth to Water 8.95 ft.

Casing Cut Below Surface

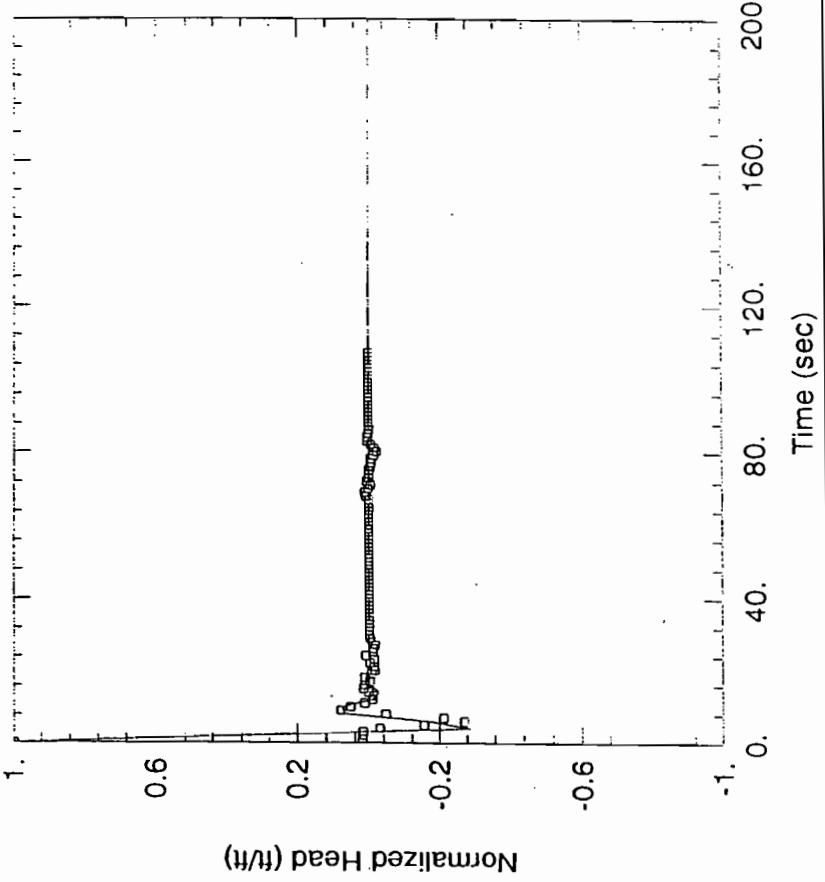
Comments: _____

TSD 000143

APENDIX A-3

SLUG TEST DATA

TSD 000144



Data Set: P:\..\11375\115s slug outA.aqt
 Date: 05/11/05
 Time: 15:21:28

PROJECT INFORMATION

Company: Natural Resource Technology
 Client: Ameren
 Project: 1375
 Location: Hutsonville, IL
 Test Well: TW-115S
 Test Date: 5/13/04

SOLUTION

Aquifer Model: Confined
 Solution Method: Butler
 $K = 0.09332 \text{ cm/sec}$
 $C(D) = 0.3464$

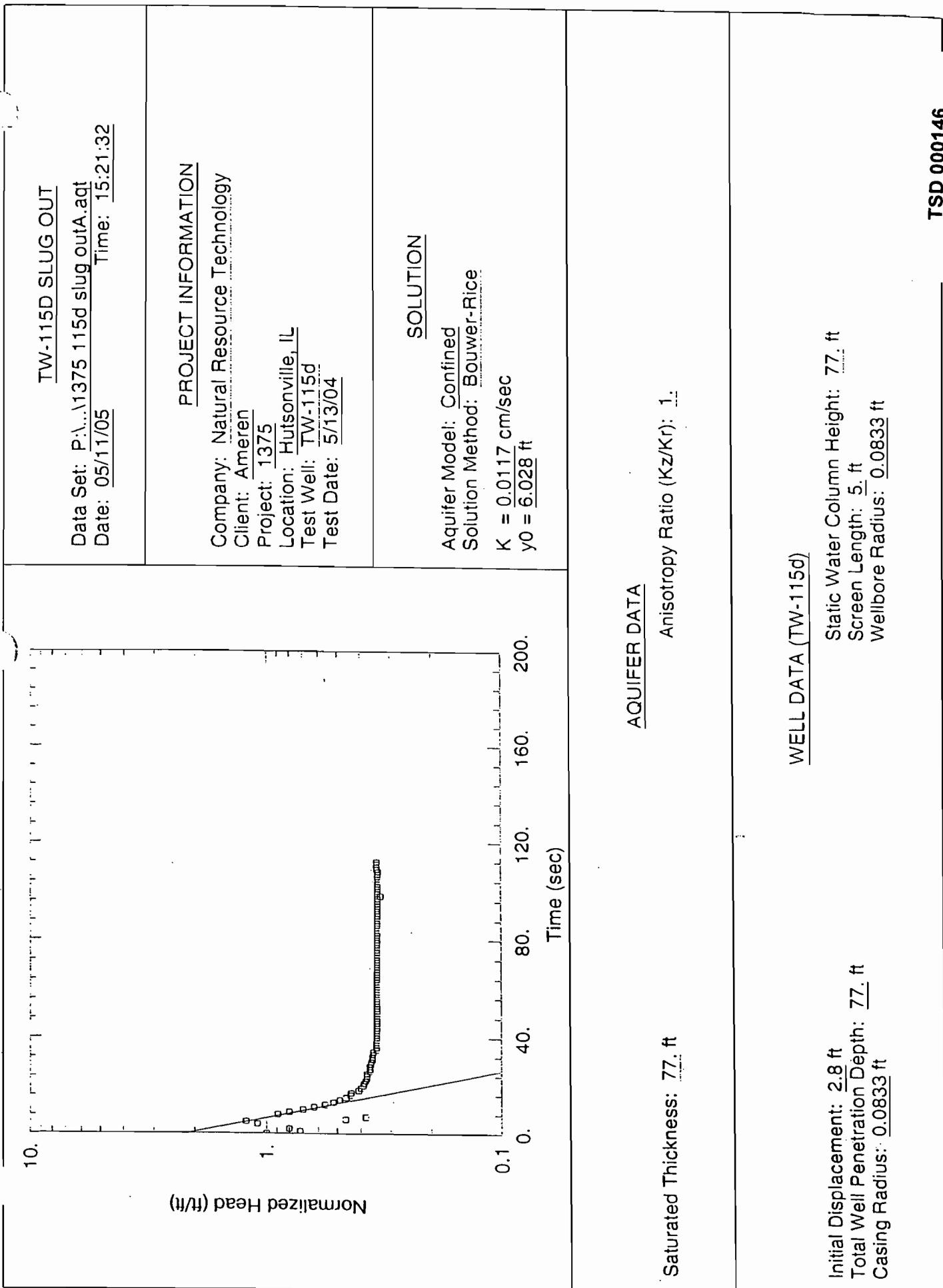
AQUIFER DATA

Anisotropy Ratio (K_z/K_r): 1.

WELL DATA (TW-115S)

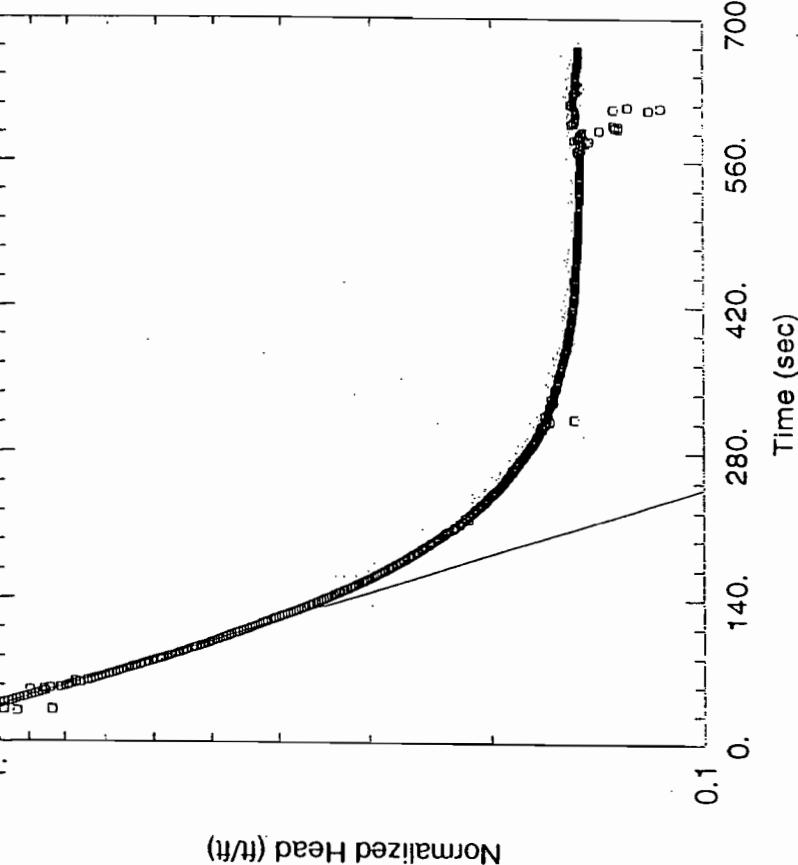
Static Water Column Height: 23.37 ft
 Screen Length: 5 ft
 Wellbore Radius: 0.0833 ft

Initial Displacement: 2.8 ft
 Total Well Penetration Depth: 23.37 ft
 Casing Radius: 0.0833 ft



TSD 000146

Initial Displacement: 2.8 ft
Total Well Penetration Depth: 77. ft
Casing Radius: 0.0833 ft



TW-116 SLUG OUT

Data Set: P:\...\1375\116 slug outA.aqt
Date: 05/11/05 Time: 15:21:22

PROJECT INFORMATION

Company: Natural Resource Technology
Client: Ameren
Project: 1375
Location: Hutsonville, IL
Test Well: TW-116
Test Date: 5/13/04

SOLUTION

Aquifer Model: Confined
Solution Method: Bouwer-Rice
 $K = 0.0004557 \text{ cm/sec}$
 $y_0 = 4.116 \text{ ft}$

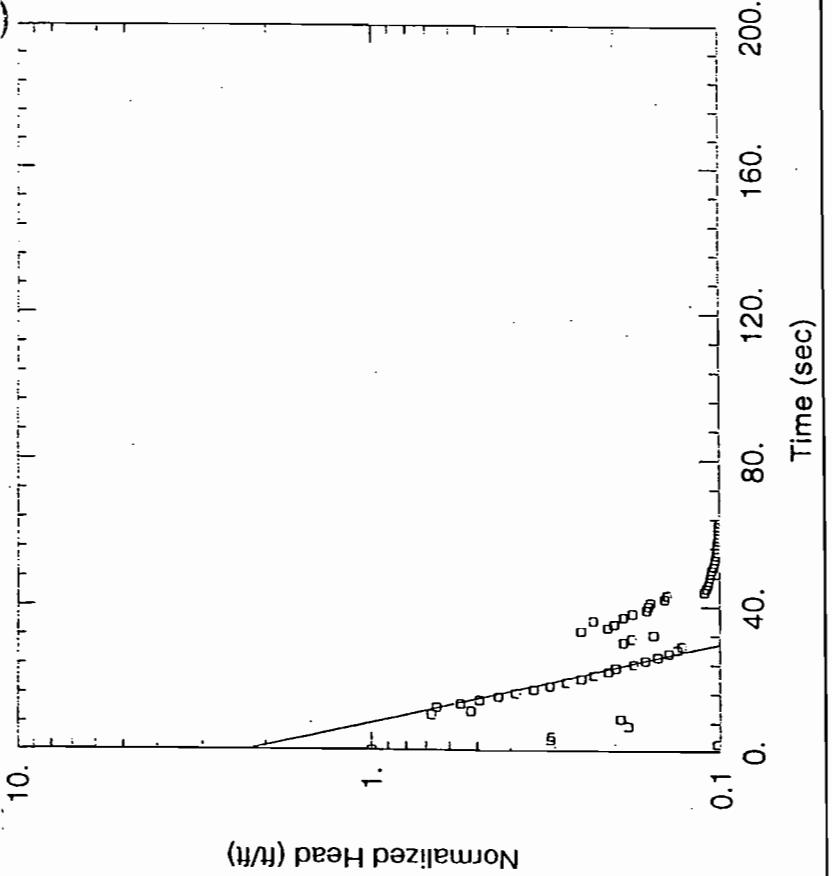
AQUIFER DATA
Anisotropy Ratio (K_z/K_t): 1.

Saturated Thickness: 50. ft

WELL DATA (TW-116)

Static Water Column Height: 20. ft
Screen Length: 5. ft
Wellbore Radius: 0.354 ft

Initial Displacement: 2.8 ft
Total Well Penetration Depth: 20. ft
Casing Radius: 0.0833 ft



TW-117 SLUG OUT

Data Set: P:\...\1375\117 slug outA.aqt
 Date: 05/11/05 Time: 15:21:18

PROJECT INFORMATION

Company: Natural Resource Technology
 Client: Ameren
 Project: 1375
 Location: Hutsonville, IL
 Test Well: TW-117
 Test Date: 5/13/04

SOLUTION

Aquifer Model: Unconfined
 Solution Method: Bouwer-Rice
 $K = \frac{0.006694}{6.341} \text{ cm/sec}$
 $y_0 = 6.341 \text{ ft}$

AQUIFER DATA

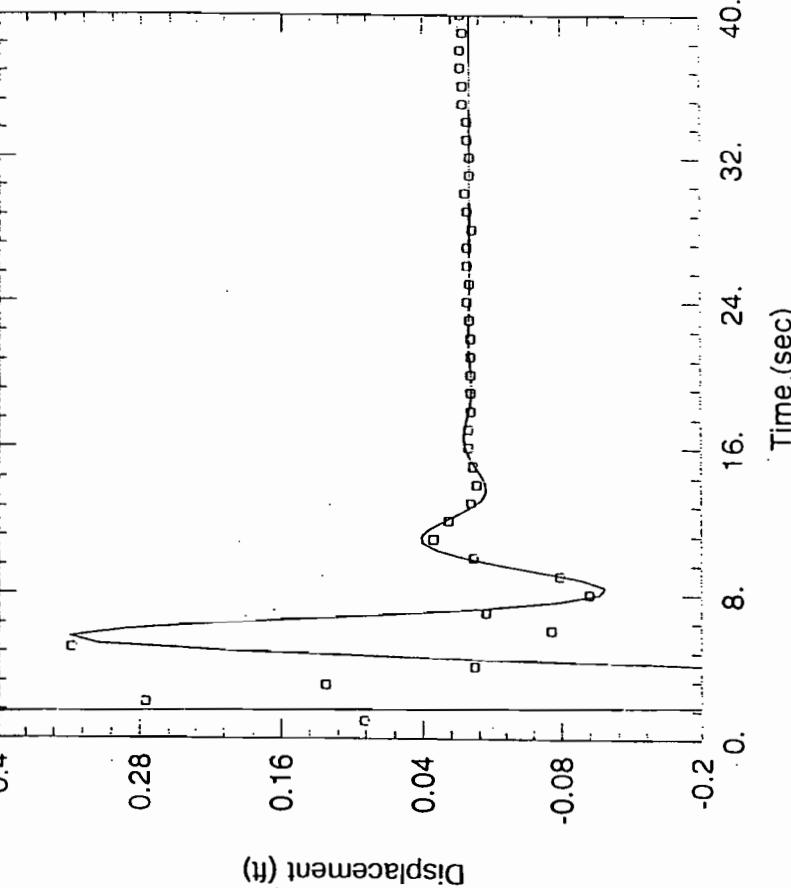
Anisotropy Ratio (K_z/K_r): 1.

WELL DATA (TW-117)

Static Water Column Height: 12. ft
 Screen Length: 5. ft
 Wellbore Radius: 0.0833 ft

Initial Displacement: 2.8 ft
 Total Well Penetration Depth: 12. ft
 Casing Radius: 0.0833 ft

TSD 000148



TW-118 SLUG IN
Data Set: P:\...\1375\118 slug inA.aqt
Date: 05/11/05 Time: 15:21:14

PROJECT INFORMATION

Company: Natural Resource Technology
Client: Ameren
Project: 1375
Location: Hudsonville, IL
Test Well: TW-118
Test Date: 5/13/04

SOLUTION

Aquifer Model: Confined
Solution Method: Butter
 $K = 0.1638 \text{ cm/sec}$
 $C(D) = 0.3179$

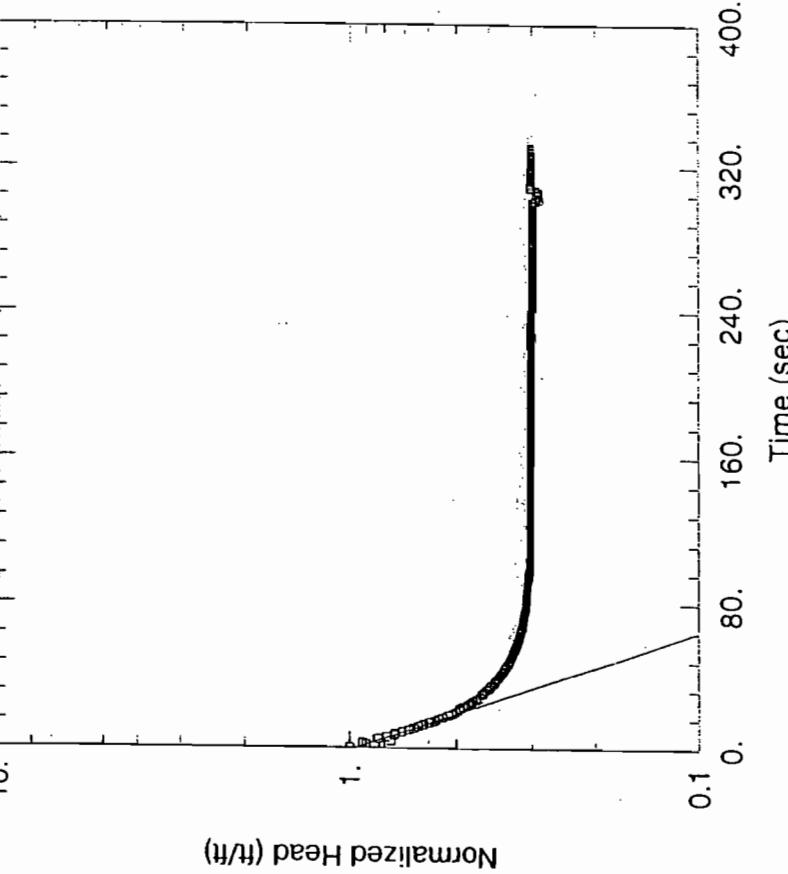
AQUIFER DATA

Anisotropy Ratio (K_z/K_r): 1

WELL DATA (TW-118)

Static Water Column Height: 16. ft
Screen Length: 5. ft
Wellbore Radius: 0.0833 ft

Initial Displacement: 2.8 ft
Total Well Penetration Depth: 16. ft
Casing Radius: 0.0833 ft



TW-119 SLUG OUT

Data Set: P:\...\1375\119 slug outA.aqt
 Date: 05/11/05 Time: 15:21:04

PROJECT INFORMATION

Company: Natural Resource Technology
 Client: Ameren
 Project: 1375
 Location: Hutsonville, IL
 Test Well: TW-119
 Test Date: 5/13/04

SOLUTION

Aquifer Model: Confined
 Solution Method: Bouwer-Rice
 $K = 0.002244 \text{ cm/sec}$
 $y_0 = 2.69 \text{ ft}$

AQUIFER DATA

Anisotropy Ratio (K_z/K_r): 1.

WELL DATA (TW-119)

Initial Displacement: 2.8 ft
 Total Well Penetration Depth: 13. ft
 Casing Radius: 0.0833 ft
 Screen Length: 5. ft
 Wellbore Radius: 0.0833 ft

Initial Displacement: 2.8 ft
 Total Well Penetration Depth: 13. ft
 Casing Radius: 0.0833 ft

TSD 000150

APENDIX A-4

GROUNDWATER SAMPLING SOP (AEG)

Monitor Well Sampling Procedure

Purpose:

The procedure for Hutsonville Power Station's Monitor Well sampling is based on IEPA Sampling Procedure Instructions. These instructions are prepared to inform owners/operators of treatment, storage and disposal facilities of proper water sampling procedures. It is expected that by complying with these procedures it will help in obtaining analytical results consistent and comparable with those obtained by the Agency. The Monitoring Well sampling is completed on a monthly basis for Monitoring Wells 1 - 5, pH readings and sample filtration is complete at Hutsonville with the samples shipped to the CIPS Central Lab-Springfield (tested for TDS, Boron, Calcium, Hardness, Manganese, Sulfate, and Alkalinity).

Equipment Needed:

Pump and Tubing (Asco portable pump)

Monitor Well Sample Bottles (5 x 1 liter)

Water Level Indicator

Data Entry Sheet

Truck, Car or 12 V Battery

Timer/Stopwatch/Secondhand on watch

Depth = Volume Data Sheet

Adapter/Connector and cord used to hookup the battery to the pump

pH Meter/Probe

Cooler w/ ice (temperature >39°F)

Sampling Procedure:

- 1) Connect the Adapter to the battery and pump.
- 2) Use the Water Level Indicator to find the distance to the top of the water in the well.
 - a) To do this, slowly lower the Water Level Indicator probe into the well. When the probe reaches the water you will hear the Water Level Indicator buzzer, indicating that water has been reached. When you hear the buzzer, pull back until it stops, and lower slow until the buzzer sounds again.
 - b) Read the increments on the wire from the North side of the casing. (Increments in 100th of an inch).
 - c) This is the first entry on the Data Entry Sheet. (See below)
- 3) From this entry, calculate the volume of water in the well, by subtracting it from the well depth + casing height. Use the data sheet when calculating. From this result, use the chart to calculate the volume of water (gals) in the well. Record this value on the data sheet. If the value does not appear on the sheet, the following calculation may be used to estimate the volume of water in the well.

$$\text{feet of water} \times 0.1632 = \text{est. volume of water in the well}$$

- 4) With the pump on, drop the pump tubing into the well until the pump starts to pump water.
- 5) Pump at least one well casing volume of water from the monitor well prior to obtaining a water sample. This is to remove stagnant water in the well and obtain water more representative of the monitored aquifer.
 - a) To do this, fill the 1L Monitor Well Sample Bottle, and note the time it takes to fill it. Multiply the time by 4. This is the time it takes for the pump, at a designated setting, to pump 1 gallon of well water.
 - b) Multiply the number of gallons of well water by the time it takes to fill one gallon. This is the amount of time it takes to pump the volume of well water out. Pump, at least, this volume of well water out. Record the amount removed on the data sheet.
 - c) After removing the required volume of well water, the well should be sampled while it is recharging. The rechargeing of Hutsonville's wells range from instantaneous to approximately 15 min. depending on how dry the season has been.
- 6) Rinse the sample bottle at least 3 times with well water, fill, measure the pH, record pH, and place in a cooler of ice (only necessary if the temperature outside is more than 39° F).
- 7) Pull tubing out while pump is running to remove most of the remaining water in the tubing.
- 8) Repeat steps 1-7 for all remaining Monitor Wells (1-5).

Filtering Procedure:

- 1) All groundwater samples to be analyzed for inorganic parameters (metals) are to be filtered through a 0.45 micron Cellulose Nitrate filter membrane.
- 2) Obtain a clean 1 L filter flask for each sample (5), a clean funnel, and a vacuum pump.

Hutsonville Monitoring Well Samples

Date:

Collected by:

MW #	Depth to top of Water	Calculations	Volume of Water in Well	Quantity Discharged before sampling	pH
1		11.50 _____			
2		21.25 _____			
3		12.42 _____			
4		18.17 _____			
5		20.67 _____			

Remarks:

APPENDIX B

ALTERNATIVE COST SUMMARY SHEETS

GROUNDWATER MANAGEMENT ALTERNATIVE: Collection Trench

 Pond D Closure Alternatives Report
 Hutsonville Power Station
 Ameren Services

 NRT PROJECT NO.: 1954/2.3
 BY: KJB CHKD BY: CAR
 DATE: 2/8/08 DATE:

CONSULTING CAPITAL COSTS

SUB-TOTAL

Consulting

Hydrogeologic Evaluation, Engineering Design, System Installation Oversight, Final System Documentation \$150,000

SUBTOTAL, CONSTRUCTION CAPITAL COSTS

\$150,000

30% Estimating Contingency

\$45,000

TOTAL, CONSULTING CAPITAL COSTS

\$200,000

<u>CONSTRUCTION CAPITAL COSTS</u>	QUANTITY	UNIT	UNIT COST	ITEM COST	SUB-TOTAL
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General Construction

\$181,600

Design Pump Test	1	LS	\$25,000	\$25,000
Mob./Demob.	1	LS	\$25,000	\$25,000
Erosion Controls	1	LS	\$8,000	\$8,000
Site Vegetation Clearing	1	LS	\$10,000	\$10,000
Pre-Engineering System Enclosure and Foundation	1	LS	\$40,000	\$40,000
PLC Control System and Electrical	1	LS	\$30,000	\$30,000
Blend Overburden Trench Spoil Into Existing Grade	1,805	CY	\$2.00	\$3,600
Startup/Testing	1	LS	\$20,000	\$20,000
Documentation Surveying	1	LS	\$10,000	\$10,000
Restoration of Disturbed Areas	1	LS	\$10,000	\$10,000

South Collection Trench Construction

\$277,200

Collection Trench Excavation	3,300	CY	\$6.00	\$19,800
Install (1") Washed River Rock	3,100	TONS	\$20.00	\$62,000
Install 6" Bentonite Seal	180	TONS	\$90.00	\$16,200
Install General Fill to Grade	1,495	CY	\$4.00	\$6,000
Install Groundwater Collection Sumps	5	EA	\$10,000	\$50,000
Pumps for Groundwater Collection Sumps (2 Each)	10	EA	\$3,000	\$30,000
6" HDPE Drain Tile For Collection Trench	2,750	LF	\$8.00	\$22,000
8 oz. Geosynthetic liner	57,400	SF	\$0.35	\$20,100
Underground Piping to Interim Pond B	2,580	LF	\$8.00	\$20,600
Electrical and Control Wiring for Each Well	6,100	LF	\$5.00	\$30,500

SUBTOTAL, CONSTRUCTION CAPITAL COSTS

\$458,800

30% Estimating Contingency

\$137,600

TOTAL, CONSTRUCTION CAPITAL COSTS

\$600,000

TOTAL CAPITAL COSTS

\$800,000

ANNUAL COSTS

\$36,000

Annual O & M Costs

O & M Sampling Labor & Equipment	1	LS	\$5,000	\$5,000
Discharge Sampling Analytical	1	LS	\$3,000	\$3,000
Annual Equipment Maintenance	1	LS	\$8,000	\$8,000
Electric Costs	1	LS	\$20,000	\$20,000

ANNUAL SUBTOTAL

\$36,000

30% Estimating Contingency

\$10,800

TOTAL ANNUAL COSTS

\$47,000

ASSUMPTIONS

- Groundwater collection via a 2,650 foot long collection trench sloped ($\geq 1.0\%$) to two collection sumps; total groundwater extraction is about 10-25 GPM.
- Trench design consists of 6" HDPE drain tile, a layer of geosynthetic, washed river rock, followed by 6" bentonite seal, backfilled to grade with general fill.
- This options assumes no treatment of extracted groundwater and discharge directly to the Interim Pond and/or the Drainage Collection Pond.
- Results of further hydrogeological assessment and design pump test could impact size and scope of the groundwater collection system.
- Additional sources of estimated costs: RS Means Site Work & Landscape Cost Data.
- Above is a preliminary estimate and may be revised if selected for final design.

GROUNDWATER MANAGEMENT ALTERNATIVE: Ash Stabilization

Pond D Closure Alternatives Report
 Hutsonville Power Station
 Ameren Services

NRT PROJECT NO.: 1954/2.3
 BY: CAR CHKD BY: BRH
 DATE: 6/27/05 EJT (5/19/05)

<u>CONSULTING CAPITAL COSTS</u>	SUB-TOTAL
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Consulting

Hydrogeologic Evaluation, Engineering Design, System Installation Oversight, Final System Documentation

\$500,000

SUBTOTAL, CONSTRUCTION CAPITAL COSTS	\$500,000
30% Estimating Contingency	\$150,000

TOTAL, CONSULTING CAPITAL COSTS	\$650,000
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<u>CONSTRUCTION CAPITAL COSTS</u>	QUANTITY	UNIT	UNIT COST	ITEM COST	SUB-TOTAL
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Construction

Bench Scale / Pilot Testing	1	LS	\$50,000	\$50,000	\$14,529,000
Stabilization Drill Rig Mobilization/Demob.	1	LS	\$250,000	\$250,000	
Fencing and Erosion Control	1	LS	\$20,000	\$20,000	
Stabilizing Reagent Materials	280,000	CY	\$19.00	\$5,320,000	
Treatment Via Shallow Soil Mixing Rig (SSM)	280,000	CY	\$30.00	\$8,400,000	
Additional Testing/Quality Control	1	LS	\$250,000	\$250,000	
Regrade Overburden From SSM Treatment	112,000	CY	\$2.00	\$224,000	
Documentation Surveying	1	LS	\$15,000	\$15,000	

SUBTOTAL, CONSTRUCTION CAPITAL COSTS	\$14,529,000
30% Estimating Contingency	\$4,358,700

TOTAL, CONSTRUCTION CAPITAL COSTS	\$18,900,000
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TOTAL CAPITAL COSTS	\$20,000,000
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ASSUMPTIONS

1. Total estimated area for saturated ash: areal extent ~ 790,000 ft², average thickness ~ 9.5 ft, average depth to bottom of saturated ash ~ 25 ft.
2. Based on above estimates 280,000 yd³ (790,000 ft² x 9.5 ft) targeted for SSM treatment.
3. This estimate is for stabilization of saturated ash only.
4. See final cover estimates for costs associated with final landfill cover construction less backfill costs (overburden from SSM treatment used for fill).
5. Earthwork quantities based on a 1.6 ton : 1 cubic yard (CY) ratio; all earthwork quantities are approximate and need to be field verified during design.
6. Additional sources of estimated costs: previous ash landfill cover construction, RS Means Site Work & Landscape Cost Data.
7. Above is a preliminary estimate and may be revised if selected for final design.

GROUNDWATER MANAGEMENT ALTERNATIVE: Ash Removal and Disposal, Recycling, or Beneficial Reuse

Pond D Closure Alternatives Report
 Hutsonville Power Station
 Ameren Services

NRT PROJECT NO.: 1954/2.3
 BY: CAR CHKD BY: BRH
 DATE: 6/27/05 EJT (5/19/05)

<u>CONSULTING CAPITAL COSTS</u>	SUB-TOTAL
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Consulting

Hydrogeologic Evaluation, Engineering Design, System Installation Oversight, Final System Documentation \$500,000

SUBTOTAL, CONSTRUCTION CAPITAL COSTS	\$500,000
30% Estimating Contingency	\$150,000
TOTAL, CONSULTING CAPITAL COSTS	\$650,000

<u>CONSTRUCTION CAPITAL COSTS</u>	QUANTITY	UNIT	UNIT COST	ITEM COST	SUB-TOTAL
Construction					\$17,345,000
Mob./Demob.	1	LS	\$50,000.00	\$50,000	
Site Facilities & Maintenance	1	LS	\$8,000.00	\$8,000	
Site Vegetation Clearing (22 acres)	22	ACRES	\$1,000.00	\$22,000	
Excavate Ash Overburden & Stockpile	550,000	CY	\$4.00	\$2,200,000	
Excavate Saturated Ash via Mudcat & Stockpile	280,000	CY	\$7.00	\$1,960,000	
Surface Water / Drainage Control / Erosion Controls	1	LS	\$100,000.00	\$100,000	
Import General Fill, Place & Compact	430,000	CY	\$8.40	\$3,612,000	
Off-Site Disposal/Recycling of Saturated Ash	280,000	CY	\$25.50	\$7,140,000	
Overburden Ash Replacement/Compaction/Regrade	550,000	CY	\$4.00	\$2,200,000	
Grain Size Analysis/Geotechnical Testing	1	LS	\$16,000.00	\$16,000	
Documentation Surveying	1	LS	\$15,000.00	\$15,000	
Revegetation (mulch, seed, fertilizer)	22	ACRES	\$1,000.00	\$22,000	
SUBTOTAL, CONSTRUCTION CAPITAL COSTS					\$17,345,000
30% Estimating Contingency					\$5,203,500
TOTAL, CONSTRUCTION CAPITAL COSTS					\$22,500,000
TOTAL CAPITAL COSTS					\$23,000,000

ASSUMPTIONS

1. Total estimated area for saturated ash: areal extent ~ 790,000 ft², average thickness ~ 9.5 ft, average depth to bottom of saturated ash ~ 25 ft (Table 3-2).
2. Based on above estimates: 280,000 yd³ saturated ash (790,000 ft² x 9.5 ft); 550,000 yd³ overburden ash (790,000 ft² x 15.5 ft + 80,000 yd³ - 2004 transfer) targeted for excavation (Table 3-2).
3. Estimate includes removal of saturated ash and replacement with clean fill to approximately 5 feet above the static water table ~ 430,000 yd³.
4. Excavated saturated ash to be stockpiled, dried and disposed/recycled off-site; overburden ash to be replaced atop clean fill.
5. See landfill cap estimates for costs associated with final landfill cover construction less backfill costs (placement of additional fill will raise grade).
6. Earthwork quantities based on a 1.6 ton : 1 cubic yard (CY) ratio; all earthwork quantities are approximate and need to be field verified during design.
7. Based on numbers discussed during 6-15-01 meeting including: \$4.00/ton to haul clean fill on-site.
8. Off-site disposal/recycling of ash cost based on previous cost estimates prepared by Hutsonville Power Station personnel for similar off-site disposal (\$7.00/ton transportation, \$7.40/ton disposal, \$1.50/ton loading @ 1.6 tons/yd³ ~ \$25.50/yd³).
 This cost could significantly increase with variable landfill pricing.
9. Additional sources of estimated costs: previous ash landfill cover construction, RS Means Site Work & Landscape Cost Data.
10. Above is a preliminary estimate and may be revised if selected for final design.

GROUNDWATER MANAGEMENT ALTERNATIVE: Ash Removal and Off-Site Disposal

 Pond D Closure Alternatives Report
 Hutsonville Power Station
 Ameren Services

 NRT PROJECT NO.: 1954/2.3
 BY: CAR CHKD BY: BRH
 DATE: 6/27/05 EJT (5/19/05)

CONSULTING CAPITAL COSTS
Consulting

Hydrogeologic Evaluation, Engineering Design, System Installation Oversight, Final System Documentation	\$500,000
SUBTOTAL, CONSTRUCTION CAPITAL COSTS	\$500,000
30% Estimating Contingency	\$150,000

TOTAL, CONSULTING CAPITAL COSTS

<u>CONSTRUCTION CAPITAL COSTS</u>	QUANTITY	UNIT	UNIT COST	ITEM COST	SUB-TOTAL
<u>Construction</u>					\$25,558,000
Mob./Demob.	1	LS	\$50,000.00	\$50,000	
Site Facilities & Maintenance	1	LS	\$8,000.00	\$8,000	
Site Vegetation Clearing (22 acres)	22	ACRES	\$1,000.00	\$22,000	
Excavate Ash & Stockpile	550,000	CY	\$4.00	\$2,200,000	
Excavate Saturated Ash via Mudcat & Stockpile	280,000	CY	\$7.00	\$1,960,000	
Surface Water / Drainage Control / Erosion Controls	1	LS	\$100,000.00	\$100,000	
Off-Site Disposal/Recycling of Ash	830,000	CY	\$25.50	\$21,165,000	
Grain Size Analysis/Geotechnical Testing	1	LS	\$16,000.00	\$16,000	
Documentation Surveying	1	LS	\$15,000.00	\$15,000	
Revegetation (mulch, seed, fertilizer)	22	ACRES	\$1,000.00	\$22,000	
SUBTOTAL, CONSTRUCTION CAPITAL COSTS					\$25,558,000
30% Estimating Contingency					\$7,667,400
<u>TOTAL, CONSTRUCTION CAPITAL COSTS</u>					\$33,200,000
TOTAL CAPITAL COSTS					\$34,000,000

ASSUMPTIONS

1. Total estimated area for saturated ash: areal extent ~ 790,000 ft², average thickness ~ 9.5 ft, average depth to bottom of saturated ash ~ 25 ft.
2. Based on above estimates: 280,000 yd³ saturated ash (790,000 ft² x 9.5 ft)
3. Total estimated area for ash: areal extent ~ (22 acres) 966,000 ft², average thickness estimated from Geoprobe boring logs (20.9 feet).
4. Based on above estimates: 830,000 yd³ ash (966,000 ft² x average thickness [20.9 feet] + 80,000 yd³ ash transfer in 2004).
5. Estimate includes removal of dry ash (550,000 yd³) and saturated ash (280,000 yd³).
6. All estimated areas and volumes are provided in Table 3-2.
7. Excavated ash and saturated ash to be stockpiled, dried and disposed/recycled off-site
8. This estimate does not include replacement of clean fill to an elevation above the static water table.
9. Earthwork quantities based on a 1.6 ton : 1 cubic yard (CY) ratio; all earthwork quantities are approximate and need to be field verified during design.
10. Off-site disposal/recycling of ash cost based on previous cost estimates prepared by Hutsonville Power Station personnel for similar off-site disposal (\$7.00/ton transportation, \$7.40/ton disposal, \$1.50/ton loading @ 1.6 tons/yd³ ~ \$25.50/yd³).
This cost could significantly increase with variable landfill pricing.
11. Additional sources of estimated costs: previous final cover construction, RS Means Site Work & Landscape Cost Data.
12. Above is a preliminary estimate and may be revised if selected for final design.

FINAL COVER ALTERNATIVE: Geomembrane

Pond D Closure Alternatives Report
 Hutsonville Power Station
 Ameren Services

NRT PROJECT NO.: 1954/2.3
 BY: CAR/KJB CHKD BY: BRH/EJT
 DATE: O-6/05, U-4/09

<u>CONSULTING CAPITAL COSTS</u>	SUB-TOTAL
<u>Consulting</u>	
Hydrogeologic Evaluation, Engineering Design, System Installation Oversight, Final System Documentation	\$400,000
SUBTOTAL, CONSTRUCTION CAPITAL COSTS	\$400,000
30% Estimating Contingency	\$120,000
TOTAL, CONSULTING CAPITAL COSTS	\$520,000

<u>CONSTRUCTION CAPITAL COSTS</u>	QUANTITY	UNIT	UNIT COST	ITEM COST	SUB-TOTAL
<u>Construction</u>					\$2,594,300
Mob./Demob.	1	LS	\$25,000	\$25,000	
Site Facilities & Maintenance (Erosion Controls)	1	LS	\$8,000	\$8,000	
Site Vegetation Clearing (22 acres)	22	ACRES	\$1,000	\$22,000	
Regrade Stockpiled Ash to Fill Depressions	50,500	CY	\$2.00	\$101,000	
4" Bedding Layer for PVC (Silty Sand)	12,000	CY	\$12.00	\$144,000	
Install 30 mil PVC Geomembrane Cover	966,000	SF	\$0.23	\$222,200	
Install 200 mil Geocomposite Drainage Layer	966,000	SF	\$0.28	\$270,500	
Place Rooting Zone to Complete Protective Layer	105,400	CY	\$8.40	\$885,400	
Place Beneficial Reuse Ash to Construct Grade	20,000	CY	\$4.00	\$80,000	
Place General Fill to Construct Grade	86,100	CY	\$8.40	\$723,200	
Grain Size Analysis/Geotechnical Testing	1	LS	\$10,000	\$10,000	
Site Drainage/piping	22	ACRES	\$3,000	\$66,000	
Documentation Surveying	1	LS	\$15,000	\$15,000	
Revegetation (mulch, seed, fertilizer)	22	ACRES	\$1,000	\$22,000	
SUBTOTAL, CONSTRUCTION CAPITAL COSTS					\$2,594,300
30% Estimating Contingency					\$778,300
TOTAL, CONSTRUCTION CAPITAL COSTS					\$3,400,000
TOTAL CAPITAL COSTS					\$3,900,000

ASSUMPTIONS

1. Total area of Pond D for final cover estimated at 966,000 SF, approximately 22 acres.
2. Geosynthetic Cover consists of: 4" Bedding layer - 30 mil PVC Geomembrane - 200 mil Geocomposite Drainage Layer - 3 foot Protective Soil Layer.
3. All estimated final cover alternative material quantities are provided in Table 3-3.
4. Earthwork quantities based on a 1.6 ton : 1 cubic yard (CY) ratio; all earthwork quantities are approximate and need to be field verified during design.
5. Above costs based on numbers discussed during 6-15-01 meeting including: \$4.00/ton to haul clean fill on-site.
6. Additional sources of estimated costs: previous final cover construction, RS Means Site Work & Landscape Cost Data.
7. Above is a preliminary estimate and may be revised if selected for final design.

FINAL COVER ALTERNATIVE: Compacted Clay

Pond D Closure Alternatives Report
 Hutsonville Power Station
 Ameren Services

NRT PROJECT NO.: 1954/2.3
 BY: CAR/KJB CHKD BY: BRH/EJT
 DATE: O-7/05, U-4/09

<u>CONSULTING CAPITAL COSTS</u>	SUB-TOTAL
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Consulting

Hydrogeologic Evaluation, Engineering Design, System Installation Oversight, Final System Documentation	\$450,000
SUBTOTAL, CONSTRUCTION CAPITAL COSTS	\$450,000
30% Estimating Contingency	\$135,000

TOTAL, CONSULTING CAPITAL COSTS	\$590,000
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<u>CONSTRUCTION CAPITAL COSTS</u>	QUANTITY	UNIT	UNIT COST	ITEM COST	SUB-TOTAL
Construction					\$2,794,400
Mob./Demob.	1	LS	\$25,000	\$25,000	
Site Facilities & Maintenance (Erosion Controls)	1	LS	\$8,000	\$8,000	
Site Vegetation Clearing (22 acres)	22	ACRES	\$1,000	\$22,000	
Regrade Stockpiled Ash to Fill Depressions	50,500	CY	\$2.00	\$101,000	
Place Beneficial Reuse Ash for Protective Layer	20,000	CY	\$4.00	\$80,000	
Place Rooting Zone to Complete Protective Layer	85,400	CY	\$8.40	\$717,400	
Clay - Purchased, Delivered and Installed (3.0')	105,400	CY	\$16.50	\$1,739,100	
Place General Fill to Construct Grade	700	CY	\$8.40	\$5,900	
Grain Size Analysis/Geotechnical Testing	1	LS	\$15,000	\$15,000	
Site Drainage	22	ACRES	\$2,000	\$44,000	
Documentation Surveying	1	LS	\$15,000	\$15,000	
Revegetation (mulch, seed, fertilizer)	22	ACRES	\$1,000	\$22,000	
SUBTOTAL, CONSTRUCTION CAPITAL COSTS					\$2,794,400
30% Estimating Contingency					\$838,300
TOTAL, CONSTRUCTION CAPITAL COSTS					\$3,600,000
TOTAL CAPITAL COSTS					\$4,200,000

ASSUMPTIONS

1. Total area of Pond D for final cover estimated at 966,000 SF, approximately 22 acres.
2. Compacted Clay cover consists of: 3 foot Compacted Clay Layer - 3 foot Protective Soil Layer.
3. All estimated final cover alternative material quantities are provided in Table 3-3.
4. Earthwork quantities based on a 1.6 ton : 1 cubic yard (CY) ratio; all earthwork quantities are approximate and need to be field verified during design.
5. Above costs based on numbers discussed during 6-15-01 meeting including: \$4.00/ton to haul clean fill on-site.
6. Additional sources of estimated costs: previous final cover construction, RS Means Site Work & Landscape Cost Data.
7. Above is a preliminary estimate and may be revised if selected for final design.

FINAL COVER ALTERNATIVE: Layered Earth

Pond D Closure Alternatives Report
 Hutsonville Power Station
 Ameren Services

NRT PROJECT NO.: 1954/2.3
 BY: CAR/KJB CHKD BY: BRH/EJT
 DATE: 0-7/05, U-4/09

<u>CONSULTING CAPITAL COSTS</u>	SUB-TOTAL
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Consulting

Hydrogeologic Evaluation, Engineering Design, System Installation Oversight, Final System Documentation	\$250,000
SUBTOTAL, CONSTRUCTION CAPITAL COSTS	\$250,000
30% Estimating Contingency	\$75,000

TOTAL, CONSULTING CAPITAL COSTS \$330,000

<u>CONSTRUCTION CAPITAL COSTS</u>	QUANTITY	UNIT	UNIT COST	ITEM COST	SUB-TOTAL
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<u>Construction</u>					\$1,993,900
Mob./Demob.	1	LS	\$25,000	\$25,000	
Site Facilities & Maintenance (Erosion Controls)	1	LS	\$8,000	\$8,000	
Site Vegetation Clearing (22 acres)	22	ACRES	\$1,000	\$22,000	
Regrade Stockpiled Ash to Fill Depressions	50,500	CY	\$2.00	\$101,000	
Place Drainage Layer (6' Clean Sand)	17,600	CY	\$12.00	\$211,200	
Place Rooting Zone for Protective Layer	87,800	CY	\$8.40	\$737,500	
Place Beneficial Reuse Ash to Make Grade	20,000	CY	\$4.00	\$80,000	
Place General Fill to Construct Grade	86,100	CY	\$8.40	\$723,200	
Grain Size Analysis/Geotechnical Testing	1	LS	\$5,000	\$5,000	
Site Drainage	22	ACRES	\$2,000	\$44,000	
Documentation Surveying	1	LS	\$15,000	\$15,000	
Revegetation (mulch, seed, fertilizer)	22	ACRES	\$1,000	\$22,000	

SUBTOTAL, CONSTRUCTION CAPITAL COSTS	\$1,993,900
30% Estimating Contingency	\$598,200
TOTAL, CONSTRUCTION CAPITAL COSTS	\$2,600,000

TOTAL CAPITAL COSTS \$2,900,000

ASSUMPTIONS

1. Total area of Pond D for final cover estimated at 966,000 SF, approximately 22 acres.
2. Earthen Cover Consists of: 6" Sand Drainage Layer (Capillary Barrier) - 2.5 foot Protective Soil Layer.
3. All estimated final cover alternative material quantities are provided in Table 3-3.
4. Earthwork quantities based on a 1.6 ton : 1 cubic yard (CY) ratio; all earthwork quantities are approximate and need to be field verified during design.
5. Above costs based on numbers discussed during 6-15-01 meeting including: \$4.00/ton to haul clean fill on-site.
6. Additional sources of estimated costs: previous final cover construction, RS Means Site Work & Landscape Cost Data.
7. Above is a preliminary estimate and may be revised if selected for final design.

FINAL COVER ALTERNATIVE: Pozzolanic
 Pond D Closure Alternatives Report
 Hutsonville Power Station
 Ameren Services

NRT PROJECT NO.: 1954/2.3
 BY: CAR/KJB CHKD BY: BRH/EJT
 DATE: 0-6/05, U-4/09

<u>CONSULTING CAPITAL COSTS</u>	SUB-TOTAL
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Consulting

Hydrogeologic Evaluation, Engineering Design, System Installation Oversight, Final System Documentation \$500,000
 Geotechnical Evaluation

SUBTOTAL, CONSTRUCTION CAPITAL COSTS	\$500,000
30% Estimating Contingency	\$150,000
TOTAL, CONSULTING CAPITAL COSTS	\$650,000

<u>CONSTRUCTION CAPITAL COSTS</u>	QUANTITY	UNIT	UNIT COST	ITEM COST	SUB-TOTAL
Construction					\$2,576,717
Mob./Demob.	1	LS	\$324,108	\$324,108	
Site Facilities & Maintenance (Erosion Controls)	1	LS	\$8,000	\$8,000	
Regrade Stockpiled Ash to Fill Depressions	50,500	CY	\$1.97	\$99,485	
Excavate Ash From Pond A for Pozzolanic Mix	100,480	CY	\$1.81	\$181,869	
Blend Ash w/ Reagents to Form Pozzolanic Mix	100,480	CY	\$1.86	\$186,893	
Place 3.0' Pozzolanic Ash Final Cover	100,480	CY	\$1.61	\$161,773	
Place Fly Ash From Pond A to Construct Grade	700	CY	\$3.42	\$2,394	
Place Rooting Zone to Complete Protective Layer	100,480	CY	\$9.31	\$935,469	

Additional Construction Items Identified by VFL

Dewatering	1	LS	\$23,951	\$23,951
Reagent Cost - Cement ⁸	6,345	TON	\$95.00	\$602,775
Relocate Sluice Pipes and Supports	1	LS	\$50,000	\$50,000
SUBTOTAL, CONSTRUCTION CAPITAL COSTS				\$2,576,717
30% Estimating Contingency				\$773,000
TOTAL, CONSTRUCTION CAPITAL COSTS				\$3,349,717

TOTAL CAPITAL COSTS (Without Additional Excavation in Pond A)	\$4,000,000
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ASSUMPTIONS

1. Total area of Pond D for final cover estimated at 966,000 SF, approximately 22 acres.
2. Pozzolanic fly ash cover consists of: 3 foot Pozzolanic Fly ash Layer - 3 foot Protective Soil Layer.
3. Mix Design - 100% Fly Ash w/ 5% cement reagent (dry weight basis).
4. All estimated final cover alternative material quantities are provided in Table 3-3.
5. Earthwork quantities based on VFL Technology Corp., 2003 Estimates
6. Estimate 100,480 yd³ of ash excavated from Pond A for pozzolanic final cover.
7. Costs for the pozzolanic fly ash cover construction based on estimates provided by VFL Technology Corporation in their letter dated May 9, 2002. Several line items from *Pozzolanic Fly Ash Final Cover (Initial Estimate)* are incorporated in this estimate as described below:
 - Line Items: Site Vegetation Clearing (22 acres), Documentation Surveying, and Revegetation (mulch, seed, fertilizer) are included in *Mob./Demob.*
 - Line Item: Load and Haul to Processing Plant is included in *Excavate Ash From Pond A for Pozzolanic Mix*.
 - Line Items: Install Beneficial Reuse Ash for Protective Layer, Grain Size Analysis/Geotechnical Testing, and Site Drainage are included in *Install 3.0' Pozzolanic Ash Final Cover* and *Install General Fill to Complete Protective Layer*.
 - Construction Capital Cost not included in VFL Estimate.
8. Reagent cost provided in VFL Technology Corporation, 2003.
9. Above is a preliminary estimate and may be revised if selected for final design - the consulting costs and estimating contingency provided in this spreadsheet are conservative.

APPENDIX C

POTABLE WELL SURVEY



TECHNICAL MEMORANDUM

www.naturalrt.com

Date: April 10, 2009

Subject: Potable Well Search, Hutsonville Power Station Pond D

From: Bruce Hensel

On April 7, 2009, NRT searched for water supply well records within a 0.5-mile radius of Pond D using the Illinois State Geological Survey's (ISGS) online interactive map of well records¹. Six wells were identified within a 0.5-mile radius of Pond D as shown on the figure and table below. On the figure, the Wabash River is shown in blue as the eastern boundary of the state, and the grid lines outline the map Sections, which are also numbered in the center of each Section. The City of Hutsonville is shown to the south by the brown shading at the southern end of Section 20, and the southeast portion of Pond D is shown as a small triangular shape near the center of the map. Wells are identified by blue dots, and the yellow numbers adjacent to wells indicate total borehole depths. A green line depicting the approximate 0.5-mile radius from Pond D is also shown on the figure. Because the Wabash River forms a hydrologic barrier in the area, the well survey was not conducted for areas east of the river (in Indiana).

- Wells 60, 61, and 64 (located in Section 20) are owned by Margaret Dement and are used for irrigation (field inspection verifies that there is no well in the position denoted by 64 on the ISGS map, the actual location is likely east of this point).
- Well number 66 (located in the north-central portion of Section 20) is also used for irrigation and is owned by Duane Wampler.
- Hutsonville Power Station Plant wells #1 and #2 are numbered 90 and 88 and located in the southeast corner of Section 17.

Based on the well log information, the two closest wells outside of the 0.5-mile radius are:

- Well 90 (located in Section 18, northwest of Pond D) is owned by Jim Allison, and is identified by the well log as a private water well.
- Well 73, a City of Hutsonville water supply well located in the southeast portion of Section 20; approximately one mile south of Pond D.

TSD 000164

¹ Map and related well records from: <http://ablation.isgs.uiuc.edu/website/ilwater/viewer.htm>

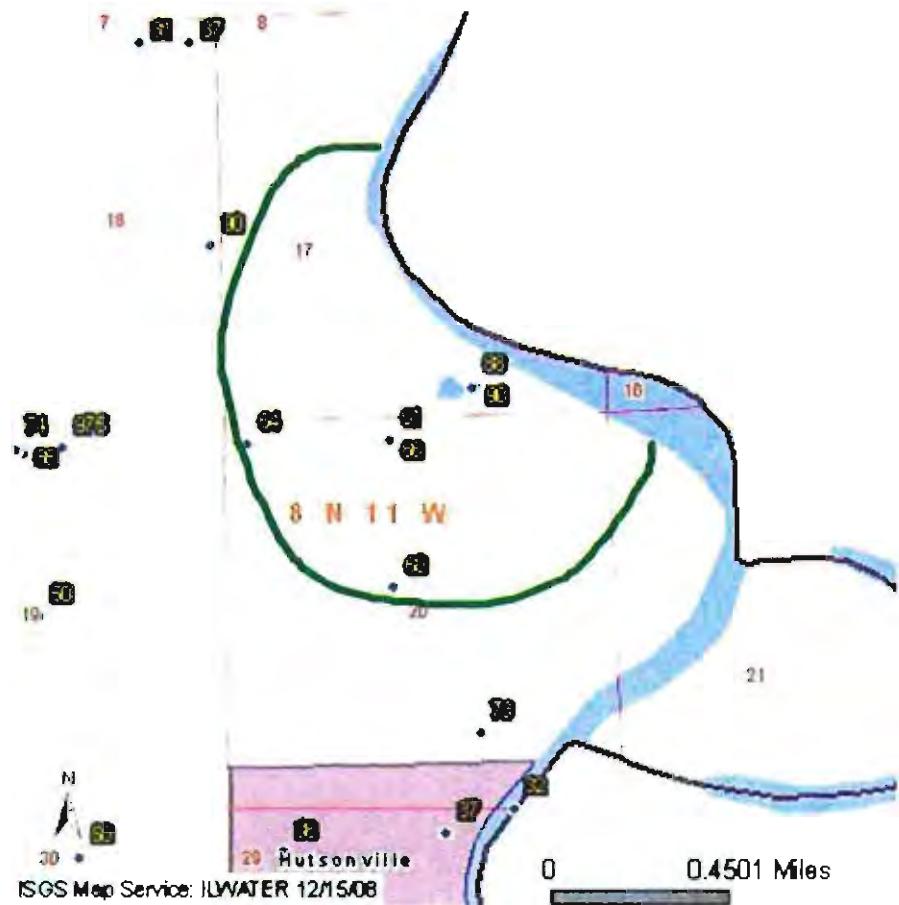
TECHNICAL MEMORANDUM

In June 2005, the following landowners were identified near the power station property: J.P. Allison, J. Grimes, Slaughter, M. Kelly, and M. Dement. There are wells, outside the 0.5-mile radius, servicing three residences on the Allison property to the northwest, and the Grimes residence to the west. These wells are upgradient of both the Station and upgradient monitoring well MW10. There are no ISGS records for potable wells servicing residences on the Dement, Slaughter, and Kelly properties, nor were wellheads visible when the properties were field-checked by personnel from the Hutsonville Power Station in 2005. Furthermore, the buildings on these three parcels are more than 0.5-mile south of Pond D, and wells, if present, would be near the buildings and outside the 0.5-mile radius. Finally, the Dement residence is reportedly connected to the City of Hutsonville public water supply. This information suggests that the Dement, Slaughter, and Kelly properties do not have wells within 0.5 mile of Pond D.

Well Identification	Section T8N, R11W	Location to 0.5-mile Radius of Pond D	Owner Name	Borehole Depth (feet)	Screened Formation	Screen Depth (feet)	
						Top	Bottom
120332991300 Power Plant	17	Within Radius	C.I.P.S. Hutsonville Unit	90	Deep Alluvial	57*	87
120333386700 Power Plant	17	Within Radius	Central IL Public Serv. Co.	88	Deep Alluvial	31	61
120333519600 Irrigation	20	Within Radius	Dement, Margaret R.	64	Deep Alluvial	46*	61
120333666700 Irrigation	20	Within Radius	Wampler, Duane	66	Deep Alluvial	34	64
120333675600 Irrigation	20	Within Radius	DeMent, Margaret	60	Deep Alluvial	32	62*
120333689800 Irrigation	20	Within Radius	DeMent, Margaret	61	Deep Alluvial	40	60
120333440500 Municipal	20	Outside Radius	City of Hutsonville	73	Deep Alluvial	30*	60*
120333741100 Domestic	18	Outside Radius	Allison, Jim	90	Sandstone	30	90

*: Estimated value, information unclear on the ISGS log.

TSD 000165



TSD 000166

Irrigation Well	Top	Bottom
dark clay	0	2
and & gravel	2	47
coarse sand	47	61
Total Depth		61
Casing: 16" PVC SCH 40 from -1' to 31'		
16" PVC SAWED SCREEN from 31' to 61'		
Screen: 30' of 16" diameter 32 slot		
Grout: BENSEAL from 3 to 20.		
Grout: GRAVEL PACK from 20 to 61.		
Static level 9' below casing top which is 1' above GL		
Location source: Location from permit		

Permit Date: June 7, 2002

Permit #:

COMPANY Speth, James

FARM DeMent, Margaret

DATE DRILLED June 12, 2002

NO

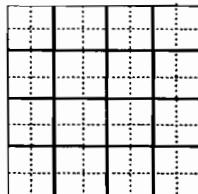
EVALUATION 2

COUNTY NO 36898

LOCATION

LATITUDE 39 127799 LONGITUDE -82 658791

COUNTY Crawford



$$30 = 8N = 11W$$

ILLINOIS STATE GEOLOGICAL SURVEY

Irrigation Well	Top	Bottom
topsoil	0	2
dry sand & gravel	2	22
coarse gray sand w/medium-large gravel	22	30
coarse gray sand with fine gravel	30	60
shale at	60	60
Total Depth		60
Casing: 12" SCH 40 PVC from 0' to 40'		
Screen: 20' of 12" diameter .06 slot		
Grout: BENTONITE from 0 to 30.		
Water from sand & gravel at 20' to 60'.		
Static level 23' below casing top which is 2' above GL		
Pumping level 0' when pumping at 750 gpm for 0 hours		
Address of well: same as above		
Location source: Location from permit		

Permit Date: January 19, 2000

Permit #:

COMPANY Hacker, Tim

FARM DeMent, Margaret

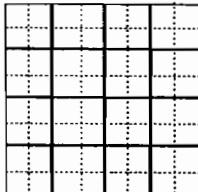
DATE DRILLED February 8, 2000 NO. 2

ELEVATION 0 COUNTY NO. 36756

LOCATION SE SE NW

LATITUDE 39.122411 LONGITUDE -87.658754

COUNTY Crawford API 120333675600 20 - 8N - 11W



ILLINOIS STATE GEOLOGICAL SURVEY

Irrigation Well	Top	Bottom
topsoil	0	3
slty dark clay	3	20
gray clay	20	25
coarse gray sand with fine-med gravel	25	66
gray clay at	66	66
Total Depth		66
Casing:	12"	SCH 40 PVC from 0' to 32'
Screen:	3'	of 12" diameter .06 slot
Grout:	BENTONITE	from 0 to 25.
Water from sand & gravel at 25' to 66'.		
Static level	11'	below casing top which is 1' above GL
Pumping level	0'	when pumping at 1000 gpm for 0 hours
Additional location info:	Lot: S of CIPS Power Plant	Subdivision:
Address of well:	Hutsonville, IL	
Location source:	Location from permit	

Permit Date: January 15, 1997

Permit #: 033-1-9

COMPANY Hacker, Tim
 FARM Wampler, Duane
 DATE DRILLED January 29, 1998 NO. 1
 ELEVATION 0 COUNTY NO. 36667
 LOCATION NE NE NW
 LATITUDE 39.127799 LONGITUDE -87.658791
 COUNTY Crawford API 120333666700 20 - 8N - 11W

ILLINOIS STATE GEOLOGICAL SURVEY

Irrigation Well	Top	Bottom
SS #66941 (0'-65')	0	0
top soil	0	1
fine brown sand	1	13
coarse brown sand	13	45
gravel & sand	45	64
Total Depth		64
Casing: 16" PVC WC SCH 80 from 2' to 64'		
Screen: 30' of 16" diameter .12 slot		
Grout: BENTONITE from 0 to 0.		
Water from sand & gravel at 0' to 0'.		
Sample set # 66941 (0' - 65') Received: June 2, 1989		
Location source: Location from permit		

Permit Date: February 10, 1989

Permit #: 139628

COMPANY Erwin, Harold E.

FARM Dement, Margaret R.

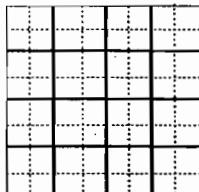
DATE DRILLED March 24, 1989 NO.

ELEVATION 0 COUNTY NO. 35196

LOCATION NW NW NW

LATITUDE 39.12778 LONGITUDE -87.665637

COUNTY Crawford API 120333519600 20 - 8N - 11W



TSD 000170

Municipal Water Supply	Top	Bottom
fine dark brown sand	0	5
line to medium sand	5	30
fine/med sand & gvl	30	73
Total Depth		73
Casing: 10" STEEL 40.48#/FT from -5' to 61'		
Screen: 15' of 10" diameter .07999999821186066 slot		
Grout: CEMENT from 0 to 20.		
Size hole below casing: 24"		
Water from Alluvial at 77' to 61'.		
Static level 245' below casing top which is 5' above GL		
Pumping level 35' when pumping at 400 gpm for 5 hours		
Permanent pump installed at 50' on June 24, 1987, with a capacity of 300 gpm		
Additional Lot: #3C Subdivision: Jacob A. Parker location info:		
Location source: Location from permit		

Permit Date: June 1, 1987

Permit #: 132217

COMPANY Peterson, Steven R.

FARM Hutsonville, City of

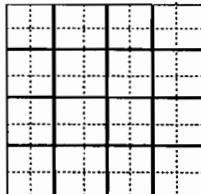
DATE DRILLED June 24, 1987 NO. 4

ELEVATION 0 COUNTY NO. 34405

LOCATION 557'S line, 1855'E line of section

LATITUDE 39.117019 LONGITUDE -87.654743

COUNTY Crawford API 120333440500 20 - 8N - 11W



ILLINOIS STATE GEOLOGICAL SURVEY

Industrial Water Well	Top	Bottom
cinders, sand & clay	0	5
) bld to soft clay	5	22
soft gray clay	22	26
f-med s, gvl & bld	26	88
Total Depth		88
Casing: 26" .375 WALL from 0' to 57'		
42" .375 WALL from -22' to 30'		
Screen: 30' of 26" diameter .5 slot		
Grout: CEMENT from 5 to 30.		
Size hole below casing: 42"		
Water from alluvial at 25' to 97'.		
Static level 15' below casing top which is 0' above GL		
Pumping level 22' when pumping at 826 gpm for 5 hours		
Permanent pump installed at 60' on , with a capacity of 600 gpm		
Driller's Log filed		
Location source: Location from permit		

Permit Date: August 26, 1983

Permit #: 109053

COMPANY Ruester, John T.

FARM Central Il Public Serv.Co.

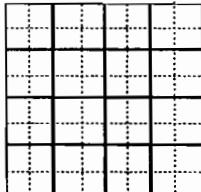
DATE DRILLED October 28, 1983 NO. 4

ELEVATION 440GL COUNTY NO. 33867

LOCATION 350'S line, 150'W line of SE SW SE

LATITUDE 39.129677 LONGITUDE -87.654832

COUNTY Crawford API 120333386700 17 - 8N - 11W

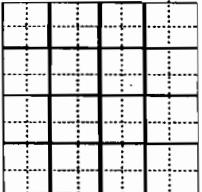


ILLINOIS STATE GEOLOGICAL SURVEY

Water Well	Top	Bottom
brown clay, very soft	0	20
gray clay very soft	20	25
crs sand & gravel w/bldr @ 40' (wtr brg)	25	54
gravel w/boulders very loose (wtr brg)	54	75
medium/fine sand very loose (wtr brg)	75	90
bedrock at	90	90
Total Depth		90
Casing: 42" from -1' to 30'		
26" from -1' to 57'		
Screen: 30' of 26" diameter 6 slot		
Water from sand & gravel at 25' to 87'.		
Static level 18' below casing top which is 2' above GL		
Pumping level 24' when pumping at 825 gpm for 3 hours		
Driller's Log filed		
Sample set # 60350 (0' - 85') Received: June 1, 1976		
Location source: Location from permit		

Permit Date: May 18, 1976

Permit #: 47367

COMPANY	owner	
FARM	C.I.P.S.-Hutsonville Unit	
DATE DRILLED	May 25, 1976	
NO. 3		
ELEVATION	440TM	
COUNTY NO.	29913	
LOCATION	350'S line, 1630'E line of SE	
LATITUDE	39.129678	
LONGITUDE	-87.654686	
COUNTY	Crawford	
API	120332991300	
	17 - 8N - 11W	

ILLINOIS STATE GEOLOGICAL SURVEY

Private Water Well	Top	Bottom
sandy clay	0	5
sand & gravel	5	8
gray hardpan	8	15
gray sandstone	15	51
gry shale	51	64
coal	64	68
gray shale	68	90
Total Depth		90
Casing:	5" PVC SDR 21 from -2' to 90'	
Grout:	BENTONITE from 0 to 30.	
Water from sandstone at 15' to 51'.		
Static level 11' below casing top which is 2' above GL		
Pumping level 85' when pumping at gpm for 5 hours		
Permanent pump installed at 85' on December 24, 2007, with a capacity of 10 gpm		
Address of well: same as above		
Location source: Location from permit		

Permit Date: December 17, 2007

Permit #: 033-7-0

COMPANY Van Gilder, Richard E.

FARM Allison, Jim

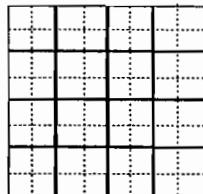
DATE DRILLED December 20, 2007 NO.

ELEVATION COUNTY NO. 37411

LOCATION NE NE SE

LATITUDE 39.135033 LONGITUDE -87.66725

COUNTY Crawford API 120333741100 18 - 8N - 11W



TSD 000174